

AD A 042755

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APPENDIX A

THE ARDC MODEL ATMOSPHERE, 1959.

App. A thru E.

1 Air Force

The atmosphere properties listed on pages A.2 through A.63 are properties of "The ARDC Model Atmosphere, 1959". Background information and basic equations describing this atmosphere may be found in: AFCRC-TR-59-267, Air Force Surveys in Geophysics, No. 115, The ARDC Model Atmosphere, 1959, by: R. A. Minzner, K. S. W. Champion, and H. L. Pond

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14 AFRLC-TR-59-267-A, A-E  
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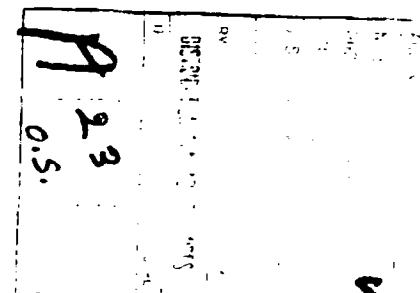
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H <sub>c</sub> (Feet)	P <sub>a</sub> ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	T <sub>a</sub> ("K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
-1000.	41.010	1.0364	0.9649	290.14	17.034	1.0069	1.0034
-900.	40.849	1.0327	0.9684	289.94	17.028	1.0062	1.0031
-800.	40.708	1.0290	0.9718	289.74	17.022	1.0055	1.0027
-700.	40.678	1.0253	0.9753	289.55	17.016	1.0048	1.0024
-600.	40.567	1.0216	0.9789	289.35	17.010	1.0041	1.0021
-500.	40.458	1.0179	0.9824	289.15	17.004	1.0034	1.0017
-400.	40.349	1.0143	0.9859	288.95	16.999	1.0028	1.0014
-300.	40.239	1.0106	0.9895	288.75	16.993	1.0021	1.0010
-200.	40.130	1.0070	0.9931	288.56	16.987	1.0014	1.0007
-100.	40.021	1.0033	0.9967	288.36	16.981	1.0007	1.0003
0.	39.921	1.0000	1.0000	288.16	16.975	1.0000	1.0000
100.	39.813	0.9964	1.0036	287.96	16.969	0.9993	0.9997
200.	39.706	0.9928	1.0073	287.76	16.964	0.9986	0.9993
300.	39.598	0.9892	1.0109	287.57	16.958	0.9979	0.9990
400.	39.491	0.9856	1.0146	287.37	16.952	0.9972	0.9986
500.	39.385	0.9821	1.0183	287.17	16.946	0.9966	0.9983
600.	39.278	0.9785	1.0220	286.97	16.940	0.9959	0.9979
700.	39.172	0.9750	1.0257	286.77	16.934	0.9952	0.9976
800.	39.066	0.9714	1.0294	286.58	16.929	0.9945	0.9972
900.	38.961	0.9679	1.0332	286.38	16.923	0.9938	0.9969
1000.	38.855	0.9644	1.0369	286.18	16.917	0.9931	0.9966
1100.	38.751	0.9609	1.0407	285.98	16.911	0.9924	0.9962
1200.	38.646	0.9574	1.0445	285.78	16.905	0.9917	0.9959
1300.	38.542	0.9539	1.0483	285.58	16.899	0.9911	0.9955
1400.	38.438	0.9504	1.0522	285.39	16.893	0.9904	0.9952
1500.	38.335	0.9470	1.0560	285.19	16.888	0.9897	0.9948
1600.	38.231	0.9435	1.0599	284.99	16.882	0.9890	0.9945
1700.	38.128	0.9401	1.0637	284.79	16.876	0.9883	0.9941
1800.	38.025	0.9366	1.0676	284.59	16.870	0.9876	0.9938
1900.	37.923	0.9332	1.0716	284.40	16.864	0.9869	0.9934
2000.	37.821	0.9298	1.0755	284.20	16.858	0.9862	0.9931
2100.	37.719	0.9264	1.0794	284.00	16.852	0.9856	0.9928
2200.	37.619	0.9230	1.0834	283.80	16.845	0.9849	0.9924
2300.	37.517	0.9196	1.0874	283.60	16.841	0.9842	0.9921
2400.	37.416	0.9163	1.0914	283.41	16.835	0.9835	0.9917
2500.	37.315	0.9129	1.0954	283.21	16.829	0.9828	0.9914
2600.	37.215	0.9095	1.0994	283.01	16.823	0.9821	0.9910
2700.	37.115	0.9062	1.1035	282.81	16.817	0.9814	0.9907
2800.	37.015	0.9029	1.1076	282.61	16.811	0.9807	0.9903
2900.	36.916	0.8996	1.1117	282.41	16.805	0.9801	0.9900
3000.	36.817	0.8962	1.1158	282.22	16.799	0.9794	0.9896
3100.	36.718	0.8929	1.1199	282.02	16.793	0.9787	0.9893

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
-1000.	1.0296	1.0147	0.9855	0.9682	0.9616	663.3148
-900.	1.0266	1.0132	0.9870	0.9714	0.9654	663.0883
-800.	1.0236	1.0117	0.9884	0.9745	0.9632	662.8617
-700.	1.0206	1.0103	0.9898	0.9777	0.9730	662.6350
-600.	1.0176	1.0088	0.9913	0.9809	0.9768	662.4083
-500.	1.0147	1.0073	0.9927	0.9841	0.9807	662.1814
-400.	1.0117	1.0058	0.9942	0.9873	0.9846	661.9546
-300.	1.0088	1.0044	0.9956	0.9905	0.9885	661.7276
-200.	1.0058	1.0029	0.9971	0.9938	0.9924	661.5005
-100.	1.0029	1.0015	0.9986	0.9970	0.9963	661.2734
0.	1.0000	1.0000	1.0000	1.0000	1.0000	661.0462
100.	0.9971	0.9985	1.0015	1.0033	1.0040	660.8189
200.	0.9942	0.9971	1.0029	1.0066	1.0090	660.5915
300.	0.9913	0.9956	1.0044	1.0099	1.0120	660.3641
400.	0.9884	0.9942	1.0059	1.0132	1.0160	660.1366
500.	0.9855	0.9927	1.0074	1.0165	1.0200	659.9090
600.	0.9826	0.9912	1.0088	1.0199	1.0241	659.6813
700.	0.9797	0.9898	1.0103	1.0232	1.0292	659.4536
800.	0.9768	0.9883	1.0118	1.0266	1.0323	659.2257
900.	0.9739	0.9869	1.0133	1.0300	1.0364	658.9978
1000.	0.9711	0.9854	1.0148	1.0334	1.0405	658.7698
1100.	0.9682	0.9840	1.0163	1.0368	1.0447	658.5417
1200.	0.9654	0.9825	1.0178	1.0402	1.0488	658.3136
1300.	0.9625	0.9811	1.0193	1.0436	1.0530	658.0854
1400.	0.9597	0.9796	1.0208	1.0471	1.0573	657.8571
1500.	0.9568	0.9782	1.0223	1.0505	1.0615	657.6287
1600.	0.9540	0.9767	1.0238	1.0540	1.0657	657.4002
1700.	0.9512	0.9753	1.0253	1.0575	1.0700	657.1717
1800.	0.9484	0.9739	1.0269	1.0610	1.0743	656.9430
1900.	0.9456	0.9724	1.0284	1.0645	1.0786	656.7143
2000.	0.9428	0.9710	1.0299	1.0681	1.0830	656.4855
2100.	0.9400	0.9695	1.0314	1.0716	1.0873	656.2567
2200.	0.9372	0.9681	1.0330	1.0752	1.0917	656.0277
2300.	0.9344	0.9666	1.0345	1.0788	1.0961	655.7987
2400.	0.9316	0.9652	1.0360	1.0824	1.1005	655.5696
2500.	0.9289	0.9638	1.0376	1.0860	1.1049	655.3404
2600.	0.9261	0.9623	1.0391	1.0896	1.1094	655.1111
2700.	0.9233	0.9609	1.0407	1.0932	1.1139	654.8818
2800.	0.9206	0.9595	1.0422	1.0969	1.1184	654.6524
2900.	0.9179	0.9580	1.0438	1.1005	1.1229	654.4229
3000.	0.9151	0.9566	1.0454	1.1042	1.1275	654.1933
3100.	0.9124	0.9552	1.0469	1.1079	1.1320	653.9636



$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
3200.	26.619	0.8896	1.1240	281.82	16.788	0.9780	0.9889
3300.	26.521	0.8864	1.1282	281.62	16.782	0.9773	0.9886
3400.	26.423	0.8831	1.1324	281.42	16.776	0.9766	0.9882
3500.	26.326	0.8798	1.1366	281.23	16.770	0.9759	0.9879
3600.	26.228	0.8766	1.1408	281.03	16.764	0.9752	0.9875
3700.	26.131	0.8733	1.1450	280.83	16.758	0.9746	0.9872
3800.	26.034	0.8701	1.1493	280.63	16.752	0.9739	0.9869
3900.	25.938	0.8669	1.1536	280.43	16.746	0.9732	0.9865
4000.	25.842	0.8637	1.1579	280.24	16.740	0.9725	0.9862
4100.	25.746	0.8605	1.1622	280.04	16.734	0.9718	0.9858
4200.	25.650	0.8573	1.1665	279.84	16.728	0.9711	0.9855
4300.	25.555	0.8541	1.1709	279.64	16.722	0.9704	0.9851
4400.	25.460	0.8509	1.1752	279.44	16.717	0.9697	0.9848
4500.	25.365	0.8477	1.1796	279.24	16.711	0.9691	0.9844
4600.	25.271	0.8446	1.1840	279.05	16.705	0.9684	0.9841
4700.	25.177	0.8414	1.1885	278.85	16.699	0.9677	0.9837
4800.	25.083	0.8383	1.1929	278.65	16.693	0.9670	0.9834
4900.	24.989	0.8352	1.1974	278.45	16.687	0.9663	0.9830
5000.	24.896	0.8320	1.2019	278.25	16.681	0.9656	0.9827
5100.	24.803	0.8289	1.2064	278.06	16.675	0.9649	0.9823
5200.	24.710	0.8258	1.2109	277.86	16.669	0.9642	0.9820
5300.	24.618	0.8227	1.2154	277.66	16.663	0.9636	0.9816
5400.	24.525	0.8197	1.2200	277.46	16.657	0.9629	0.9813
5500.	24.433	0.8166	1.2246	277.26	16.651	0.9622	0.9809
5600.	24.342	0.8135	1.2292	277.07	16.645	0.9615	0.9806
5700.	24.250	0.8105	1.2338	276.87	16.639	0.9608	0.9802
5800.	24.159	0.8074	1.2385	276.67	16.633	0.9601	0.9799
5900.	24.069	0.8044	1.2432	276.47	16.627	0.9594	0.9795
6000.	23.978	0.8014	1.2479	276.27	16.621	0.9587	0.9792
6100.	23.888	0.7984	1.2526	276.07	16.615	0.9581	0.9788
6200.	23.798	0.7954	1.2573	275.88	16.610	0.9574	0.9785
6300.	23.708	0.7924	1.2621	275.68	16.604	0.9567	0.9781
6400.	23.619	0.7894	1.2668	275.48	16.598	0.9560	0.9778
6500.	23.530	0.7864	1.2716	275.28	16.592	0.9553	0.9774
6600.	23.441	0.7834	1.2765	275.08	16.586	0.9546	0.9770
6700.	23.352	0.7805	1.2813	274.89	16.580	0.9539	0.9767
6800.	23.264	0.7775	1.2862	274.69	16.574	0.9532	0.9763
6900.	23.176	0.7746	1.2911	274.49	16.568	0.9526	0.9760
7000.	23.088	0.7716	1.2960	274.29	16.562	0.9519	0.9756
7100.	23.000	0.7687	1.3009	274.09	16.556	0.9512	0.9753
7200.	22.913	0.7658	1.3059	273.90	16.550	0.9505	0.9749
7300.	22.826	0.7629	1.3108	273.70	16.544	0.9498	0.9746

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
3200.	0.9097	0.9538	1.0485	1.1116	1.1346	653.7339
3300.	0.9069	0.9523	1.0501	1.1153	1.1412	653.5041
3400.	0.9042	0.9509	1.0516	1.1191	1.1459	653.2741
3500.	0.9015	0.9495	1.0532	1.1229	1.1505	653.0442
3600.	0.8978	0.9481	1.0548	1.1266	1.1552	652.8141
3700.	0.8961	0.9466	1.0564	1.1304	1.1599	652.5839
3800.	0.8934	0.9452	1.0580	1.1342	1.1646	652.3537
3900.	0.8908	0.9438	1.0595	1.1380	1.1694	652.1234
4000.	0.8881	0.9424	1.0611	1.1418	1.1741	651.8930
4100.	0.8854	0.9410	1.0627	1.1457	1.1789	651.6625
4200.	0.8828	0.9395	1.0643	1.1495	1.1837	651.4319
4300.	0.8801	0.9381	1.0659	1.1534	1.1886	651.2013
4400.	0.8774	0.9367	1.0676	1.1573	1.1934	650.9706
4500.	0.8748	0.9353	1.0692	1.1612	1.1983	650.7398
4600.	0.8722	0.9339	1.0708	1.1652	1.2032	650.5089
4700.	0.8695	0.9325	1.0724	1.1691	1.2081	650.2779
4800.	0.8669	0.9311	1.0740	1.1731	1.2131	650.0469
4900.	0.8643	0.9297	1.0757	1.1770	1.2181	649.8157
5000.	0.8617	0.9283	1.0773	1.1810	1.2231	649.5845
5100.	0.8591	0.9269	1.0789	1.1850	1.2281	649.3532
5200.	0.8565	0.9254	1.0806	1.1891	1.2331	649.1218
5300.	0.8539	0.9240	1.0822	1.1931	1.2382	648.8904
5400.	0.8513	0.9226	1.0838	1.1972	1.2433	648.6588
5500.	0.8487	0.9212	1.0855	1.2012	1.2484	648.4272
5600.	0.8461	0.9198	1.0871	1.2053	1.2536	648.1955
5700.	0.8435	0.9184	1.0888	1.2094	1.2588	647.9637
5800.	0.8410	0.9170	1.0905	1.2135	1.2639	647.7318
5900.	0.8384	0.9156	1.0921	1.2177	1.2692	647.4999
6000.	0.8359	0.9143	1.0938	1.2218	1.2744	647.2678
6100.	0.8333	0.9129	1.0955	1.2260	1.2797	647.0357
6200.	0.8308	0.9115	1.0971	1.2302	1.2850	646.8035
6300.	0.8282	0.9101	1.0988	1.2344	1.2903	646.5712
6400.	0.8257	0.9087	1.1005	1.2387	1.2957	646.3388
6500.	0.8232	0.9073	1.1022	1.2429	1.3010	646.1064
6600.	0.8207	0.9059	1.1039	1.2472	1.3064	645.8738
6700.	0.8181	0.9045	1.1056	1.2514	1.3119	645.6412
6800.	0.8156	0.9031	1.1073	1.2557	1.3173	645.4085
6900.	0.8131	0.9017	1.1090	1.2601	1.3228	645.1757
7000.	0.8106	0.9004	1.1107	1.2644	1.3283	644.9428
7100.	0.8082	0.8990	1.1124	1.2687	1.3339	644.7099
7200.	0.8057	0.8976	1.1141	1.2731	1.3394	644.4768
7300.	0.8032	0.8962	1.1158	1.2775	1.3450	644.2437

$H_c$ (Feet)	$P_a$ ( $^{\circ}\text{Hg}$ )	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ ( $^{\circ}\text{K}$ )	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
7400.	22.140	0.7600	1.3158	273.50	16.538	0.9491	0.9742
7500.	22.133	0.7571	1.3208	273.30	16.532	0.9484	0.9739
7600.	22.126	0.7542	1.3259	273.10	16.526	0.9477	0.9735
7700.	22.119	0.7513	1.3310	272.90	16.520	0.9471	0.9732
7800.	22.112	0.7485	1.3360	272.71	16.514	0.9464	0.9728
7900.	22.105	0.7456	1.3412	272.51	16.508	0.9457	0.9725
8000.	22.098	0.7428	1.3463	272.31	16.502	0.9450	0.9721
8100.	22.091	0.7399	1.3515	272.11	16.496	0.9443	0.9718
8200.	22.084	0.7371	1.3566	271.91	16.490	0.9436	0.9714
8300.	21.971	0.7343	1.3619	271.72	16.484	0.9429	0.9710
8400.	21.887	0.7315	1.3671	271.52	16.478	0.9422	0.9707
8500.	21.803	0.7287	1.3723	271.32	16.472	0.9416	0.9703
8600.	21.720	0.7259	1.3776	271.12	16.466	0.9409	0.9700
8700.	21.636	0.7231	1.3829	270.92	16.460	0.9402	0.9696
8800.	21.553	0.7203	1.3882	270.73	16.454	0.9395	0.9693
8900.	21.470	0.7176	1.3936	270.53	16.448	0.9388	0.9689
9000.	21.384	0.7148	1.3990	270.33	16.442	0.9381	0.9686
9100.	21.300	0.7121	1.4044	270.13	16.436	0.9374	0.9682
9200.	21.224	0.7093	1.4098	269.93	16.430	0.9367	0.9679
9300.	21.142	0.7066	1.4153	269.73	16.424	0.9361	0.9675
9400.	21.060	0.7039	1.4207	269.54	16.418	0.9354	0.9671
9500.	20.979	0.7011	1.4262	269.34	16.412	0.9347	0.9668
9600.	20.893	0.6984	1.4318	269.14	16.406	0.9340	0.9664
9700.	20.817	0.6957	1.4373	268.94	16.399	0.9333	0.9661
9800.	20.737	0.6931	1.4429	268.74	16.393	0.9326	0.9657
9900.	20.657	0.6904	1.4485	268.55	16.387	0.9319	0.9654
10000.	20.577	0.6877	1.4541	268.35	16.381	0.9312	0.9650
10100.	20.497	0.6850	1.4598	268.15	16.375	0.9306	0.9647
10200.	20.418	0.6824	1.4655	267.95	16.369	0.9299	0.9643
10300.	20.334	0.6797	1.4712	267.75	16.363	0.9292	0.9639
10400.	20.259	0.6771	1.4769	267.56	16.357	0.9285	0.9636
10500.	20.181	0.6745	1.4827	267.36	16.351	0.9278	0.9632
10600.	20.102	0.6718	1.4885	267.16	16.345	0.9271	0.9629
10700.	20.024	0.6692	1.4943	266.96	16.339	0.9264	0.9625
10800.	19.946	0.6666	1.5001	266.76	16.333	0.9257	0.9622
10900.	19.868	0.6640	1.5060	266.56	16.327	0.9251	0.9618
11000.	19.791	0.6614	1.5119	266.37	16.321	0.9244	0.9614
11100.	19.713	0.6598	1.5178	266.17	16.315	0.9237	0.9611
11200.	19.636	0.6563	1.5238	265.97	16.309	0.9230	0.9607
11300.	19.560	0.6537	1.5297	265.77	16.303	0.9223	0.9604
11400.	19.483	0.6511	1.5357	265.57	16.296	0.9216	0.9600
11500.	19.407	0.6486	1.5418	265.38	16.290	0.9209	0.9597

$H_c$ (Feet)	$\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{\delta\sqrt{\theta}}$	$a$ (Knots)
7400.	0.8907	0.8946	1.1175	1.2819	1.3506	644.0105
7500.	0.8913	0.8934	1.1193	1.2863	1.3563	643.7772
7600.	0.8918	0.8921	1.1210	1.2904	1.3620	643.5438
7700.	0.8923	0.8907	1.1227	1.2952	1.3677	643.3103
7800.	0.8928	0.8893	1.1245	1.2997	1.3734	643.0764
7900.	0.8934	0.8874	1.1262	1.3042	1.3791	642.8431
8000.	0.8940	0.8866	1.1279	1.3088	1.3849	642.6094
8100.	0.8946	0.8852	1.1297	1.3133	1.3907	642.3756
8200.	0.8952	0.8838	1.1314	1.3178	1.3966	642.1417
8300.	0.8957	0.8825	1.1332	1.3224	1.4025	641.9077
8400.	0.8963	0.8811	1.1350	1.3270	1.4084	641.6737
8500.	0.8969	0.8797	1.1367	1.3316	1.4143	641.4395
8600.	0.8975	0.8784	1.1385	1.3363	1.4202	641.2053
8700.	0.8981	0.8770	1.1403	1.3409	1.4262	640.9709
8800.	0.8987	0.8756	1.1420	1.3455	1.4323	640.7365
8900.	0.8993	0.8743	1.1438	1.3503	1.4383	640.5021
9000.	0.8999	0.8729	1.1456	1.3550	1.4444	640.2675
9100.	0.9005	0.8715	1.1474	1.3597	1.4505	640.0328
9200.	0.9012	0.8702	1.1492	1.3645	1.4566	639.7981
9300.	0.9018	0.8688	1.1510	1.3693	1.4628	639.5632
9400.	0.9025	0.8675	1.1528	1.3741	1.4690	639.3283
9500.	0.9031	0.8661	1.1546	1.3789	1.4752	639.0933
9600.	0.9038	0.8648	1.1564	1.3837	1.4815	638.8582
9700.	0.9045	0.8634	1.1582	1.3886	1.4878	638.6230
9800.	0.9051	0.8620	1.1600	1.3934	1.4941	638.3877
9900.	0.9058	0.8607	1.1619	1.3983	1.5005	638.1524
10000.	0.9065	0.8593	1.1637	1.4032	1.5068	637.9169
10100.	0.9072	0.8580	1.1655	1.4082	1.5133	637.6814
10200.	0.9079	0.8566	1.1673	1.4131	1.5197	637.4458
10300.	0.9086	0.8553	1.1692	1.4181	1.5262	637.2101
10400.	0.9093	0.8540	1.1710	1.4231	1.5327	636.9743
10500.	0.9100	0.8526	1.1729	1.4281	1.5393	636.7384
10600.	0.9107	0.8513	1.1747	1.4332	1.5459	636.5025
10700.	0.9114	0.8499	1.1766	1.4383	1.5525	636.2664
10800.	0.9121	0.8486	1.1784	1.4433	1.5591	636.0303
10900.	0.9128	0.8472	1.1803	1.4485	1.5658	635.7940
11000.	0.9135	0.8459	1.1822	1.4536	1.5725	635.5577
11100.	0.9143	0.8446	1.1840	1.4587	1.5793	635.3213
11200.	0.9150	0.8432	1.1859	1.4639	1.5860	635.0848
11300.	0.9158	0.8419	1.1878	1.4691	1.5929	634.8483
11400.	0.9165	0.8406	1.1897	1.4743	1.5997	634.6116
11500.	0.9173	0.8392	1.1916	1.4796	1.6066	634.3748



$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ ("K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
11600.	19.331	0.6461	1.5479	265.18	16.284	0.9202	0.9593
11700.	19.255	0.6435	1.5539	264.98	16.278	0.9196	0.9589
11800.	19.180	0.6410	1.5601	264.78	16.272	0.9190	0.9586
11900.	19.104	0.6385	1.5662	264.58	16.266	0.9182	0.9582
12000.	19.029	0.6360	1.5724	264.39	16.260	0.9175	0.9579
12100.	18.954	0.6335	1.5786	264.19	16.254	0.9168	0.9575
12200.	18.880	0.6310	1.5848	263.99	16.248	0.9161	0.9571
12300.	18.805	0.6285	1.5911	263.79	16.242	0.9154	0.9568
12400.	18.731	0.6260	1.5974	263.59	16.236	0.9147	0.9564
12500.	18.657	0.6235	1.6037	263.40	16.229	0.9141	0.9561
12600.	18.584	0.6211	1.6101	263.20	16.223	0.9134	0.9557
12700.	18.510	0.6186	1.6165	263.00	16.217	0.9127	0.9553
12800.	18.437	0.6162	1.6229	262.80	16.211	0.9120	0.9550
12900.	18.364	0.6138	1.6293	262.60	16.205	0.9113	0.9546
13000.	18.292	0.6113	1.6358	262.40	16.199	0.9106	0.9543
13100.	18.219	0.6089	1.6423	262.21	16.193	0.9099	0.9539
13200.	18.147	0.6065	1.6488	262.01	16.187	0.9092	0.9535
13300.	18.075	0.6041	1.6554	261.81	16.181	0.9086	0.9532
13400.	18.003	0.6017	1.6620	261.61	16.174	0.9079	0.9528
13500.	17.931	0.5993	1.6686	261.41	16.168	0.9072	0.9525
13600.	17.860	0.5969	1.6753	261.22	16.162	0.9065	0.9521
13700.	17.789	0.5945	1.6820	261.02	16.156	0.9058	0.9517
13800.	17.718	0.5922	1.6887	260.82	16.150	0.9051	0.9514
13900.	17.648	0.5898	1.6955	260.62	16.144	0.9044	0.9510
14000.	17.577	0.5874	1.7023	260.42	16.138	0.9037	0.9507
14100.	17.507	0.5851	1.7091	260.23	16.131	0.9031	0.9503
14200.	17.437	0.5828	1.7160	260.03	16.125	0.9024	0.9499
14300.	17.367	0.5804	1.7228	259.83	16.119	0.9017	0.9496
14400.	17.298	0.5781	1.7298	259.63	16.113	0.9010	0.9492
14500.	17.229	0.5758	1.7367	259.43	16.107	0.9003	0.9488
14600.	17.160	0.5735	1.7437	259.23	16.101	0.8996	0.9485
14700.	17.091	0.5712	1.7507	259.04	16.095	0.8989	0.9481
14800.	17.022	0.5689	1.7578	258.84	16.088	0.8982	0.9478
14900.	16.954	0.5666	1.7649	258.64	16.082	0.8976	0.9474
15000.	16.886	0.5643	1.7720	258.44	16.076	0.8969	0.9470
15100.	16.818	0.5621	1.7792	258.24	16.070	0.8962	0.9467
15200.	16.750	0.5598	1.7863	258.05	16.064	0.8955	0.9463
15300.	16.682	0.5575	1.7936	257.85	16.058	0.8948	0.9459
15400.	16.615	0.5553	1.8008	257.65	16.051	0.8941	0.9456
15500.	16.548	0.5531	1.8081	257.45	16.045	0.8934	0.9452
15600.	16.481	0.5508	1.8155	257.25	16.039	0.8927	0.9449
15700.	16.415	0.5486	1.8228	257.06	16.033	0.8921	0.9445

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{g}$	$\frac{1}{\sqrt{g}}$	$\frac{\sqrt{g}}{\theta}$	$\frac{1}{h\sqrt{g}}$	$a$ (Knots)
11600.	0.7021	0.8379	1.1935	1.4848	1.6135	634.1380
11700.	0.6998	0.8366	1.1954	1.4901	1.6205	633.9011
11800.	0.6976	0.8352	1.1973	1.4954	1.6275	633.6640
11900.	0.6954	0.8339	1.1992	1.5008	1.6345	633.4269
12000.	0.6932	0.8326	1.2011	1.5061	1.6416	633.1897
12100.	0.6910	0.8312	1.2030	1.5115	1.6487	632.9524
12200.	0.6888	0.8299	1.2049	1.5169	1.6558	632.7150
12300.	0.6866	0.8286	1.2069	1.5223	1.6630	632.4776
12400.	0.6844	0.8273	1.2088	1.5278	1.6702	632.2400
12500.	0.6822	0.8259	1.2107	1.5333	1.6774	632.0024
12600.	0.6800	0.8246	1.2127	1.5388	1.6847	631.7647
12700.	0.6778	0.8233	1.2146	1.5443	1.6920	631.5268
12800.	0.6757	0.8220	1.2166	1.5498	1.6994	631.2889
12900.	0.6735	0.8207	1.2185	1.5554	1.7068	631.0509
13000.	0.6713	0.8193	1.2205	1.5610	1.7142	630.8128
13100.	0.6692	0.8180	1.2225	1.5666	1.7217	630.5746
13200.	0.6670	0.8167	1.2244	1.5722	1.7292	630.3364
13300.	0.6649	0.8154	1.2264	1.5779	1.7367	630.0980
13400.	0.6627	0.8141	1.2284	1.5836	1.7443	629.8596
13500.	0.6606	0.8128	1.2304	1.5893	1.7519	629.6210
13600.	0.6585	0.8115	1.2323	1.5951	1.7596	629.3824
13700.	0.6564	0.8102	1.2343	1.6008	1.7673	629.1437
13800.	0.6542	0.8088	1.2363	1.6066	1.7750	628.9048
13900.	0.6521	0.8075	1.2383	1.6124	1.7828	628.6659
14000.	0.6500	0.8062	1.2403	1.6183	1.7906	628.4269
14100.	0.6479	0.8049	1.2423	1.6241	1.7985	628.1879
14200.	0.6458	0.8036	1.2444	1.6300	1.8064	627.9487
14300.	0.6437	0.8023	1.2464	1.6360	1.8143	627.7094
14400.	0.6416	0.8010	1.2484	1.6419	1.8223	627.4700
14500.	0.6396	0.7997	1.2504	1.6479	1.8304	627.2306
14600.	0.6375	0.7984	1.2525	1.6539	1.8384	626.9910
14700.	0.6354	0.7971	1.2545	1.6599	1.8465	626.7514
14800.	0.6333	0.7958	1.2566	1.6660	1.8547	626.5117
14900.	0.6313	0.7945	1.2586	1.6720	1.8629	626.2719
15000.	0.6292	0.7932	1.2607	1.6781	1.8711	626.0320
15100.	0.6272	0.7919	1.2627	1.6843	1.8794	625.7920
15200.	0.6251	0.7907	1.2648	1.6904	1.8877	625.5519
15300.	0.6231	0.7894	1.2668	1.6966	1.8961	625.3117
15400.	0.6211	0.7881	1.2689	1.7028	1.9045	625.0714
15500.	0.6190	0.7868	1.2710	1.7091	1.9129	624.8310
15600.	0.6170	0.7855	1.2731	1.7153	1.9214	624.5906
15700.	0.6150	0.7842	1.2752	1.7216	1.9300	624.3500

$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ ('K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
15800.	15.344	0.5464	1.8302	256.86	16.027	0.8914	0.9441
15900.	15.332	0.5442	1.8377	256.66	16.021	0.8907	0.9438
16000.	15.321	0.5420	1.8451	256.46	16.014	0.8900	0.9434
16100.	15.310	0.5399	1.8527	256.26	16.008	0.8893	0.9430
16200.	15.299	0.5377	1.8602	256.06	16.002	0.8886	0.9427
16300.	15.288	0.5354	1.8678	255.87	15.996	0.8879	0.9423
16400.	15.277	0.5332	1.8754	255.67	15.990	0.8872	0.9419
16500.	15.266	0.5311	1.8831	255.47	15.983	0.8866	0.9416
16600.	15.255	0.5289	1.8908	255.27	15.977	0.8859	0.9412
16700.	15.244	0.5267	1.8985	255.07	15.971	0.8852	0.9408
16800.	15.233	0.5246	1.9063	254.88	15.965	0.8845	0.9405
16900.	15.222	0.5224	1.9141	254.68	15.959	0.8838	0.9401
17000.	15.211	0.5203	1.9219	254.48	15.952	0.8831	0.9397
17100.	15.200	0.5182	1.9298	254.28	15.946	0.8824	0.9394
17200.	15.189	0.5161	1.9377	254.08	15.940	0.8817	0.9390
17300.	15.178	0.5140	1.9457	253.89	15.934	0.8811	0.9386
17400.	15.167	0.5119	1.9537	253.69	15.928	0.8804	0.9383
17500.	15.156	0.5098	1.9617	253.49	15.921	0.8797	0.9379
17600.	15.145	0.5077	1.9698	253.29	15.915	0.8790	0.9375
17700.	15.134	0.5056	1.9779	253.09	15.909	0.8783	0.9372
17800.	15.123	0.5035	1.9861	252.89	15.903	0.8776	0.9368
17900.	15.112	0.5014	1.9943	252.70	15.896	0.8769	0.9364
18000.	15.101	0.4993	2.0025	252.50	15.890	0.8762	0.9361
18100.	14.890	0.4973	2.0108	252.30	15.884	0.8756	0.9357
18200.	14.879	0.4953	2.0191	252.10	15.878	0.8749	0.9353
18300.	14.868	0.4932	2.0275	251.90	15.871	0.8742	0.9350
18400.	14.857	0.4912	2.0359	251.71	15.865	0.8735	0.9346
18500.	14.846	0.4892	2.0443	251.51	15.859	0.8728	0.9342
18600.	14.835	0.4871	2.0528	251.31	15.853	0.8721	0.9339
18700.	14.824	0.4851	2.0613	251.11	15.846	0.8714	0.9335
18800.	14.813	0.4831	2.0699	250.91	15.840	0.8707	0.9331
18900.	14.802	0.4811	2.0785	250.72	15.834	0.8701	0.9328
19000.	14.791	0.4791	2.0872	250.52	15.828	0.8694	0.9324
19100.	14.780	0.4771	2.0959	250.32	15.821	0.8687	0.9320
19200.	14.769	0.4751	2.1046	250.12	15.815	0.8680	0.9317
19300.	14.758	0.4732	2.1134	249.92	15.809	0.8673	0.9313
19400.	14.747	0.4712	2.1222	249.72	15.803	0.8666	0.9309
19500.	14.736	0.4692	2.1311	249.53	15.796	0.8659	0.9306
19600.	13.982	0.4673	2.1400	249.33	15.790	0.8652	0.9302
19700.	13.971	0.4653	2.1490	249.13	15.784	0.8646	0.9298
19800.	13.960	0.4634	2.1580	248.93	15.778	0.8639	0.9294
19900.	13.949	0.4615	2.1670	248.73	15.771	0.8632	0.9291

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{A\sqrt{\theta}}$	$a$ (Knots)
15800.	0.6130	0.7823	1.2773	1.7280	1.9385	624.1094
15900.	0.6110	0.7816	1.2794	1.7343	1.9472	623.8686
16000.	0.6090	0.7804	1.2815	1.7407	1.9559	623.6278
16100.	0.6070	0.7791	1.2836	1.7471	1.9646	623.3869
16200.	0.6050	0.7778	1.2857	1.7535	1.9733	623.1458
16300.	0.6030	0.7765	1.2878	1.7600	1.9822	622.9047
16400.	0.6010	0.7752	1.2899	1.7665	1.9910	622.6635
16500.	0.5990	0.7740	1.2921	1.7730	1.9999	622.4222
16600.	0.5970	0.7727	1.2942	1.7796	2.0089	622.1808
16700.	0.5951	0.7714	1.2963	1.7862	2.0179	621.9393
16800.	0.5931	0.7701	1.2985	1.7928	2.0269	621.6977
16900.	0.5911	0.7689	1.3006	1.7994	2.0350	621.4561
17000.	0.5892	0.7676	1.3028	1.8061	2.0451	621.2143
17100.	0.5872	0.7663	1.3050	1.8128	2.0543	620.9724
17200.	0.5853	0.7650	1.3071	1.8195	2.0636	620.7305
17300.	0.5833	0.7638	1.3093	1.8263	2.0729	620.4884
17400.	0.5814	0.7625	1.3115	1.8331	2.0822	620.2463
17500.	0.5795	0.7612	1.3137	1.8399	2.0916	620.0040
17600.	0.5776	0.7600	1.3158	1.8468	2.1010	619.7617
17700.	0.5756	0.7587	1.3180	1.8537	2.1105	619.5193
17800.	0.5737	0.7574	1.3202	1.8606	2.1200	619.2767
17900.	0.5718	0.7562	1.3224	1.8675	2.1296	619.0341
18000.	0.5699	0.7549	1.3246	1.8745	2.1393	618.7914
18100.	0.5680	0.7537	1.3269	1.8815	2.1489	618.5486
18200.	0.5661	0.7524	1.3291	1.8886	2.1597	618.3057
18300.	0.5642	0.7511	1.3313	1.8956	2.1695	618.0627
18400.	0.5623	0.7499	1.3335	1.9027	2.1793	617.8196
18500.	0.5604	0.7486	1.3358	1.9097	2.1892	617.5764
18600.	0.5586	0.7474	1.3380	1.9171	2.1992	617.3331
18700.	0.5567	0.7461	1.3403	1.9243	2.2092	617.0897
18800.	0.5548	0.7449	1.3425	1.9315	2.2192	616.8462
18900.	0.5530	0.7436	1.3448	1.9398	2.2293	616.6027
19000.	0.5511	0.7424	1.3470	1.9461	2.2395	616.3590
19100.	0.5493	0.7411	1.3493	1.9534	2.2497	616.1152
19200.	0.5474	0.7399	1.3516	1.9608	2.2590	615.8714
19300.	0.5456	0.7386	1.3539	1.9682	2.2693	615.6274
19400.	0.5437	0.7374	1.3562	1.9756	2.2797	615.3833
19500.	0.5419	0.7361	1.3584	1.9831	2.2901	615.1392
19600.	0.5401	0.7349	1.3607	1.9906	2.3006	614.8949
19700.	0.5382	0.7337	1.3630	1.9981	2.3112	614.6506
19800.	0.5364	0.7324	1.3654	2.0057	2.3218	614.4061
19900.	0.5346	0.7312	1.3677	2.0133	2.3324	614.1616

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
20000.	13.750	0.4595	2.1761	248.54	15.765	0.8614	0.9287
20100.	13.692	0.4576	2.1852	248.34	15.759	0.8614	0.9283
20200.	13.635	0.4557	2.1944	248.14	15.752	0.8611	0.9280
20300.	13.578	0.4538	2.2037	247.94	15.746	0.8609	0.9276
20400.	13.521	0.4519	2.2129	247.74	15.740	0.8597	0.9272
20500.	13.464	0.4500	2.2223	247.55	15.734	0.8591	0.9269
20600.	13.409	0.4481	2.2316	247.35	15.727	0.8584	0.9265
20700.	13.351	0.4462	2.2411	247.15	15.721	0.8577	0.9261
20800.	13.295	0.4443	2.2505	246.95	15.715	0.8570	0.9257
20900.	13.239	0.4425	2.2600	246.75	15.708	0.8563	0.9254
21000.	13.183	0.4406	2.2695	246.55	15.702	0.8556	0.9250
21100.	13.128	0.4387	2.2792	246.36	15.696	0.8549	0.9246
21200.	13.072	0.4369	2.2889	246.16	15.689	0.8542	0.9243
21300.	13.017	0.4351	2.2986	245.96	15.683	0.8536	0.9239
21400.	12.962	0.4332	2.3083	245.76	15.677	0.8529	0.9235
21500.	12.907	0.4314	2.3181	245.56	15.670	0.8522	0.9231
21600.	12.853	0.4296	2.3280	245.37	15.664	0.8515	0.9228
21700.	12.798	0.4277	2.3379	245.17	15.658	0.8508	0.9224
21800.	12.744	0.4259	2.3479	244.97	15.652	0.8501	0.9220
21900.	12.690	0.4241	2.3579	244.77	15.645	0.8494	0.9216
22000.	12.636	0.4223	2.3679	244.57	15.639	0.8487	0.9213
22100.	12.582	0.4205	2.3780	244.38	15.633	0.8481	0.9209
22200.	12.529	0.4187	2.3882	244.18	15.626	0.8474	0.9205
22300.	12.476	0.4169	2.3984	243.98	15.620	0.8467	0.9202
22400.	12.422	0.4152	2.4087	243.78	15.613	0.8460	0.9198
22500.	12.369	0.4134	2.4190	243.59	15.607	0.8453	0.9194
22600.	12.317	0.4116	2.4293	243.38	15.601	0.8446	0.9190
22700.	12.264	0.4099	2.4398	243.19	15.594	0.8439	0.9187
22800.	12.212	0.4081	2.4502	242.99	15.588	0.8432	0.9183
22900.	12.159	0.4064	2.4608	242.79	15.582	0.8426	0.9179
23000.	12.107	0.4046	2.4714	242.59	15.575	0.8419	0.9175
23100.	12.055	0.4029	2.4820	242.39	15.569	0.8412	0.9172
23200.	12.004	0.4012	2.4927	242.20	15.563	0.8405	0.9168
23300.	11.952	0.3995	2.5034	242.00	15.556	0.8398	0.9164
23400.	11.901	0.3977	2.5142	241.80	15.550	0.8391	0.9160
23500.	11.850	0.3960	2.5251	241.60	15.544	0.8384	0.9157
23600.	11.799	0.3943	2.5360	241.40	15.537	0.8377	0.9153
23700.	11.748	0.3926	2.5470	241.21	15.531	0.8371	0.9149
23800.	11.697	0.3909	2.5580	241.01	15.524	0.8364	0.9145
23900.	11.647	0.3892	2.5691	240.81	15.518	0.8357	0.9142
24000.	11.596	0.3876	2.5802	240.61	15.512	0.8350	0.9138
24100.	11.546	0.3859	2.5914	240.41	15.505	0.8343	0.9134

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
20000.	0.5325	0.7299	1.3700	2.0210	2.3632	613.9169
20100.	0.5319	0.7297	1.3723	2.0285	2.3539	613.6722
20200.	0.5312	0.7275	1.3747	2.0364	2.3443	613.4274
20300.	0.5304	0.7252	1.3770	2.0441	2.3357	613.1824
20400.	0.5296	0.7250	1.3793	2.0517	2.3266	612.9374
20500.	0.5288	0.7238	1.3817	2.0597	2.3177	612.6923
20600.	0.5280	0.7225	1.3840	2.0676	2.3087	612.4470
20700.	0.5273	0.7213	1.3864	2.0755	2.4100	612.2017
20800.	0.5149	0.7201	1.3888	2.0834	2.4311	611.9563
20900.	0.5167	0.7143	1.3911	2.0914	2.4423	611.7107
21000.	0.5150	0.7176	1.3935	2.0994	2.4536	611.4651
21100.	0.5132	0.7154	1.3959	2.1074	2.4650	611.2194
21200.	0.5114	0.7152	1.3983	2.1155	2.4765	610.9736
21300.	0.5077	0.7139	1.4007	2.1236	2.4880	610.7277
21400.	0.5079	0.7127	1.4031	2.1318	2.4995	610.4816
21500.	0.5062	0.7115	1.4055	2.1400	2.5112	610.2355
21600.	0.5045	0.7103	1.4079	2.1482	2.5229	609.9893
21700.	0.5027	0.7090	1.4104	2.1565	2.5346	609.7430
21800.	0.5010	0.7078	1.4128	2.1648	2.5464	609.4966
21900.	0.4993	0.7066	1.4152	2.1731	2.5583	609.2501
22000.	0.4975	0.7054	1.4177	2.1815	2.5703	609.0034
22100.	0.4958	0.7042	1.4201	2.1899	2.5823	608.7567
22200.	0.4942	0.7030	1.4226	2.1984	2.5944	608.5099
22300.	0.4924	0.7017	1.4250	2.2069	2.6065	608.2630
22400.	0.4907	0.7005	1.4275	2.2154	2.6187	608.0160
22500.	0.4891	0.6993	1.4300	2.2240	2.6310	607.7689
22600.	0.4874	0.6981	1.4324	2.2326	2.6434	607.5217
22700.	0.4857	0.6969	1.4349	2.2413	2.6558	607.2743
22800.	0.4840	0.6957	1.4374	2.2500	2.6683	607.0269
22900.	0.4823	0.6945	1.4399	2.2588	2.6808	606.7794
23000.	0.4806	0.6933	1.4424	2.2675	2.6935	606.5318
23100.	0.4790	0.6921	1.4449	2.2764	2.7062	606.2841
23200.	0.4773	0.6909	1.4474	2.2852	2.7189	606.0362
23300.	0.4757	0.6897	1.4500	2.2942	2.7318	605.7883
23400.	0.4740	0.6885	1.4525	2.3031	2.7447	605.5403
23500.	0.4723	0.6873	1.4550	2.3121	2.7577	605.2922
23600.	0.4707	0.6861	1.4576	2.3211	2.7707	605.0439
23700.	0.4691	0.6849	1.4601	2.3302	2.7838	604.7956
23800.	0.4674	0.6837	1.4627	2.3394	2.7970	604.5472
23900.	0.4658	0.6825	1.4652	2.3485	2.8103	604.2986
24000.	0.4642	0.6813	1.4678	2.3577	2.8237	604.0500
24100.	0.4625	0.6801	1.4704	2.3670	2.8371	603.8013

$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
24200.	11.436	0.3842	2.6027	240.21	15.499	0.8336	0.9130
24300.	11.447	0.3826	2.6140	240.02	15.492	0.8329	0.9126
24400.	11.397	0.3809	2.6253	239.82	15.486	0.8322	0.9123
24500.	11.348	0.3793	2.6368	239.62	15.480	0.8316	0.9119
24600.	11.298	0.3776	2.6483	239.42	15.473	0.8309	0.9115
24700.	11.249	0.3760	2.6598	239.22	15.467	0.8302	0.9111
24800.	11.201	0.3743	2.6714	239.03	15.460	0.8295	0.9108
24900.	11.152	0.3727	2.6831	238.83	15.454	0.8288	0.9104
25000.	11.103	0.3711	2.6948	238.63	15.448	0.8281	0.9100
25100.	11.055	0.3695	2.7066	238.43	15.441	0.8274	0.9096
25200.	11.007	0.3679	2.7184	238.23	15.435	0.8267	0.9093
25300.	10.959	0.3663	2.7304	238.04	15.428	0.8261	0.9089
25400.	10.911	0.3647	2.7423	237.84	15.422	0.8254	0.9085
25500.	10.863	0.3631	2.7544	237.64	15.416	0.8247	0.9081
25600.	10.816	0.3615	2.7665	237.44	15.409	0.8240	0.9077
25700.	10.768	0.3599	2.7786	237.24	15.403	0.8233	0.9074
25800.	10.721	0.3583	2.7909	237.05	15.396	0.8226	0.9070
25900.	10.674	0.3567	2.8032	236.85	15.390	0.8219	0.9066
26000.	10.627	0.3552	2.8155	236.65	15.383	0.8212	0.9062
26100.	10.581	0.3536	2.8279	236.45	15.377	0.8206	0.9058
26200.	10.534	0.3521	2.8404	236.25	15.371	0.8199	0.9055
26300.	10.488	0.3505	2.8530	236.05	15.364	0.8192	0.9051
26400.	10.442	0.3490	2.8656	235.86	15.358	0.8185	0.9047
26500.	10.396	0.3474	2.8783	235.66	15.351	0.8178	0.9043
26600.	10.350	0.3459	2.8910	235.46	15.345	0.8171	0.9039
26700.	10.304	0.3444	2.9039	235.26	15.338	0.8164	0.9036
26800.	10.258	0.3428	2.9167	235.06	15.332	0.8157	0.9032
26900.	10.213	0.3413	2.9297	234.87	15.325	0.8151	0.9028
27000.	10.168	0.3398	2.9427	234.67	15.319	0.8144	0.9024
27100.	10.123	0.3383	2.9558	234.47	15.312	0.8137	0.9020
27200.	10.078	0.3368	2.9690	234.27	15.306	0.8130	0.9017
27300.	10.033	0.3353	2.9822	234.07	15.299	0.8123	0.9013
27400.	9.989	0.3338	2.9955	233.88	15.293	0.8116	0.9009
27500.	9.944	0.3323	3.0089	233.68	15.286	0.8109	0.9005
27600.	9.900	0.3309	3.0223	233.48	15.280	0.8102	0.9001
27700.	9.856	0.3294	3.0359	233.28	15.274	0.8096	0.8998
27800.	9.812	0.3279	3.0494	233.08	15.267	0.8089	0.8994
27900.	9.768	0.3265	3.0631	232.88	15.261	0.8082	0.8990
28000.	9.725	0.3250	3.0768	232.69	15.254	0.8075	0.8986
28100.	9.681	0.3236	3.0906	232.49	15.248	0.8068	0.8982
28200.	9.638	0.3221	3.1045	232.29	15.241	0.8061	0.8978
28300.	9.595	0.3207	3.1185	232.09	15.235	0.8054	0.8975

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
24200.	0.4609	0.6789	1.4730	2.3763	2.8506	603.5524
24300.	0.4593	0.6777	1.4755	2.3856	2.8641	603.3035
24400.	0.4577	0.6765	1.4781	2.3950	2.8778	603.0544
24500.	0.4561	0.6753	1.4807	2.4045	2.8915	602.8053
24600.	0.4545	0.6741	1.4834	2.4139	2.9053	602.5560
24700.	0.4529	0.6730	1.4860	2.4235	2.9192	602.3067
24800.	0.4513	0.6718	1.4886	2.4330	2.9332	602.0572
24900.	0.4497	0.6706	1.4912	2.4426	2.9472	601.8076
25000.	0.4481	0.6694	1.4939	2.4523	2.9613	601.5580
25100.	0.4465	0.6682	1.4965	2.4620	2.9755	601.3082
25200.	0.4449	0.6670	1.4991	2.4718	2.9898	601.0583
25300.	0.4434	0.6659	1.5018	2.4816	3.0041	600.8083
25400.	0.4418	0.6647	1.5045	2.4914	3.0185	600.5583
25500.	0.4402	0.6635	1.5071	2.5013	3.0331	600.3081
25600.	0.4387	0.6623	1.5098	2.5112	3.0477	600.0578
25700.	0.4371	0.6612	1.5125	2.5212	3.0623	599.8074
25800.	0.4356	0.6600	1.5152	2.5313	3.0771	599.5569
25900.	0.4340	0.6588	1.5179	2.5414	3.0919	599.3063
26000.	0.4325	0.6576	1.5206	2.5515	3.1069	599.0556
26100.	0.4309	0.6565	1.5233	2.5617	3.1219	598.8048
26200.	0.4294	0.6553	1.5260	2.5719	3.1370	598.5538
26300.	0.4278	0.6541	1.5288	2.5822	3.1522	598.3028
26400.	0.4264	0.6530	1.5315	2.5925	3.1674	598.0517
26500.	0.4248	0.6518	1.5342	2.6029	3.1828	597.8005
26600.	0.4233	0.6506	1.5370	2.6133	3.1983	597.5491
26700.	0.4218	0.6495	1.5397	2.6239	3.2138	597.2977
26800.	0.4204	0.6483	1.5425	2.6344	3.2294	597.0461
26900.	0.4188	0.6471	1.5453	2.6449	3.2451	596.7944
27000.	0.4173	0.6460	1.5480	2.6556	3.2609	596.5427
27100.	0.4158	0.6448	1.5508	2.6663	3.2768	596.2908
27200.	0.4143	0.6437	1.5536	2.6770	3.2928	596.0388
27300.	0.4128	0.6425	1.5564	2.6878	3.3089	595.7868
27400.	0.4113	0.6413	1.5592	2.6987	3.3250	595.5346
27500.	0.4098	0.6402	1.5620	2.7096	3.3413	595.2823
27600.	0.4084	0.6390	1.5649	2.7205	3.3577	595.0299
27700.	0.4069	0.6379	1.5677	2.7315	3.3741	594.7774
27800.	0.4054	0.6367	1.5705	2.7426	3.3906	594.5247
27900.	0.4040	0.6356	1.5734	2.7537	3.4073	594.2720
28000.	0.4025	0.6344	1.5762	2.7649	3.4240	594.0192
28100.	0.4010	0.6333	1.5791	2.7761	3.4408	593.7662
28200.	0.3995	0.6321	1.5820	2.7874	3.4578	593.5132
28300.	0.3981	0.6310	1.5848	2.7987	3.4748	593.2600



$H_c$ (Feet)	$P_a$ ("Hg)	$\theta$ $P_a/P_{aSL}$	$\frac{1}{\theta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
28400.	9.552	0.3192	3.1325	231.89	15.228	0.8047	0.8971
28500.	9.509	0.3178	3.1466	231.70	15.222	0.8041	0.8967
28600.	9.466	0.3164	3.1608	231.50	15.215	0.8034	0.8963
28700.	9.424	0.3150	3.1750	231.30	15.209	0.8027	0.8959
28800.	9.382	0.3135	3.1894	231.10	15.202	0.8020	0.8955
28900.	9.339	0.3121	3.2038	230.90	15.196	0.8013	0.8952
29000.	9.297	0.3107	3.2183	230.71	15.189	0.8006	0.8948
29100.	9.255	0.3093	3.2328	230.51	15.182	0.7999	0.8944
29200.	9.214	0.3079	3.2475	230.31	15.176	0.7992	0.8940
29300.	9.172	0.3065	3.2622	230.11	15.169	0.7986	0.8936
29400.	9.131	0.3052	3.2770	229.91	15.163	0.7979	0.8932
29500.	9.089	0.3038	3.2919	229.71	15.156	0.7972	0.8928
29600.	9.048	0.3024	3.3069	229.52	15.150	0.7965	0.8925
29700.	9.007	0.3010	3.3219	229.32	15.143	0.7958	0.8921
29800.	8.966	0.2997	3.3370	229.12	15.137	0.7951	0.8917
29900.	8.926	0.2983	3.3522	228.92	15.130	0.7944	0.8913
30000.	8.885	0.2970	3.3675	228.72	15.124	0.7937	0.8909
30100.	8.845	0.2956	3.3829	228.53	15.117	0.7931	0.8905
30200.	8.805	0.2943	3.3984	228.33	15.111	0.7924	0.8901
30300.	8.765	0.2929	3.4139	228.13	15.104	0.7917	0.8898
30400.	8.725	0.2916	3.4295	227.93	15.097	0.7910	0.8894
30500.	8.685	0.2903	3.4452	227.73	15.091	0.7903	0.8890
30600.	8.645	0.2889	3.4610	227.54	15.084	0.7896	0.8886
30700.	8.606	0.2876	3.4769	227.34	15.078	0.7889	0.8882
30800.	8.566	0.2863	3.4929	227.14	15.071	0.7882	0.8878
30900.	8.527	0.2850	3.5089	226.94	15.065	0.7876	0.8874
31000.	8.488	0.2837	3.5251	226.74	15.058	0.7869	0.8871
31100.	8.449	0.2824	3.5413	226.54	15.051	0.7862	0.8867
31200.	8.410	0.2811	3.5577	226.35	15.045	0.7855	0.8863
31300.	8.372	0.2798	3.5741	226.15	15.038	0.7848	0.8859
31400.	8.333	0.2785	3.5906	225.95	15.032	0.7841	0.8855
31500.	8.295	0.2772	3.6072	225.75	15.025	0.7834	0.8851
31600.	8.257	0.2759	3.6238	225.55	15.018	0.7827	0.8847
31700.	8.219	0.2747	3.6406	225.36	15.012	0.7821	0.8843
31800.	8.181	0.2734	3.6575	225.16	15.005	0.7814	0.8839
31900.	8.143	0.2721	3.6745	224.96	14.999	0.7807	0.8836
32000.	8.105	0.2709	3.6915	224.76	14.992	0.7800	0.8832
32100.	8.068	0.2696	3.7087	224.56	14.985	0.7793	0.8828
32200.	8.031	0.2684	3.7259	224.37	14.979	0.7786	0.8824
32300.	7.993	0.2671	3.7432	224.17	14.972	0.7779	0.8820
32400.	7.956	0.2659	3.7607	223.97	14.966	0.7772	0.8816
32500.	7.919	0.2647	3.7782	223.77	14.959	0.7766	0.8812

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{K\sqrt{\theta}}$	$a$ (Knots)
28400.	0.3967	0.6298	1.5877	2.8101	3.4919	593.0068
28500.	0.3953	0.6287	1.5906	2.8215	3.5091	592.7534
28600.	0.3939	0.6275	1.5935	2.8330	3.5265	592.4999
28700.	0.3924	0.6264	1.5964	2.8446	3.5439	592.2463
28800.	0.3910	0.6253	1.5993	2.8562	3.5614	591.9926
28900.	0.3895	0.6241	1.6022	2.8679	3.5790	591.7388
29000.	0.3881	0.6230	1.6052	2.8796	3.5968	591.4849
29100.	0.3867	0.6218	1.6081	2.8914	3.6146	591.2309
29200.	0.3853	0.6207	1.6111	2.9033	3.6325	590.9767
29300.	0.3839	0.6196	1.6140	2.9152	3.6506	590.7225
29400.	0.3825	0.6184	1.6170	2.9271	3.6697	590.4681
29500.	0.3811	0.6173	1.6199	2.9392	3.6870	590.2137
29600.	0.3797	0.6162	1.6229	2.9513	3.7053	589.9591
29700.	0.3783	0.6150	1.6259	2.9634	3.7238	589.7044
29800.	0.3769	0.6139	1.6289	2.9756	3.7424	589.4496
29900.	0.3755	0.6128	1.6319	2.9879	3.7610	589.1947
30000.	0.3741	0.6117	1.6349	3.0002	3.7798	588.9397
30100.	0.3727	0.6105	1.6379	3.0126	3.7987	588.6846
30200.	0.3714	0.6094	1.6410	3.0250	3.8177	588.4293
30300.	0.3700	0.6083	1.6440	3.0376	3.8369	588.1740
30400.	0.3686	0.6072	1.6470	3.0501	3.8561	587.9185
30500.	0.3673	0.6060	1.6501	3.0629	3.8755	587.6630
30600.	0.3659	0.6049	1.6531	3.0755	3.8947	587.4073
30700.	0.3646	0.6038	1.6562	3.0883	3.9145	587.1515
30800.	0.3632	0.6027	1.6593	3.1011	3.9342	586.8956
30900.	0.3619	0.6016	1.6624	3.1140	3.9540	586.6396
31000.	0.3605	0.6004	1.6655	3.1269	3.9739	586.3835
31100.	0.3592	0.5993	1.6686	3.1400	3.9940	586.1272
31200.	0.3578	0.5982	1.6717	3.1531	4.0141	585.8709
31300.	0.3565	0.5971	1.6748	3.1662	4.0344	585.6144
31400.	0.3552	0.5960	1.6779	3.1795	4.0548	585.3578
31500.	0.3539	0.5949	1.6811	3.1927	4.0754	585.1012
31600.	0.3525	0.5938	1.6842	3.2061	4.0960	584.8444
31700.	0.3512	0.5926	1.6873	3.2195	4.1168	584.5874
31800.	0.3499	0.5915	1.6905	3.2330	4.1377	584.3304
31900.	0.3486	0.5904	1.6937	3.2466	4.1587	584.0733
32000.	0.3473	0.5893	1.6969	3.2602	4.1798	583.8160
32100.	0.3460	0.5882	1.7000	3.2739	4.2011	583.5587
32200.	0.3447	0.5871	1.7032	3.2877	4.2225	583.3012
32300.	0.3434	0.5860	1.7064	3.3015	4.2440	583.0436
32400.	0.3421	0.5849	1.7097	3.3155	4.2657	582.7859
32500.	0.3409	0.5838	1.7129	3.3294	4.2875	582.5281

$H_c$ (Feet)	$P_a$ ("Hg)	$\theta$ $P_a/P_{aSL}$	$\frac{1}{\theta}$	$T_a$ ("K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
32600.	7.883	0.2634	3.7959	223.57	14.952	0.7759	0.8808
32700.	7.846	0.2622	3.8136	223.37	14.946	0.7752	0.8804
32800.	7.809	0.2610	3.8314	223.18	14.939	0.7745	0.8801
32900.	7.773	0.2598	3.8493	222.98	14.932	0.7738	0.8797
33000.	7.737	0.2586	3.8674	222.78	14.926	0.7731	0.8793
33100.	7.701	0.2574	3.8855	222.58	14.919	0.7724	0.8789
33200.	7.665	0.2562	3.9037	222.38	14.913	0.7717	0.8785
33300.	7.629	0.2550	3.9221	222.19	14.906	0.7711	0.8781
33400.	7.593	0.2538	3.9405	221.99	14.899	0.7704	0.8777
33500.	7.558	0.2526	3.9590	221.79	14.893	0.7697	0.8773
33600.	7.522	0.2514	3.9777	221.59	14.886	0.7690	0.8769
33700.	7.487	0.2502	3.9964	221.39	14.879	0.7683	0.8765
33800.	7.452	0.2491	4.0153	221.20	14.873	0.7676	0.8761
33900.	7.417	0.2479	4.0342	221.00	14.866	0.7669	0.8757
34000.	7.382	0.2467	4.0533	220.80	14.859	0.7662	0.8754
34100.	7.347	0.2455	4.0724	220.60	14.853	0.7656	0.8750
34200.	7.313	0.2444	4.0917	220.40	14.846	0.7649	0.8746
34300.	7.278	0.2432	4.1111	220.20	14.839	0.7642	0.8742
34400.	7.244	0.2421	4.1306	220.01	14.833	0.7635	0.8738
34500.	7.210	0.2410	4.1502	219.81	14.826	0.7628	0.8734
34600.	7.175	0.2398	4.1699	219.61	14.819	0.7621	0.8730
34700.	7.142	0.2387	4.1898	219.41	14.813	0.7614	0.8726
34800.	7.108	0.2375	4.2097	219.21	14.806	0.7607	0.8722
34900.	7.074	0.2364	4.2298	219.02	14.799	0.7601	0.8718
35000.	7.040	0.2353	4.2499	218.82	14.792	0.7594	0.8714
35100.	7.007	0.2342	4.2702	218.62	14.786	0.7587	0.8710
35200.	6.974	0.2331	4.2906	218.42	14.779	0.7580	0.8706
35300.	6.940	0.2320	4.3111	218.22	14.772	0.7573	0.8702
35400.	6.907	0.2309	4.3318	218.03	14.766	0.7566	0.8698
35500.	6.874	0.2298	4.3525	217.83	14.759	0.7559	0.8694
35600.	6.842	0.2287	4.3734	217.63	14.752	0.7552	0.8690
35700.	6.809	0.2276	4.3944	217.43	14.746	0.7546	0.8686
35800.	6.776	0.2265	4.4155	217.23	14.739	0.7539	0.8683
35900.	6.744	0.2254	4.4367	217.03	14.732	0.7532	0.8679
36000.	6.712	0.2243	4.4580	216.84	14.725	0.7525	0.8675
36100.	6.678	0.2232	4.4804	216.66	14.719	0.7519	0.8671
36200.	6.646	0.2221	4.5020	216.66	14.719	0.7519	0.8671
36300.	6.614	0.2211	4.5237	216.66	14.719	0.7519	0.8671
36400.	6.583	0.2200	4.5455	216.66	14.719	0.7519	0.8671
36500.	6.551	0.2189	4.5674	216.66	14.719	0.7519	0.8671
36600.	6.520	0.2179	4.5894	216.66	14.719	0.7519	0.8671
36700.	6.488	0.2168	4.6115	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $p/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\delta}$	$\frac{1}{\delta\sqrt{\sigma}}$	$a$ (Knots)
32600.	0.3396	0.5827	1.7161	3.3435	4.3094	582.2701
32700.	0.3393	0.5816	1.7194	3.3576	4.3314	582.0121
32800.	0.3390	0.5805	1.7226	3.3718	4.3536	581.7539
32900.	0.3387	0.5794	1.7259	3.3861	4.3759	581.4957
33000.	0.3385	0.5783	1.7291	3.4005	4.3984	581.2373
33100.	0.3382	0.5772	1.7324	3.4147	4.4210	580.9788
33200.	0.3379	0.5761	1.7357	3.4294	4.4437	580.7201
33300.	0.3377	0.5750	1.7390	3.4437	4.4665	580.4614
33400.	0.3294	0.5740	1.7423	3.4596	4.4895	580.2026
33500.	0.3282	0.5729	1.7456	3.4733	4.5127	579.9436
33600.	0.3267	0.5718	1.7489	3.4881	4.5359	579.6845
33700.	0.3257	0.5707	1.7523	3.5030	4.5594	579.4253
33800.	0.3244	0.5696	1.7556	3.5179	4.5829	579.1660
33900.	0.3232	0.5685	1.7590	3.5329	4.6066	578.9066
34000.	0.3220	0.5674	1.7623	3.5480	4.6305	578.6470
34100.	0.3208	0.5664	1.7657	3.5632	4.6545	578.3873
34200.	0.3195	0.5653	1.7691	3.5785	4.6786	578.1276
34300.	0.3183	0.5642	1.7725	3.5938	4.7029	577.8677
34400.	0.3171	0.5631	1.7759	3.6092	4.7273	577.6077
34500.	0.3159	0.5620	1.7793	3.6247	4.7519	577.3475
34600.	0.3147	0.5610	1.7827	3.6403	4.7766	577.0873
34700.	0.3135	0.5599	1.7861	3.6560	4.8015	576.8269
34800.	0.3123	0.5588	1.7895	3.6717	4.8265	576.5664
34900.	0.3111	0.5577	1.7930	3.6875	4.8517	576.3058
35000.	0.3099	0.5567	1.7964	3.7034	4.8770	576.0451
35100.	0.3087	0.5556	1.7999	3.7194	4.9025	575.7843
35200.	0.3075	0.5545	1.8034	3.7355	4.9282	575.5233
35300.	0.3063	0.5534	1.8069	3.7517	4.9540	575.2622
35400.	0.3051	0.5524	1.8104	3.7679	4.9800	575.0010
35500.	0.3039	0.5513	1.8139	3.7842	5.0061	574.7397
35600.	0.3028	0.5502	1.8174	3.8007	5.0324	574.4783
35700.	0.3016	0.5492	1.8209	3.8171	5.0588	574.2168
35800.	0.3004	0.5481	1.8245	3.8337	5.0855	573.9551
35900.	0.2993	0.5470	1.8280	3.8504	5.1122	573.6933
36000.	0.2981	0.5460	1.8316	3.8672	5.1392	573.4314
36100.	0.2969	0.5449	1.8352	3.8850	5.1671	573.1776
36200.	0.2955	0.5436	1.8396	3.9037	5.1920	573.1976
36300.	0.2941	0.5423	1.8440	3.9226	5.2170	573.1976
36400.	0.2927	0.5410	1.8484	3.9415	5.2422	573.1976
36500.	0.2913	0.5397	1.8529	3.9604	5.2674	573.1976
36600.	0.2899	0.5384	1.8573	3.9795	5.2928	573.1976
36700.	0.2885	0.5371	1.8618	3.9987	5.3183	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
36800.	6.457	0.2158	4.6338	216.66	14.719	0.7519	0.8671
36900.	6.426	0.2148	4.6561	216.66	14.719	0.7519	0.8671
37000.	6.395	0.2137	4.6785	216.66	14.719	0.7519	0.8671
37100.	6.365	0.2127	4.7011	216.66	14.719	0.7519	0.8671
37200.	6.334	0.2117	4.7237	216.66	14.719	0.7519	0.8671
37300.	6.304	0.2107	4.7465	216.66	14.719	0.7519	0.8671
37400.	6.274	0.2097	4.7693	216.66	14.719	0.7519	0.8671
37500.	6.244	0.2087	4.7923	216.66	14.719	0.7519	0.8671
37600.	6.214	0.2077	4.8154	216.66	14.719	0.7519	0.8671
37700.	6.184	0.2067	4.8386	216.66	14.719	0.7519	0.8671
37800.	6.154	0.2057	4.8619	216.66	14.719	0.7519	0.8671
37900.	6.125	0.2047	4.8853	216.66	14.719	0.7519	0.8671
38000.	6.095	0.2037	4.9089	216.66	14.719	0.7519	0.8671
38100.	6.066	0.2027	4.9325	216.66	14.719	0.7519	0.8671
38200.	6.037	0.2018	4.9563	216.66	14.719	0.7519	0.8671
38300.	6.008	0.2008	4.9802	216.66	14.719	0.7519	0.8671
38400.	5.979	0.1998	5.0042	216.66	14.719	0.7519	0.8671
38500.	5.951	0.1989	5.0283	216.66	14.719	0.7519	0.8671
38600.	5.922	0.1979	5.0525	216.66	14.719	0.7519	0.8671
38700.	5.894	0.1970	5.0768	216.66	14.719	0.7519	0.8671
38800.	5.865	0.1960	5.1013	216.66	14.719	0.7519	0.8671
38900.	5.837	0.1951	5.1259	216.66	14.719	0.7519	0.8671
39000.	5.809	0.1942	5.1506	216.66	14.719	0.7519	0.8671
39100.	5.781	0.1932	5.1754	216.66	14.719	0.7519	0.8671
39200.	5.754	0.1923	5.2003	216.66	14.719	0.7519	0.8671
39300.	5.726	0.1914	5.2254	216.66	14.719	0.7519	0.8671
39400.	5.699	0.1905	5.2505	216.66	14.719	0.7519	0.8671
39500.	5.671	0.1895	5.2758	216.66	14.719	0.7519	0.8671
39600.	5.644	0.1886	5.3013	216.66	14.719	0.7519	0.8671
39700.	5.617	0.1877	5.3268	216.66	14.719	0.7519	0.8671
39800.	5.590	0.1868	5.3525	216.66	14.719	0.7519	0.8671
39900.	5.563	0.1859	5.3783	216.66	14.719	0.7519	0.8671
40000.	5.537	0.1850	5.4042	216.66	14.719	0.7519	0.8671
40100.	5.510	0.1842	5.4302	216.66	14.719	0.7519	0.8671
40200.	5.484	0.1833	5.4564	216.66	14.719	0.7519	0.8671
40300.	5.457	0.1824	5.4827	216.66	14.719	0.7519	0.8671
40400.	5.431	0.1815	5.5091	216.66	14.719	0.7519	0.8671
40500.	5.405	0.1806	5.5356	216.66	14.719	0.7519	0.8671
40600.	5.379	0.1798	5.5623	216.66	14.719	0.7519	0.8671
40700.	5.354	0.1789	5.5891	216.66	14.719	0.7519	0.8671
40800.	5.328	0.1781	5.6160	216.66	14.719	0.7519	0.8671
40900.	5.302	0.1772	5.6431	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{\Delta\sqrt{\theta}}$	$a$ (Knots)
36800.	0.2871	0.5358	1.8663	4.0180	5.3429	573.1976
36900.	0.2857	0.5345	1.8708	4.0373	5.3607	573.1976
37000.	0.2844	0.5333	1.8753	4.0568	5.3785	573.1976
37100.	0.2830	0.5320	1.8798	4.0763	5.4215	573.1976
37200.	0.2816	0.5307	1.8843	4.0960	5.4477	573.1976
37300.	0.2803	0.5294	1.8889	4.1157	5.4739	573.1976
37400.	0.2789	0.5282	1.8934	4.1355	5.5003	573.1976
37500.	0.2776	0.5269	1.8980	4.1554	5.5268	573.1976
37600.	0.2763	0.5256	1.9025	4.1755	5.5534	573.1976
37700.	0.2749	0.5244	1.9071	4.1956	5.5802	573.1976
37800.	0.2736	0.5231	1.9117	4.2158	5.6070	573.1976
37900.	0.2723	0.5219	1.9163	4.2361	5.6341	573.1976
38000.	0.2710	0.5206	1.9209	4.2565	5.6612	573.1976
38100.	0.2697	0.5193	1.9255	4.2770	5.6885	573.1976
38200.	0.2684	0.5181	1.9302	4.2976	5.7159	573.1976
38300.	0.2671	0.5168	1.9348	4.3183	5.7434	573.1976
38400.	0.2659	0.5156	1.9395	4.3391	5.7711	573.1976
38500.	0.2646	0.5144	1.9441	4.3600	5.7989	573.1976
38600.	0.2633	0.5131	1.9488	4.3811	5.8268	573.1976
38700.	0.2620	0.5119	1.9535	4.4022	5.8549	573.1976
38800.	0.2608	0.5107	1.9582	4.4234	5.8821	573.1976
38900.	0.2595	0.5095	1.9629	4.4447	5.9110	573.1976
39000.	0.2583	0.5082	1.9676	4.4661	5.9399	573.1976
39100.	0.2571	0.5070	1.9724	4.4876	5.9686	573.1976
39200.	0.2558	0.5058	1.9771	4.5092	5.9973	573.1976
39300.	0.2546	0.5046	1.9819	4.5310	6.0262	573.1976
39400.	0.2534	0.5034	1.9866	4.5528	6.0553	573.1976
39500.	0.2522	0.5022	1.9914	4.5747	6.0844	573.1976
39600.	0.2510	0.5010	1.9962	4.5968	6.1137	573.1976
39700.	0.2498	0.4998	2.0010	4.6189	6.1432	573.1976
39800.	0.2486	0.4986	2.0058	4.6412	6.1728	573.1976
39900.	0.2474	0.4974	2.0106	4.6635	6.2025	573.1976
40000.	0.2462	0.4962	2.0155	4.6860	6.2324	573.1976
40100.	0.2450	0.4950	2.0203	4.7086	6.2624	573.1976
40200.	0.2438	0.4938	2.0252	4.7313	6.2926	573.1976
40300.	0.2427	0.4926	2.0301	4.7540	6.3229	573.1976
40400.	0.2415	0.4914	2.0349	4.7770	6.3534	573.1976
40500.	0.2403	0.4902	2.0398	4.8000	6.3840	573.1976
40600.	0.2392	0.4891	2.0448	4.8231	6.4148	573.1976
40700.	0.2380	0.4879	2.0497	4.8463	6.4457	573.1976
40800.	0.2369	0.4867	2.0546	4.8697	6.4767	573.1976
40900.	0.2358	0.4855	2.0595	4.8931	6.5079	573.1976



$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Lambda\sqrt{\sigma}}$	$a$ (Knots)
41000.	0.2346	0.4844	2.0645	4.9167	6.5303	573.1976
41100.	0.2335	0.4832	2.0695	4.9404	6.5708	573.1976
41200.	0.2324	0.4821	2.0744	4.9642	6.6074	573.1976
41300.	0.2313	0.4809	2.0794	4.9891	6.6343	573.1976
41400.	0.2302	0.4797	2.0844	5.0122	6.6662	573.1976
41500.	0.2291	0.4786	2.0895	5.0363	6.6983	573.1976
41600.	0.2280	0.4774	2.0945	5.0606	6.7306	573.1976
41700.	0.2269	0.4763	2.0995	5.0850	6.7630	573.1976
41800.	0.2258	0.4752	2.1046	5.1094	6.7956	573.1976
41900.	0.2247	0.4740	2.1096	5.1341	6.8284	573.1976
42000.	0.2236	0.4729	2.1147	5.1589	6.8613	573.1976
42100.	0.2225	0.4717	2.1198	5.1837	6.8943	573.1976
42200.	0.2215	0.4706	2.1249	5.2086	6.9275	573.1976
42300.	0.2204	0.4695	2.1300	5.2337	6.9609	573.1976
42400.	0.2194	0.4684	2.1351	5.2589	6.9944	573.1976
42500.	0.2183	0.4672	2.1403	5.2843	7.0281	573.1976
42600.	0.2173	0.4661	2.1454	5.3097	7.0620	573.1976
42700.	0.2162	0.4650	2.1506	5.3353	7.0960	573.1976
42800.	0.2152	0.4639	2.1558	5.3610	7.1302	573.1976
42900.	0.2141	0.4628	2.1610	5.3869	7.1646	573.1976
43000.	0.2131	0.4616	2.1662	5.4129	7.1991	573.1976
43100.	0.2121	0.4605	2.1714	5.4389	7.2338	573.1976
43200.	0.2111	0.4594	2.1766	5.4651	7.2686	573.1976
43300.	0.2101	0.4583	2.1818	5.4914	7.3036	573.1976
43400.	0.2091	0.4572	2.1871	5.5179	7.3388	573.1976
43500.	0.2081	0.4561	2.1923	5.5445	7.3742	573.1976
43600.	0.2071	0.4550	2.1976	5.5712	7.4097	573.1976
43700.	0.2061	0.4539	2.2029	5.5980	7.4454	573.1976
43800.	0.2051	0.4529	2.2082	5.6250	7.4813	573.1976
43900.	0.2041	0.4518	2.2135	5.6521	7.5173	573.1976
44000.	0.2031	0.4507	2.2188	5.6793	7.5536	573.1976
44100.	0.2021	0.4496	2.2242	5.7067	7.5899	573.1976
44200.	0.2012	0.4485	2.2295	5.7342	7.6265	573.1976
44300.	0.2002	0.4474	2.2349	5.7618	7.6633	573.1976
44400.	0.1993	0.4464	2.2403	5.7896	7.7002	573.1976
44500.	0.1983	0.4453	2.2457	5.8175	7.7373	573.1976
44600.	0.1973	0.4442	2.2511	5.8455	7.7746	573.1976
44700.	0.1964	0.4432	2.2565	5.8736	7.8120	573.1976
44800.	0.1955	0.4421	2.2619	5.9019	7.8496	573.1976
44900.	0.1945	0.4410	2.2674	5.9304	7.8875	573.1976
45000.	0.1936	0.4400	2.2728	5.9590	7.9255	573.1976
45100.	0.1927	0.4389	2.2783	5.9877	7.9637	573.1976



$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{1}{\sqrt{T_a}}$	$\frac{1}{\sqrt{T_a}}$
45200.	4.312	0.1441	6.9386	216.66	14.719	0.7519	0.8671
45300.	4.292	0.1434	6.9720	216.66	14.719	0.7519	0.8671
45400.	4.271	0.1427	7.0056	216.66	14.719	0.7519	0.8671
45500.	4.251	0.1421	7.0394	216.66	14.719	0.7519	0.8671
45600.	4.230	0.1414	7.0733	216.66	14.719	0.7519	0.8671
45700.	4.210	0.1407	7.1074	216.66	14.719	0.7519	0.8671
45800.	4.190	0.1400	7.1416	216.66	14.719	0.7519	0.8671
45900.	4.170	0.1394	7.1760	216.66	14.719	0.7519	0.8671
46000.	4.150	0.1387	7.2106	216.66	14.719	0.7519	0.8671
46100.	4.130	0.1380	7.2453	216.66	14.719	0.7519	0.8671
46200.	4.110	0.1374	7.2802	216.66	14.719	0.7519	0.8671
46300.	4.090	0.1367	7.3153	216.66	14.719	0.7519	0.8671
46400.	4.071	0.1360	7.3506	216.66	14.719	0.7519	0.8671
46500.	4.051	0.1354	7.3860	216.66	14.719	0.7519	0.8671
46600.	4.032	0.1347	7.4216	216.66	14.719	0.7519	0.8671
46700.	4.012	0.1341	7.4573	216.66	14.719	0.7519	0.8671
46800.	3.993	0.1335	7.4932	216.66	14.719	0.7519	0.8671
46900.	3.974	0.1328	7.5293	216.66	14.719	0.7519	0.8671
47000.	3.955	0.1322	7.5656	216.66	14.719	0.7519	0.8671
47100.	3.936	0.1315	7.6021	216.66	14.719	0.7519	0.8671
47200.	3.917	0.1309	7.6387	216.66	14.719	0.7519	0.8671
47300.	3.898	0.1303	7.6755	216.66	14.719	0.7519	0.8671
47400.	3.880	0.1297	7.7125	216.66	14.719	0.7519	0.8671
47500.	3.861	0.1290	7.7496	216.66	14.719	0.7519	0.8671
47600.	3.842	0.1284	7.7870	216.66	14.719	0.7519	0.8671
47700.	3.824	0.1278	7.8245	216.66	14.719	0.7519	0.8671
47800.	3.806	0.1272	7.8622	216.66	14.719	0.7519	0.8671
47900.	3.787	0.1266	7.9001	216.66	14.719	0.7519	0.8671
48000.	3.769	0.1260	7.9381	216.66	14.719	0.7519	0.8671
48100.	3.751	0.1254	7.9764	216.66	14.719	0.7519	0.8671
48200.	3.733	0.1248	8.0148	216.66	14.719	0.7519	0.8671
48300.	3.715	0.1242	8.0534	216.66	14.719	0.7519	0.8671
48400.	3.698	0.1236	8.0922	216.66	14.719	0.7519	0.8671
48500.	3.680	0.1230	8.1312	216.66	14.719	0.7519	0.8671
48600.	3.662	0.1224	8.1704	216.66	14.719	0.7519	0.8671
48700.	3.645	0.1218	8.2098	216.66	14.719	0.7519	0.8671
48800.	3.627	0.1212	8.2493	216.66	14.719	0.7519	0.8671
48900.	3.610	0.1206	8.2891	216.66	14.719	0.7519	0.8671
49000.	3.592	0.1201	8.3290	216.66	14.719	0.7519	0.8671
49100.	3.575	0.1195	8.3691	216.66	14.719	0.7519	0.8671
49200.	3.558	0.1189	8.4094	216.66	14.719	0.7519	0.8671
49300.	3.541	0.1183	8.4500	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $p/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
45200.	0.1917	0.4379	2.2838	6.0165	8.0020	573.1976
45300.	0.1924	0.4368	2.2893	6.0455	8.0476	573.1976
45400.	0.1897	0.4358	2.2948	6.0746	8.0793	573.1976
45500.	0.1890	0.4347	2.3003	6.1037	8.1182	573.1976
45600.	0.1881	0.4337	2.3058	6.1333	8.1574	573.1976
45700.	0.1872	0.4326	2.3114	6.1628	8.1967	573.1976
45800.	0.1863	0.4316	2.3169	6.1925	8.2361	573.1976
45900.	0.1854	0.4306	2.3225	6.2224	8.2758	573.1976
46000.	0.1845	0.4295	2.3281	6.2524	8.3157	573.1976
46100.	0.1836	0.4285	2.3337	6.2825	8.3558	573.1976
46200.	0.1827	0.4275	2.3393	6.3127	8.3970	573.1976
46300.	0.1819	0.4265	2.3449	6.3432	8.4365	573.1976
46400.	0.1810	0.4254	2.3506	6.3737	8.4771	573.1976
46500.	0.1801	0.4244	2.3562	6.4044	8.5180	573.1976
46600.	0.1793	0.4234	2.3619	6.4353	8.5590	573.1976
46700.	0.1784	0.4224	2.3676	6.4663	8.6002	573.1976
46800.	0.1775	0.4214	2.3733	6.4974	8.6417	573.1976
46900.	0.1767	0.4203	2.3790	6.5287	8.6833	573.1976
47000.	0.1758	0.4193	2.3847	6.5602	8.7251	573.1976
47100.	0.1750	0.4183	2.3905	6.5918	8.7672	573.1976
47200.	0.1742	0.4173	2.3962	6.6236	8.8094	573.1976
47300.	0.1733	0.4163	2.4020	6.6555	8.8519	573.1976
47400.	0.1725	0.4153	2.4077	6.6875	8.8945	573.1976
47500.	0.1717	0.4143	2.4135	6.7198	8.9374	573.1976
47600.	0.1708	0.4133	2.4193	6.7521	8.9804	573.1976
47700.	0.1700	0.4123	2.4252	6.7847	9.0237	573.1976
47800.	0.1692	0.4114	2.4310	6.8174	9.0672	573.1976
47900.	0.1684	0.4104	2.4369	6.8502	9.1108	573.1976
48000.	0.1676	0.4094	2.4427	6.8832	9.1547	573.1976
48100.	0.1668	0.4084	2.4486	6.9164	9.1988	573.1976
48200.	0.1660	0.4074	2.4545	6.9497	9.2432	573.1976
48300.	0.1652	0.4064	2.4604	6.9832	9.2877	573.1976
48400.	0.1644	0.4055	2.4663	7.0169	9.3324	573.1976
48500.	0.1636	0.4045	2.4722	7.0506	9.3774	573.1976
48600.	0.1628	0.4035	2.4782	7.0846	9.4226	573.1976
48700.	0.1620	0.4026	2.4842	7.1187	9.4680	573.1976
48800.	0.1613	0.4016	2.4901	7.1530	9.5136	573.1976
48900.	0.1605	0.4006	2.4961	7.1875	9.5594	573.1976
49000.	0.1597	0.3997	2.5021	7.2221	9.6055	573.1976
49100.	0.1590	0.3987	2.5081	7.2569	9.6518	573.1976
49200.	0.1582	0.3977	2.5142	7.2919	9.6983	573.1976
49300.	0.1574	0.3968	2.5202	7.3270	9.7450	573.1976

$h_a$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
4440.	3.524	0.1178	8.4907	216.66	14.719	0.7519	0.8671
4450.	3.520	0.1172	8.5316	216.66	14.719	0.7519	0.8671
4460.	3.516	0.1166	8.5727	216.66	14.719	0.7519	0.8671
4470.	3.512	0.1161	8.6140	216.66	14.719	0.7519	0.8671
4480.	3.507	0.1155	8.6555	216.66	14.719	0.7519	0.8671
4490.	3.503	0.1150	8.6972	216.66	14.719	0.7519	0.8671
4500.	3.500	0.1145	8.7391	216.66	14.719	0.7519	0.8671
50100.	3.402	0.1139	8.7812	216.66	14.719	0.7519	0.8671
50200.	3.398	0.1133	8.8235	216.66	14.719	0.7519	0.8671
50300.	3.394	0.1128	8.8660	216.66	14.719	0.7519	0.8671
50400.	3.390	0.1122	8.9087	216.66	14.719	0.7519	0.8671
50500.	3.386	0.1117	8.9516	216.66	14.719	0.7519	0.8671
50600.	3.382	0.1112	8.9948	216.66	14.719	0.7519	0.8671
50700.	3.378	0.1106	9.0381	216.66	14.719	0.7519	0.8671
50800.	3.374	0.1101	9.0817	216.66	14.719	0.7519	0.8671
50900.	3.370	0.1096	9.1254	216.66	14.719	0.7519	0.8671
51000.	3.366	0.1091	9.1694	216.66	14.719	0.7519	0.8671
51100.	3.362	0.1085	9.2135	216.66	14.719	0.7519	0.8671
51200.	3.358	0.1080	9.2579	216.66	14.719	0.7519	0.8671
51300.	3.354	0.1075	9.3025	216.66	14.719	0.7519	0.8671
51400.	3.350	0.1070	9.3474	216.66	14.719	0.7519	0.8671
51500.	3.346	0.1065	9.3924	216.66	14.719	0.7519	0.8671
51600.	3.342	0.1060	9.4376	216.66	14.719	0.7519	0.8671
51700.	3.338	0.1055	9.4831	216.66	14.719	0.7519	0.8671
51800.	3.334	0.1049	9.5288	216.66	14.719	0.7519	0.8671
51900.	3.330	0.1044	9.5747	216.66	14.719	0.7519	0.8671
52000.	3.326	0.1039	9.6208	216.66	14.719	0.7519	0.8671
52100.	3.322	0.1034	9.6672	216.66	14.719	0.7519	0.8671
52200.	3.318	0.1029	9.7138	216.66	14.719	0.7519	0.8671
52300.	3.314	0.1025	9.7606	216.66	14.719	0.7519	0.8671
52400.	3.310	0.1020	9.8076	216.66	14.719	0.7519	0.8671
52500.	3.306	0.1015	9.8549	216.66	14.719	0.7519	0.8671
52600.	3.302	0.1010	9.9023	216.66	14.719	0.7519	0.8671
52700.	3.298	0.1005	9.9500	216.66	14.719	0.7519	0.8671
52800.	2.993	0.1000	9.9980	216.66	14.719	0.7519	0.8671
52900.	2.989	0.0995	10.0461	216.66	14.719	0.7519	0.8671
53000.	2.984	0.0991	10.0946	216.66	14.719	0.7519	0.8671
53100.	2.980	0.0986	10.1432	216.66	14.719	0.7519	0.8671
53200.	2.976	0.0981	10.1921	216.66	14.719	0.7519	0.8671
53300.	2.972	0.0976	10.2412	216.66	14.719	0.7519	0.8671
53400.	2.968	0.0972	10.2905	216.66	14.719	0.7519	0.8671
53500.	2.964	0.0967	10.3401	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
47400.	0.1547	0.3933	2.5263	7.3623	9.7910	573.1976
47500.	0.1547	0.3940	2.5324	7.3973	9.8371	573.1976
47600.	0.1547	0.3947	2.5385	7.4334	9.8835	573.1976
47700.	0.1546	0.3930	2.5446	7.4692	9.9302	573.1976
47800.	0.1537	0.3920	2.5507	7.5052	9.9770	573.1976
47900.	0.1531	0.3911	2.5568	7.5414	10.0231	573.1976
50000.	0.1522	0.3902	2.5630	7.5777	10.0704	573.1976
50100.	0.1515	0.3892	2.5692	7.6142	10.1270	573.1976
50200.	0.1508	0.3883	2.5753	7.6509	10.1758	573.1976
50300.	0.1501	0.3874	2.5815	7.6878	10.2248	573.1976
50400.	0.1493	0.3864	2.5877	7.7248	10.2741	573.1976
50500.	0.1486	0.3855	2.5940	7.7620	10.3236	573.1976
50600.	0.1479	0.3846	2.6002	7.7994	10.3733	573.1976
50700.	0.1472	0.3837	2.6065	7.8370	10.4233	573.1976
50800.	0.1465	0.3827	2.6127	7.8748	10.475	573.1976
50900.	0.1458	0.3818	2.6190	7.9127	10.5240	573.1976
51000.	0.1451	0.3809	2.6253	7.9508	10.5747	573.1976
51100.	0.1444	0.3800	2.6316	7.9891	10.6256	573.1976
51200.	0.1437	0.3791	2.6380	8.0276	10.6768	573.1976
51300.	0.1430	0.3782	2.6443	8.0663	10.7283	573.1976
51400.	0.1423	0.3773	2.6507	8.1052	10.7799	573.1976
51500.	0.1416	0.3764	2.6571	8.1442	10.8319	573.1976
51600.	0.1410	0.3755	2.6635	8.1834	10.8841	573.1976
51700.	0.1403	0.3746	2.6699	8.2229	10.9365	573.1976
51800.	0.1396	0.3737	2.6763	8.2625	10.9892	573.1976
51900.	0.1389	0.3728	2.6827	8.3023	11.0421	573.1976
52000.	0.1383	0.3719	2.6892	8.3423	11.0953	573.1976
52100.	0.1376	0.3710	2.6957	8.3825	11.1488	573.1976
52200.	0.1370	0.3701	2.7021	8.4229	11.2025	573.1976
52300.	0.1363	0.3692	2.7086	8.4635	11.2565	573.1976
52400.	0.1356	0.3683	2.7152	8.5042	11.3107	573.1976
52500.	0.1350	0.3674	2.7217	8.5452	11.3652	573.1976
52600.	0.1343	0.3665	2.7282	8.5864	11.4200	573.1976
52700.	0.1337	0.3657	2.7348	8.6277	11.4750	573.1976
52800.	0.1331	0.3648	2.7414	8.6693	11.5303	573.1976
52900.	0.1324	0.3639	2.7480	8.7111	11.5858	573.1976
53000.	0.1318	0.3630	2.7546	8.7531	11.6416	573.1976
53100.	0.1312	0.3622	2.7612	8.7952	11.6977	573.1976
53200.	0.1305	0.3613	2.7679	8.8376	11.7541	573.1976
53300.	0.1299	0.3604	2.7745	8.8802	11.8107	573.1976
53400.	0.1293	0.3596	2.7812	8.9230	11.8676	573.1976
53500.	0.1287	0.3587	2.7879	8.9660	11.9248	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ ("K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
53600.	2.880	0.0962	10.3899	216.66	14.719	0.7519	0.8671
53700.	2.866	0.0958	10.4400	216.66	14.719	0.7519	0.8671
53800.	2.852	0.0953	10.4903	216.66	14.719	0.7519	0.8671
53900.	2.839	0.0949	10.5408	216.66	14.719	0.7519	0.8671
54000.	2.825	0.0944	10.5916	216.66	14.719	0.7519	0.8671
54100.	2.811	0.0940	10.6426	216.66	14.719	0.7519	0.8671
54200.	2.798	0.0935	10.6939	216.66	14.719	0.7519	0.8671
54300.	2.785	0.0931	10.7454	216.66	14.719	0.7519	0.8671
54400.	2.771	0.0926	10.7972	216.66	14.719	0.7519	0.8671
54500.	2.758	0.0922	10.8492	216.66	14.719	0.7519	0.8671
54600.	2.745	0.0917	10.9015	216.66	14.719	0.7519	0.8671
54700.	2.732	0.0913	10.9540	216.66	14.719	0.7519	0.8671
54800.	2.718	0.0909	11.0068	216.66	14.719	0.7519	0.8671
54900.	2.705	0.0904	11.0598	216.66	14.719	0.7519	0.8671
55000.	2.692	0.0900	11.1131	216.66	14.719	0.7519	0.8671
55100.	2.680	0.0896	11.1666	216.66	14.719	0.7519	0.8671
55200.	2.667	0.0891	11.2204	216.66	14.719	0.7519	0.8671
55300.	2.654	0.0887	11.2745	216.66	14.719	0.7519	0.8671
55400.	2.641	0.0883	11.3288	216.66	14.719	0.7519	0.8671
55500.	2.629	0.0878	11.3834	216.66	14.719	0.7519	0.8671
55600.	2.616	0.0874	11.4382	216.66	14.719	0.7519	0.8671
55700.	2.603	0.0870	11.4933	216.66	14.719	0.7519	0.8671
55800.	2.591	0.0866	11.5487	216.66	14.719	0.7519	0.8671
55900.	2.578	0.0862	11.6043	216.66	14.719	0.7519	0.8671
56000.	2.566	0.0858	11.6603	216.66	14.719	0.7519	0.8671
56100.	2.554	0.0854	11.7164	216.66	14.719	0.7519	0.8671
56200.	2.542	0.0849	11.7729	216.66	14.719	0.7519	0.8671
56300.	2.529	0.0845	11.8296	216.66	14.719	0.7519	0.8671
56400.	2.517	0.0841	11.8866	216.66	14.719	0.7519	0.8671
56500.	2.505	0.0837	11.9439	216.66	14.719	0.7519	0.8671
56600.	2.493	0.0833	12.0014	216.66	14.719	0.7519	0.8671
56700.	2.481	0.0829	12.0592	216.66	14.719	0.7519	0.8671
56800.	2.469	0.0825	12.1173	216.66	14.719	0.7519	0.8671
56900.	2.457	0.0821	12.1757	216.66	14.719	0.7519	0.8671
57000.	2.446	0.0817	12.2344	216.66	14.719	0.7519	0.8671
57100.	2.434	0.0813	12.2933	216.66	14.719	0.7519	0.8671
57200.	2.422	0.0810	12.3525	216.66	14.719	0.7519	0.8671
57300.	2.411	0.0806	12.4121	216.66	14.719	0.7519	0.8671
57400.	2.399	0.0802	12.4719	216.66	14.719	0.7519	0.8671
57500.	2.388	0.0798	12.5319	216.66	14.719	0.7519	0.8671
57600.	2.376	0.0794	12.5923	216.66	14.719	0.7519	0.8671
57700.	2.365	0.0790	12.6530	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
53600.	0.1290	0.3570	2.7946	9.0091	11.9573	573.1976
53700.	0.1274	0.3570	2.8013	9.0526	12.0400	573.1976
53800.	0.1268	0.3561	2.8081	9.0962	12.0990	573.1976
53900.	0.1262	0.3553	2.8148	9.1407	12.1563	573.1976
54000.	0.1256	0.3544	2.8216	9.1840	12.2147	573.1976
54100.	0.1250	0.3536	2.8284	9.2283	12.2727	573.1976
54200.	0.1244	0.3527	2.8352	9.2727	12.3328	573.1976
54300.	0.1239	0.3519	2.8420	9.3174	12.3923	573.1976
54400.	0.1232	0.3510	2.8488	9.3623	12.4520	573.1976
54500.	0.1226	0.3502	2.8557	9.4074	12.5120	573.1976
54600.	0.1220	0.3493	2.8626	9.4527	12.5722	573.1976
54700.	0.1215	0.3485	2.8695	9.4983	12.6328	573.1976
54800.	0.1209	0.3477	2.8764	9.5440	12.6927	573.1976
54900.	0.1203	0.3468	2.8833	9.5900	12.7548	573.1976
55000.	0.1197	0.3460	2.8902	9.6362	12.8163	573.1976
55100.	0.1191	0.3452	2.8972	9.6827	12.8790	573.1976
55200.	0.1186	0.3443	2.9041	9.7293	12.9401	573.1976
55300.	0.1180	0.3435	2.9111	9.7762	13.0024	573.1976
55400.	0.1174	0.3427	2.9181	9.8233	13.0651	573.1976
55500.	0.1169	0.3419	2.9252	9.8706	13.1290	573.1976
55600.	0.1163	0.3410	2.9322	9.9182	13.1913	573.1976
55700.	0.1158	0.3402	2.9393	9.9659	13.2548	573.1976
55800.	0.1152	0.3394	2.9463	10.0147	13.3197	573.1976
55900.	0.1146	0.3386	2.9534	10.0622	13.3828	573.1976
56000.	0.1141	0.3378	2.9605	10.1107	13.4473	573.1976
56100.	0.1135	0.3370	2.9676	10.1594	13.5121	573.1976
56200.	0.1130	0.3362	2.9748	10.2083	13.5772	573.1976
56300.	0.1125	0.3354	2.9819	10.2575	13.6426	573.1976
56400.	0.1119	0.3345	2.9891	10.3069	13.7093	573.1976
56500.	0.1114	0.3337	2.9963	10.3566	13.7744	573.1976
56600.	0.1109	0.3329	3.0035	10.4065	13.8408	573.1976
56700.	0.1103	0.3321	3.0107	10.4566	13.9074	573.1976
56800.	0.1099	0.3313	3.0180	10.5070	13.9744	573.1976
56900.	0.1093	0.3306	3.0252	10.5576	14.0418	573.1976
57000.	0.1087	0.3298	3.0325	10.6085	14.1094	573.1976
57100.	0.1082	0.3290	3.0398	10.6596	14.1774	573.1976
57200.	0.1077	0.3282	3.0471	10.7110	14.2457	573.1976
57300.	0.1072	0.3274	3.0545	10.7626	14.3143	573.1976
57400.	0.1067	0.3266	3.0618	10.8144	14.3833	573.1976
57500.	0.1062	0.3259	3.0692	10.8665	14.4526	573.1976
57600.	0.1056	0.3250	3.0766	10.9189	14.5222	573.1976
57700.	0.1051	0.3243	3.0840	10.9715	14.5922	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\theta$ $P_a/P_{aSL}$	$\frac{1}{\theta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
57800.	2.353	0.0787	12.7140	216.66	14.719	0.7519	0.8671
57900.	2.347	0.0783	12.7752	216.66	14.719	0.7519	0.8671
58000.	2.331	0.0779	12.8368	216.66	14.719	0.7519	0.8671
58100.	2.325	0.0775	12.8986	216.66	14.719	0.7519	0.8671
58200.	2.309	0.0772	12.9608	216.66	14.719	0.7519	0.8671
58300.	2.298	0.0768	13.0232	216.66	14.719	0.7519	0.8671
58400.	2.287	0.0764	13.0859	216.66	14.719	0.7519	0.8671
58500.	2.276	0.0761	13.1490	216.66	14.719	0.7519	0.8671
58600.	2.265	0.0757	13.2123	216.66	14.719	0.7519	0.8671
58700.	2.254	0.0753	13.2760	216.66	14.719	0.7519	0.8671
58800.	2.243	0.0750	13.3400	216.66	14.719	0.7519	0.8671
58900.	2.232	0.0746	13.4042	216.66	14.719	0.7519	0.8671
59000.	2.222	0.0742	13.4688	216.66	14.719	0.7519	0.8671
59100.	2.211	0.0739	13.5337	216.66	14.719	0.7519	0.8671
59200.	2.200	0.0735	13.5989	216.66	14.719	0.7519	0.8671
59300.	2.190	0.0732	13.6644	216.66	14.719	0.7519	0.8671
59400.	2.179	0.0728	13.7303	216.66	14.719	0.7519	0.8671
59500.	2.169	0.0725	13.7964	216.66	14.719	0.7519	0.8671
59600.	2.158	0.0721	13.8629	216.66	14.719	0.7519	0.8671
59700.	2.148	0.0718	13.9297	216.66	14.719	0.7519	0.8671
59800.	2.138	0.0714	13.9968	216.66	14.719	0.7519	0.8671
59900.	2.127	0.0711	14.0642	216.66	14.719	0.7519	0.8671
60000.	2.117	0.0708	14.1320	216.66	14.719	0.7519	0.8671
60100.	2.107	0.0704	14.2001	216.66	14.719	0.7519	0.8671
60200.	2.097	0.0701	14.2685	216.66	14.719	0.7519	0.8671
60300.	2.087	0.0697	14.3372	216.66	14.719	0.7519	0.8671
60400.	2.077	0.0694	14.4063	216.66	14.719	0.7519	0.8671
60500.	2.067	0.0691	14.4757	216.66	14.719	0.7519	0.8671
60600.	2.057	0.0688	14.5454	216.66	14.719	0.7519	0.8671
60700.	2.047	0.0684	14.6155	216.66	14.719	0.7519	0.8671
60800.	2.037	0.0681	14.6859	216.66	14.719	0.7519	0.8671
60900.	2.024	0.0678	14.7567	216.66	14.719	0.7519	0.8671
61000.	2.013	0.0674	14.8278	216.66	14.719	0.7519	0.8671
61100.	2.003	0.0671	14.8992	216.66	14.719	0.7519	0.8671
61200.	1.993	0.0668	14.9710	216.66	14.719	0.7519	0.8671
61300.	1.983	0.0665	15.0431	216.66	14.719	0.7519	0.8671
61400.	1.973	0.0662	15.1156	216.66	14.719	0.7519	0.8671
61500.	1.970	0.0658	15.1884	216.66	14.719	0.7519	0.8671
61600.	1.961	0.0655	15.2616	216.66	14.719	0.7519	0.8671
61700.	1.951	0.0652	15.3352	216.66	14.719	0.7519	0.8671
61800.	1.942	0.0649	15.4090	216.66	14.719	0.7519	0.8671
61900.	1.932	0.0646	15.4833	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{\lambda\sqrt{\theta}}$	$a$ (Knots)
57900.	0.1144	0.3382	3.0914	11.0244	14.6625	573.1976
57900.	0.1141	0.3327	3.0998	11.0775	14.7321	573.1976
57900.	0.1136	0.3219	3.1063	11.1303	14.8041	573.1976
58100.	0.1131	0.3212	3.1138	11.1845	14.8755	573.1976
58200.	0.1126	0.3204	3.1213	11.2384	14.9471	573.1976
58300.	0.1022	0.3196	3.1288	11.2925	15.0191	573.1976
58400.	0.1017	0.3188	3.1363	11.3469	15.0915	573.1976
58500.	0.1012	0.3181	3.1438	11.4016	15.1642	573.1976
58600.	0.1007	0.3173	3.1514	11.4565	15.2373	573.1976
58700.	0.1002	0.3166	3.1590	11.5117	15.3107	573.1976
58800.	0.0997	0.3158	3.1666	11.5672	15.3844	573.1976
58900.	0.0993	0.3150	3.1742	11.6229	15.4586	573.1976
59000.	0.0988	0.3143	3.1818	11.6787	15.5330	573.1976
59100.	0.0983	0.3135	3.1895	11.7352	15.6079	573.1976
59200.	0.0978	0.3128	3.1972	11.7917	15.6831	573.1976
59300.	0.0974	0.3120	3.2049	11.8485	15.7596	573.1976
59400.	0.0969	0.3112	3.2126	11.9056	15.8346	573.1976
59500.	0.0964	0.3105	3.2203	11.9630	15.9109	573.1976
59600.	0.0960	0.3098	3.2281	12.0206	15.9875	573.1976
59700.	0.0955	0.3090	3.2358	12.0785	16.0645	573.1976
59800.	0.0951	0.3083	3.2436	12.1367	16.1419	573.1976
59900.	0.0946	0.3076	3.2514	12.1952	16.2197	573.1976
60000.	0.0941	0.3068	3.2592	12.2537	16.2979	573.1976
60100.	0.0937	0.3061	3.2671	12.3130	16.3764	573.1976
60200.	0.0932	0.3053	3.2749	12.3723	16.4553	573.1976
60300.	0.0928	0.3046	3.2828	12.4319	16.5346	573.1976
60400.	0.0923	0.3039	3.2907	12.4918	16.6142	573.1976
60500.	0.0919	0.3032	3.2986	12.5520	16.6943	573.1976
60600.	0.0915	0.3024	3.3066	12.6125	16.7747	573.1976
60700.	0.0910	0.3017	3.3145	12.6732	16.8555	573.1976
60800.	0.0906	0.3010	3.3225	12.7343	16.9367	573.1976
60900.	0.0902	0.3003	3.3305	12.7956	17.0183	573.1976
61000.	0.0897	0.2995	3.3385	12.8573	17.1003	573.1976
61100.	0.0893	0.2988	3.3465	12.9192	17.1827	573.1976
61200.	0.0889	0.2981	3.3546	12.9815	17.2655	573.1976
61300.	0.0884	0.2974	3.3627	13.0440	17.3487	573.1976
61400.	0.0880	0.2967	3.3708	13.1069	17.4323	573.1976
61500.	0.0876	0.2960	3.3789	13.1700	17.5162	573.1976
61600.	0.0872	0.2952	3.3870	13.2335	17.6006	573.1976
61700.	0.0868	0.2945	3.3951	13.2972	17.6854	573.1976
61800.	0.0863	0.2939	3.4033	13.3613	17.7706	573.1976
61900.	0.0859	0.2931	3.4115	13.4257	17.8563	573.1976



$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
62000.	1.923	0.0643	15.5579	216.66	14.719	0.7519	0.8671
62100.	1.914	0.0640	15.6328	216.66	14.719	0.7519	0.8671
62200.	1.905	0.0637	15.7081	216.66	14.719	0.7519	0.8671
62300.	1.896	0.0634	15.7838	216.66	14.719	0.7519	0.8671
62400.	1.887	0.0631	15.8599	216.66	14.719	0.7519	0.8671
62500.	1.878	0.0627	15.9363	216.66	14.719	0.7519	0.8671
62600.	1.869	0.0624	16.0131	216.66	14.719	0.7519	0.8671
62700.	1.860	0.0621	16.0902	216.66	14.719	0.7519	0.8671
62800.	1.851	0.0619	16.1677	216.66	14.719	0.7519	0.8671
62900.	1.842	0.0616	16.2456	216.66	14.719	0.7519	0.8671
63000.	1.833	0.0613	16.3239	216.66	14.719	0.7519	0.8671
63100.	1.824	0.0610	16.4025	216.66	14.719	0.7519	0.8671
63200.	1.815	0.0607	16.4816	216.66	14.719	0.7519	0.8671
63300.	1.807	0.0604	16.5610	216.66	14.719	0.7519	0.8671
63400.	1.798	0.0601	16.6406	216.66	14.719	0.7519	0.8671
63500.	1.789	0.0598	16.7209	216.66	14.719	0.7519	0.8671
63600.	1.781	0.0595	16.8015	216.66	14.719	0.7519	0.8671
63700.	1.772	0.0592	16.8825	216.66	14.719	0.7519	0.8671
63800.	1.764	0.0589	16.9638	216.66	14.719	0.7519	0.8671
63900.	1.755	0.0587	17.0455	216.66	14.719	0.7519	0.8671
64000.	1.747	0.0584	17.1276	216.66	14.719	0.7519	0.8671
64100.	1.739	0.0581	17.2102	216.66	14.719	0.7519	0.8671
64200.	1.730	0.0578	17.2931	216.66	14.719	0.7519	0.8671
64300.	1.722	0.0575	17.3764	216.66	14.719	0.7519	0.8671
64400.	1.714	0.0573	17.4601	216.66	14.719	0.7519	0.8671
64500.	1.705	0.0570	17.5442	216.66	14.719	0.7519	0.8671
64600.	1.697	0.0567	17.6288	216.66	14.719	0.7519	0.8671
64700.	1.689	0.0565	17.7137	216.66	14.719	0.7519	0.8671
64800.	1.681	0.0562	17.7990	216.66	14.719	0.7519	0.8671
64900.	1.673	0.0559	17.8848	216.66	14.719	0.7519	0.8671
65000.	1.665	0.0556	17.9710	216.66	14.719	0.7519	0.8671
65100.	1.657	0.0554	18.0575	216.66	14.719	0.7519	0.8671
65200.	1.649	0.0551	18.1445	216.66	14.719	0.7519	0.8671
65300.	1.641	0.0548	18.2320	216.66	14.719	0.7519	0.8671
65400.	1.633	0.0546	18.3198	216.66	14.719	0.7519	0.8671
65500.	1.625	0.0543	18.4081	216.66	14.719	0.7519	0.8671
65600.	1.618	0.0541	18.4968	216.66	14.719	0.7519	0.8671
65700.	1.610	0.0538	18.5859	216.66	14.719	0.7519	0.8671
65800.	1.602	0.0535	18.6754	216.66	14.719	0.7519	0.8671
65900.	1.594	0.0533	18.7654	216.66	14.719	0.7519	0.8671
66000.	1.587	0.0530	18.8558	216.66	14.719	0.7519	0.8671
66100.	1.579	0.0528	18.9466	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
62000.	0.2855	0.2924	3.4197	13.4903	17.9423	573.1976
62100.	0.2851	0.2917	3.4279	13.5553	18.0297	573.1976
62200.	0.2847	0.2910	3.4362	13.6206	18.1156	573.1976
62300.	0.2843	0.2903	3.4444	13.6863	18.2029	573.1976
62400.	0.2839	0.2896	3.4527	13.7522	18.2906	573.1976
62500.	0.2835	0.2889	3.4610	13.8185	18.3787	573.1976
62600.	0.2831	0.2882	3.4694	13.8850	18.4672	573.1976
62700.	0.2827	0.2875	3.4777	13.9517	18.5562	573.1976
62800.	0.2823	0.2869	3.4861	14.0192	18.6456	573.1976
62900.	0.2819	0.2862	3.4945	14.0867	18.7354	573.1976
63000.	0.2815	0.2855	3.5029	14.1546	18.8257	573.1976
63100.	0.2811	0.2848	3.5113	14.2228	18.9164	573.1976
63200.	0.2807	0.2841	3.5198	14.2913	19.0076	573.1976
63300.	0.2803	0.2834	3.5282	14.3601	19.0991	573.1976
63400.	0.2799	0.2827	3.5367	14.4293	19.1911	573.1976
63500.	0.2796	0.2821	3.5452	14.4988	19.2836	573.1976
63600.	0.2792	0.2814	3.5538	14.5687	19.3765	573.1976
63700.	0.2788	0.2807	3.5623	14.6389	19.4699	573.1976
63800.	0.2784	0.2800	3.5709	14.7094	19.5637	573.1976
63900.	0.2780	0.2794	3.5795	14.7803	19.6579	573.1976
64000.	0.2777	0.2787	3.5881	14.8515	19.7526	573.1976
64100.	0.2773	0.2780	3.5967	14.9230	19.8478	573.1976
64200.	0.2769	0.2774	3.6054	14.9949	19.9434	573.1976
64300.	0.2766	0.2767	3.6140	15.0672	20.0395	573.1976
64400.	0.2762	0.2760	3.6227	15.1398	20.1361	573.1976
64500.	0.2758	0.2754	3.6315	15.2127	20.2331	573.1976
64600.	0.2755	0.2747	3.6402	15.2860	20.3306	573.1976
64700.	0.2751	0.2741	3.6490	15.3597	20.4295	573.1976
64800.	0.2747	0.2734	3.6577	15.4337	20.5299	573.1976
64900.	0.2744	0.2727	3.6665	15.5080	20.6258	573.1976
65000.	0.2740	0.2721	3.6754	15.5827	20.7252	573.1976
65100.	0.2737	0.2714	3.6842	15.6579	20.8251	573.1976
65200.	0.2733	0.2708	3.6931	15.7333	20.9254	573.1976
65300.	0.2730	0.2701	3.7019	15.8091	21.0262	573.1976
65400.	0.2726	0.2695	3.7109	15.8852	21.1275	573.1976
65500.	0.2723	0.2688	3.7198	15.9619	21.2293	573.1976
65600.	0.2719	0.2682	3.7287	16.0387	21.3316	573.1976
65700.	0.2716	0.2675	3.7377	16.1159	21.4344	573.1976
65800.	0.2712	0.2669	3.7467	16.1936	21.5376	573.1976
65900.	0.2709	0.2663	3.7557	16.2716	21.6414	573.1976
66000.	0.2706	0.2656	3.7648	16.3500	21.7457	573.1976
66100.	0.2702	0.2650	3.7738	16.4288	21.8504	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
66200.	1.572	0.0525	19.0379	216.66	14.719	0.7519	0.8671
66300.	1.564	0.0523	19.1297	216.66	14.719	0.7519	0.8671
66400.	1.557	0.0520	19.2218	216.66	14.719	0.7519	0.8671
66500.	1.549	0.0518	19.3144	216.66	14.719	0.7519	0.8671
66600.	1.542	0.0515	19.4075	216.66	14.719	0.7519	0.8671
66700.	1.534	0.0513	19.5010	216.66	14.719	0.7519	0.8671
66800.	1.527	0.0510	19.5949	216.66	14.719	0.7519	0.8671
66900.	1.520	0.0508	19.6893	216.66	14.719	0.7519	0.8671
67000.	1.512	0.0505	19.7842	216.66	14.719	0.7519	0.8671
67100.	1.505	0.0503	19.8795	216.66	14.719	0.7519	0.8671
67200.	1.498	0.0501	19.9753	216.66	14.719	0.7519	0.8671
67300.	1.491	0.0498	20.0715	216.66	14.719	0.7519	0.8671
67400.	1.484	0.0496	20.1683	216.66	14.719	0.7519	0.8671
67500.	1.476	0.0493	20.2654	216.66	14.719	0.7519	0.8671
67600.	1.469	0.0491	20.3631	216.66	14.719	0.7519	0.8671
67700.	1.462	0.0489	20.4612	216.66	14.719	0.7519	0.8671
67800.	1.455	0.0486	20.5597	216.66	14.719	0.7519	0.8671
67900.	1.448	0.0484	20.6588	216.66	14.719	0.7519	0.8671
68000.	1.441	0.0482	20.7583	216.66	14.719	0.7519	0.8671
68100.	1.434	0.0479	20.8583	216.66	14.719	0.7519	0.8671
68200.	1.428	0.0477	20.9588	216.66	14.719	0.7519	0.8671
68300.	1.421	0.0475	21.0598	216.66	14.719	0.7519	0.8671
68400.	1.414	0.0473	21.1613	216.66	14.719	0.7519	0.8671
68500.	1.407	0.0470	21.2632	216.66	14.719	0.7519	0.8671
68600.	1.400	0.0468	21.3657	216.66	14.719	0.7519	0.8671
68700.	1.394	0.0466	21.4686	216.66	14.719	0.7519	0.8671
68800.	1.387	0.0464	21.5720	216.66	14.719	0.7519	0.8671
68900.	1.380	0.0461	21.6760	216.66	14.719	0.7519	0.8671
69000.	1.374	0.0459	21.7804	216.66	14.719	0.7519	0.8671
69100.	1.367	0.0457	21.8854	216.66	14.719	0.7519	0.8671
69200.	1.361	0.0455	21.9908	216.66	14.719	0.7519	0.8671
69300.	1.354	0.0453	22.0967	216.66	14.719	0.7519	0.8671
69400.	1.348	0.0450	22.2032	216.66	14.719	0.7519	0.8671
69500.	1.341	0.0448	22.3102	216.66	14.719	0.7519	0.8671
69600.	1.335	0.0446	22.4177	216.66	14.719	0.7519	0.8671
69700.	1.329	0.0444	22.5257	216.66	14.719	0.7519	0.8671
69800.	1.322	0.0442	22.6342	216.66	14.719	0.7519	0.8671
69900.	1.316	0.0440	22.7432	216.66	14.719	0.7519	0.8671
70000.	1.309	0.0438	22.8528	216.66	14.719	0.7519	0.8671
70100.	1.303	0.0435	22.9629	216.66	14.719	0.7519	0.8671
70200.	1.297	0.0433	23.0736	216.66	14.719	0.7519	0.8671
70300.	1.291	0.0431	23.1847	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/\text{PSL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{h\sqrt{\sigma}}$	$a$ (Knots)
66200.	0.2659	0.2643	3.7829	16.5077	21.9557	573.1976
66300.	0.2659	0.2637	3.7920	16.5875	22.0615	573.1976
66400.	0.2659	0.2631	3.8011	16.6674	22.1678	573.1976
66500.	0.2659	0.2624	3.8103	16.7477	22.2746	573.1976
66600.	0.2659	0.2618	3.8194	16.8284	22.3819	573.1976
66700.	0.2682	0.2612	3.8286	16.9094	22.4897	573.1976
66800.	0.2679	0.2606	3.8378	16.9909	22.5981	573.1976
66900.	0.2676	0.2599	3.8471	17.0723	22.7070	573.1976
67000.	0.2672	0.2593	3.8563	17.1550	22.8164	573.1976
67100.	0.2669	0.2587	3.8656	17.2377	22.9263	573.1976
67200.	0.2666	0.2581	3.8749	17.3207	23.0367	573.1976
67300.	0.2663	0.2575	3.8842	17.4042	23.1477	573.1976
67400.	0.2660	0.2568	3.8936	17.4880	23.2592	573.1976
67500.	0.2656	0.2562	3.9029	17.5723	23.3713	573.1976
67600.	0.2653	0.2556	3.9123	17.6569	23.4839	573.1976
67700.	0.2650	0.2550	3.9217	17.7420	23.5971	573.1976
67800.	0.2647	0.2544	3.9312	17.8275	23.7107	573.1976
67900.	0.2644	0.2538	3.9406	17.9134	23.8250	573.1976
68000.	0.2641	0.2532	3.9501	17.9997	23.9398	573.1976
68100.	0.2638	0.2525	3.9596	18.0864	24.0551	573.1976
68200.	0.2635	0.2519	3.9691	18.1735	24.1710	573.1976
68300.	0.2632	0.2513	3.9787	18.2611	24.2875	573.1976
68400.	0.2629	0.2507	3.9883	18.3491	24.4045	573.1976
68500.	0.2625	0.2501	3.9979	18.4375	24.5220	573.1976
68600.	0.2623	0.2495	4.0075	18.5263	24.6402	573.1976
68700.	0.2620	0.2489	4.0171	18.6156	24.7589	573.1976
68800.	0.2617	0.2483	4.0268	18.7053	24.8782	573.1976
68900.	0.2614	0.2477	4.0365	18.7954	24.9981	573.1976
69000.	0.2611	0.2471	4.0462	18.8859	25.1185	573.1976
69100.	0.2608	0.2466	4.0559	18.9769	25.2395	573.1976
69200.	0.2605	0.2460	4.0657	19.0684	25.3611	573.1976
69300.	0.2602	0.2454	4.0755	19.1602	25.4833	573.1976
69400.	0.2599	0.2448	4.0853	19.2525	25.6061	573.1976
69500.	0.2596	0.2442	4.0951	19.3453	25.7294	573.1976
69600.	0.2593	0.2436	4.1050	19.4385	25.8534	573.1976
69700.	0.2591	0.2430	4.1148	19.5322	25.9780	573.1976
69800.	0.2588	0.2424	4.1247	19.6263	26.1031	573.1976
69900.	0.2585	0.2419	4.1347	19.7209	26.2289	573.1976
70000.	0.2582	0.2413	4.1446	19.8159	26.3553	573.1976
70100.	0.2579	0.2407	4.1546	19.9113	26.4822	573.1976
70200.	0.2577	0.2401	4.1646	20.0072	26.6098	573.1976
70300.	0.2574	0.2395	4.1746	20.1036	26.7380	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\theta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
70400.	1.284	0.0429	23.2964	216.66	14.719	0.7519	0.8671
70500.	1.278	0.0427	23.4087	216.66	14.719	0.7519	0.8671
70600.	1.272	0.0425	23.5214	216.66	14.719	0.7519	0.8671
70700.	1.266	0.0423	23.6348	216.66	14.719	0.7519	0.8671
70800.	1.260	0.0421	23.7486	216.66	14.719	0.7519	0.8671
70900.	1.254	0.0419	23.8631	216.66	14.719	0.7519	0.8671
71000.	1.248	0.0417	23.9780	216.66	14.719	0.7519	0.8671
71100.	1.242	0.0415	24.0936	216.66	14.719	0.7519	0.8671
71200.	1.236	0.0413	24.2096	216.66	14.719	0.7519	0.8671
71300.	1.230	0.0411	24.3263	216.66	14.719	0.7519	0.8671
71400.	1.224	0.0409	24.4435	216.66	14.719	0.7519	0.8671
71500.	1.218	0.0407	24.5612	216.66	14.719	0.7519	0.8671
71600.	1.212	0.0405	24.6796	216.66	14.719	0.7519	0.8671
71700.	1.207	0.0403	24.7985	216.66	14.719	0.7519	0.8671
71800.	1.201	0.0401	24.9180	216.66	14.719	0.7519	0.8671
71900.	1.195	0.0399	25.0380	216.66	14.719	0.7519	0.8671
72000.	1.189	0.0397	25.1586	216.66	14.719	0.7519	0.8671
72100.	1.184	0.0396	25.2799	216.66	14.719	0.7519	0.8671
72200.	1.178	0.0394	25.4017	216.66	14.719	0.7519	0.8671
72300.	1.172	0.0392	25.5240	216.66	14.719	0.7519	0.8671
72400.	1.167	0.0390	25.6470	216.66	14.719	0.7519	0.8671
72500.	1.161	0.0388	25.7706	216.66	14.719	0.7519	0.8671
72600.	1.155	0.0386	25.8947	216.66	14.719	0.7519	0.8671
72700.	1.150	0.0384	26.0195	216.66	14.719	0.7519	0.8671
72800.	1.144	0.0382	26.1449	216.66	14.719	0.7519	0.8671
72900.	1.139	0.0381	26.2708	216.66	14.719	0.7519	0.8671
73000.	1.133	0.0379	26.3974	216.66	14.719	0.7519	0.8671
73100.	1.128	0.0377	26.5246	216.66	14.719	0.7519	0.8671
73200.	1.123	0.0375	26.6524	216.66	14.719	0.7519	0.8671
73300.	1.117	0.0373	26.7808	216.66	14.719	0.7519	0.8671
73400.	1.112	0.0372	26.9098	216.66	14.719	0.7519	0.8671
73500.	1.107	0.0370	27.0394	216.66	14.719	0.7519	0.8671
73600.	1.101	0.0368	27.1697	216.66	14.719	0.7519	0.8671
73700.	1.096	0.0366	27.3006	216.66	14.719	0.7519	0.8671
73800.	1.091	0.0365	27.4322	216.66	14.719	0.7519	0.8671
73900.	1.086	0.0363	27.5643	216.66	14.719	0.7519	0.8671
74000.	1.080	0.0361	27.6971	216.66	14.719	0.7519	0.8671
74100.	1.075	0.0359	27.8306	216.66	14.719	0.7519	0.8671
74200.	1.070	0.0358	27.9646	216.66	14.719	0.7519	0.8671
74300.	1.065	0.0356	28.0994	216.66	14.719	0.7519	0.8671
74400.	1.060	0.0354	28.2348	216.66	14.719	0.7519	0.8671
74500.	1.055	0.0352	28.3708	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
70400.	0.0571	0.2390	4.1846	20.2005	26.8669	573.1976
70500.	0.0568	0.2384	4.1947	20.2979	26.9963	573.1976
70600.	0.0566	0.2379	4.2048	20.3956	27.1264	573.1976
70700.	0.0563	0.2373	4.2149	20.4939	27.2571	573.1976
70800.	0.0560	0.2367	4.2251	20.5926	27.3884	573.1976
70900.	0.0558	0.2361	4.2352	20.6913	27.5203	573.1976
71000.	0.0555	0.2355	4.2454	20.7915	27.6529	573.1976
71100.	0.0552	0.2350	4.2556	20.8917	27.7861	573.1976
71200.	0.0550	0.2344	4.2659	20.9923	27.9200	573.1976
71300.	0.0547	0.2339	4.2761	21.0935	28.0545	573.1976
71400.	0.0544	0.2333	4.2864	21.1951	28.1897	573.1976
71500.	0.0542	0.2327	4.2967	21.2972	28.3255	573.1976
71600.	0.0539	0.2322	4.3071	21.3998	28.4620	573.1976
71700.	0.0536	0.2316	4.3174	21.5029	28.5991	573.1976
71800.	0.0534	0.2311	4.3278	21.6065	28.7369	573.1976
71900.	0.0531	0.2305	4.3382	21.7106	28.8754	573.1976
72000.	0.0529	0.2300	4.3487	21.8152	29.0145	573.1976
72100.	0.0526	0.2294	4.3591	21.9203	29.1543	573.1976
72200.	0.0524	0.2289	4.3696	22.0259	29.2947	573.1976
72300.	0.0521	0.2283	4.3801	22.1321	29.4359	573.1976
72400.	0.0519	0.2278	4.3907	22.2387	29.5777	573.1976
72500.	0.0516	0.2272	4.4012	22.3458	29.7202	573.1976
72600.	0.0514	0.2267	4.4118	22.4535	29.8634	573.1976
72700.	0.0511	0.2261	4.4225	22.5617	30.0073	573.1976
72800.	0.0509	0.2256	4.4331	22.6704	30.1518	573.1976
72900.	0.0506	0.2250	4.4438	22.7796	30.2971	573.1976
73000.	0.0504	0.2245	4.4545	22.8893	30.4431	573.1976
73100.	0.0502	0.2240	4.4652	22.9996	30.5897	573.1976
73200.	0.0499	0.2234	4.4759	23.1104	30.7371	573.1976
73300.	0.0497	0.2229	4.4867	23.2219	30.8852	573.1976
73400.	0.0494	0.2223	4.4975	23.3337	31.0340	573.1976
73500.	0.0492	0.2218	4.5083	23.4461	31.1835	573.1976
73600.	0.0490	0.2213	4.5191	23.5590	31.3339	573.1976
73700.	0.0487	0.2207	4.5300	23.6725	31.4847	573.1976
73800.	0.0485	0.2202	4.5409	23.7866	31.6364	573.1976
73900.	0.0483	0.2197	4.5518	23.9012	31.7898	573.1976
74000.	0.0480	0.2192	4.5628	24.0164	31.9420	573.1976
74100.	0.0479	0.2186	4.5738	24.1321	32.0959	573.1976
74200.	0.0476	0.2181	4.5848	24.2483	32.2505	573.1976
74300.	0.0473	0.2175	4.5958	24.3652	32.4059	573.1976
74400.	0.0471	0.2171	4.6069	24.4825	32.5610	573.1976
74500.	0.0469	0.2165	4.6180	24.6005	32.7169	573.1976

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ ("K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
74600.	1.050	0.0351	28.5075	216.66	14.719	0.7519	0.8671
74700.	1.045	0.0347	28.6448	216.66	14.719	0.7519	0.8671
74800.	1.040	0.0347	28.7828	216.66	14.719	0.7519	0.8671
74900.	1.035	0.0346	28.9215	216.66	14.719	0.7519	0.8671
75000.	1.030	0.0344	29.0609	216.66	14.719	0.7519	0.8671
75100.	1.025	0.0342	29.2009	216.66	14.719	0.7519	0.8671
75200.	1.020	0.0341	29.3416	216.66	14.719	0.7519	0.8671
75300.	1.015	0.0339	29.4829	216.66	14.719	0.7519	0.8671
75400.	1.010	0.0338	29.6250	216.66	14.719	0.7519	0.8671
75500.	1.005	0.0336	29.7677	216.66	14.719	0.7519	0.8671
75600.	1.000	0.0334	29.9111	216.66	14.719	0.7519	0.8671
75700.	0.995	0.0333	30.0552	216.66	14.719	0.7519	0.8671
75800.	0.991	0.0331	30.2000	216.66	14.719	0.7519	0.8671
75900.	0.986	0.0330	30.3455	216.66	14.719	0.7519	0.8671
76000.	0.981	0.0328	30.4917	216.66	14.719	0.7519	0.8671
76100.	0.977	0.0326	30.6386	216.66	14.719	0.7519	0.8671
76200.	0.972	0.0325	30.7862	216.66	14.719	0.7519	0.8671
76300.	0.967	0.0323	30.9346	216.66	14.719	0.7519	0.8671
76400.	0.963	0.0322	31.0836	216.66	14.719	0.7519	0.8671
76500.	0.958	0.0320	31.2334	216.66	14.719	0.7519	0.8671
76600.	0.953	0.0319	31.3839	216.66	14.719	0.7519	0.8671
76700.	0.949	0.0317	31.5351	216.66	14.719	0.7519	0.8671
76800.	0.944	0.0316	31.6870	216.66	14.719	0.7519	0.8671
76900.	0.940	0.0314	31.8397	216.66	14.719	0.7519	0.8671
77000.	0.935	0.0313	31.9931	216.66	14.719	0.7519	0.8671
77100.	0.931	0.0311	32.1472	216.66	14.719	0.7519	0.8671
77200.	0.926	0.0310	32.3021	216.66	14.719	0.7519	0.8671
77300.	0.922	0.0308	32.4577	216.66	14.719	0.7519	0.8671
77400.	0.917	0.0307	32.6141	216.66	14.719	0.7519	0.8671
77500.	0.913	0.0305	32.7712	216.66	14.719	0.7519	0.8671
77600.	0.909	0.0304	32.9291	216.66	14.719	0.7519	0.8671
77700.	0.904	0.0302	33.0878	216.66	14.719	0.7519	0.8671
77800.	0.900	0.0301	33.2472	216.66	14.719	0.7519	0.8671
77900.	0.896	0.0299	33.4073	216.66	14.719	0.7519	0.8671
78000.	0.891	0.0298	33.5683	216.66	14.719	0.7519	0.8671
78100.	0.887	0.0296	33.7300	216.66	14.719	0.7519	0.8671
78200.	0.883	0.0295	33.8925	216.66	14.719	0.7519	0.8671
78300.	0.879	0.0294	34.0558	216.66	14.719	0.7519	0.8671
78400.	0.874	0.0292	34.2199	216.66	14.719	0.7519	0.8671
78500.	0.870	0.0291	34.3848	216.66	14.719	0.7519	0.8671
78600.	0.866	0.0289	34.5504	216.66	14.719	0.7519	0.8671
78700.	0.862	0.0298	34.7169	216.66	14.719	0.7519	0.8671

$H_c$ (Feet)	$\sigma$ $p/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\delta}$	$\frac{1}{\delta\sqrt{\sigma}}$	$a$ (Knots)
74600.	0.2467	0.2160	4.6291	24.7190	32.8766	573.1976
74700.	0.2464	0.2155	4.6402	24.8381	33.0350	573.1976
74800.	0.2462	0.2150	4.6514	24.9578	33.1941	573.1976
74900.	0.2460	0.2145	4.6626	25.0780	33.3540	573.1976
75000.	0.2458	0.2140	4.6738	25.1989	33.5147	573.1976
75100.	0.2456	0.2134	4.6850	25.3203	33.6762	573.1976
75200.	0.2453	0.2129	4.6963	25.4423	33.8395	573.1976
75300.	0.2451	0.2124	4.7076	25.5648	34.0015	573.1976
75400.	0.2449	0.2119	4.7189	25.6880	34.1653	573.1976
75500.	0.2447	0.2114	4.7303	25.8118	34.3299	573.1976
75600.	0.2445	0.2109	4.7417	25.9361	34.4953	573.1976
75700.	0.2443	0.2104	4.7531	26.0611	34.6615	573.1976
75800.	0.2441	0.2099	4.7645	26.1866	34.8285	573.1976
75900.	0.2439	0.2094	4.7760	26.3128	34.9963	573.1976
76000.	0.2436	0.2089	4.7875	26.4396	35.1649	573.1976
76100.	0.2434	0.2084	4.7990	26.5670	35.3343	573.1976
76200.	0.2432	0.2079	4.8105	26.6950	35.5046	573.1976
76300.	0.2430	0.2074	4.8221	26.8236	35.6756	573.1976
76400.	0.2428	0.2069	4.8337	26.9528	35.8475	573.1976
76500.	0.2426	0.2064	4.8453	27.0827	36.0202	573.1976
76600.	0.2424	0.2059	4.8570	27.2131	36.1938	573.1976
76700.	0.2422	0.2054	4.8687	27.3443	36.3681	573.1976
76800.	0.2420	0.2049	4.8804	27.4760	36.5434	573.1976
76900.	0.2418	0.2044	4.8921	27.6084	36.7194	573.1976
77000.	0.2416	0.2039	4.9039	27.7414	36.8963	573.1976
77100.	0.2414	0.2034	4.9157	27.8750	37.0741	573.1976
77200.	0.2412	0.2029	4.9275	28.0093	37.2527	573.1976
77300.	0.2410	0.2025	4.9394	28.1443	37.4322	573.1976
77400.	0.2408	0.2020	4.9513	28.2799	37.6125	573.1976
77500.	0.2406	0.2015	4.9632	28.4161	37.7938	573.1976
77600.	0.2404	0.2010	4.9751	28.5530	37.9758	573.1976
77700.	0.2402	0.2005	4.9871	28.6906	38.1598	573.1976
77800.	0.2400	0.2000	4.9991	28.8288	38.3427	573.1976
77900.	0.2398	0.1996	5.0111	29.9677	38.5274	573.1976
78000.	0.2396	0.1991	5.0232	29.1073	38.7130	573.1976
78100.	0.2394	0.1986	5.0353	29.2475	38.8995	573.1976
78200.	0.2393	0.1981	5.0474	29.3884	39.0869	573.1976
78300.	0.2391	0.1976	5.0595	29.5300	39.2753	573.1976
78400.	0.2389	0.1972	5.0717	29.6723	39.4645	573.1976
78500.	0.2387	0.1967	5.0839	29.8153	39.6546	573.1976
78600.	0.2385	0.1962	5.0961	29.9589	39.8457	573.1976
78700.	0.2383	0.1958	5.1084	30.1033	40.0376	573.1976



$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\theta}{P_a/P_{aSL}}$	$\frac{1}{\theta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
78800.	0.858	0.0297	34.8842	216.66	14.719	0.7519	0.8671
78900.	0.854	0.0285	35.0522	216.66	14.719	0.7519	0.8671
79000.	0.850	0.0284	35.2211	216.66	14.719	0.7519	0.8671
79100.	0.845	0.0283	35.3908	216.66	14.719	0.7519	0.8671
79200.	0.841	0.0281	35.5613	216.66	14.719	0.7519	0.8671
79300.	0.837	0.0290	35.7326	216.66	14.719	0.7519	0.8671
79400.	0.833	0.0279	35.9048	216.66	14.719	0.7519	0.8671
79500.	0.829	0.0277	36.0778	216.66	14.719	0.7519	0.8671
79600.	0.825	0.0276	36.2516	216.66	14.719	0.7519	0.8671
79700.	0.821	0.0275	36.4263	216.66	14.719	0.7519	0.8671
79800.	0.817	0.0273	36.6018	216.66	14.719	0.7519	0.8671
79900.	0.814	0.0272	36.7781	216.66	14.719	0.7519	0.8671
80000.	0.810	0.0271	36.9553	216.66	14.719	0.7519	0.8671
80100.	0.806	0.0269	37.1334	216.66	14.719	0.7519	0.8671
80200.	0.802	0.0268	37.3123	216.66	14.719	0.7519	0.8671
80300.	0.798	0.0267	37.4920	216.66	14.719	0.7519	0.8671
80400.	0.794	0.0265	37.6727	216.66	14.719	0.7519	0.8671
80500.	0.790	0.0264	37.8542	216.66	14.719	0.7519	0.8671
80600.	0.787	0.0263	38.0365	216.66	14.719	0.7519	0.8671
80700.	0.783	0.0262	38.2198	216.66	14.719	0.7519	0.8671
80800.	0.779	0.0260	38.4039	216.66	14.719	0.7519	0.8671
80900.	0.775	0.0259	38.5890	216.66	14.719	0.7519	0.8671
81000.	0.772	0.0258	38.7749	216.66	14.719	0.7519	0.8671
81100.	0.768	0.0257	38.9617	216.66	14.719	0.7519	0.8671
81200.	0.764	0.0255	39.1494	216.66	14.719	0.7519	0.8671
81300.	0.761	0.0254	39.3380	216.66	14.719	0.7519	0.8671
81400.	0.757	0.0253	39.5276	216.66	14.719	0.7519	0.8671
81500.	0.753	0.0252	39.7180	216.66	14.719	0.7519	0.8671
81600.	0.750	0.0251	39.9094	216.66	14.719	0.7519	0.8671
81700.	0.746	0.0249	40.1016	216.66	14.719	0.7519	0.8671
81800.	0.743	0.0248	40.2948	216.66	14.719	0.7519	0.8671
81900.	0.739	0.0247	40.4890	216.66	14.719	0.7519	0.8671
82000.	0.735	0.0246	40.6841	216.66	14.719	0.7519	0.8671
82100.	0.732	0.0247	40.5167	216.73	14.722	0.7521	0.8673
82200.	0.735	0.0246	40.7118	216.82	14.725	0.7524	0.8674
82300.	0.731	0.0244	40.9078	216.92	14.728	0.7528	0.8676
82400.	0.728	0.0243	41.1046	217.01	14.731	0.7531	0.8678
82500.	0.724	0.0242	41.3023	217.10	14.734	0.7534	0.8680
82600.	0.721	0.0241	41.5008	217.19	14.737	0.7537	0.8682
82700.	0.714	0.0240	41.7003	217.28	14.740	0.7540	0.8683
82800.	0.714	0.0239	41.9006	217.37	14.744	0.7543	0.8685
82900.	0.711	0.0238	42.1017	217.46	14.747	0.7547	0.8687

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
78800.	0.0381	0.1953	5.1207	30.2483	40.2305	573.1976
78900.	0.0380	0.1948	5.1330	30.3940	40.4244	573.1976
79000.	0.0378	0.1944	5.1454	30.5405	40.6191	573.1976
79100.	0.0376	0.1939	5.1577	30.6876	40.8148	573.1976
79200.	0.0374	0.1934	5.1701	30.8355	41.0115	573.1976
79300.	0.0372	0.1930	5.1826	30.9840	41.2091	573.1976
79400.	0.0371	0.1925	5.1951	31.1333	41.4076	573.1976
79500.	0.0369	0.1920	5.2076	31.2833	41.6071	573.1976
79600.	0.0367	0.1916	5.2201	31.4340	41.8076	573.1976
79700.	0.0365	0.1911	5.2326	31.5855	42.0090	573.1976
79800.	0.0363	0.1906	5.2452	31.7376	42.2114	573.1976
79900.	0.0362	0.1902	5.2579	31.8905	42.4147	573.1976
80000.	0.0360	0.1897	5.2705	32.0442	42.6191	573.1976
80100.	0.0358	0.1893	5.2832	32.1986	42.8244	573.1976
80200.	0.0357	0.1888	5.2959	32.3537	43.0308	573.1976
80300.	0.0355	0.1884	5.3086	32.5096	43.2381	573.1976
80400.	0.0353	0.1879	5.3214	32.6662	43.4464	573.1976
80500.	0.0351	0.1875	5.3342	32.8236	43.6557	573.1976
80600.	0.0350	0.1870	5.3470	32.9817	43.8660	573.1976
80700.	0.0348	0.1866	5.3599	33.1406	44.0774	573.1976
80800.	0.0346	0.1861	5.3728	33.3003	44.2898	573.1976
80900.	0.0345	0.1857	5.3857	33.4607	44.5031	573.1976
81000.	0.0343	0.1852	5.3987	33.6220	44.7175	573.1976
81100.	0.0341	0.1848	5.4117	33.7839	44.9330	573.1976
81200.	0.0340	0.1843	5.4247	33.9467	45.1495	573.1976
81300.	0.0338	0.1839	5.4378	34.1103	45.3670	573.1976
81400.	0.0337	0.1835	5.4508	34.2746	45.5856	573.1976
81500.	0.0335	0.1830	5.4640	34.4397	45.8052	573.1976
81600.	0.0333	0.1826	5.4771	34.6057	46.0259	573.1976
81700.	0.0332	0.1821	5.4903	34.7724	46.2476	573.1976
81800.	0.0330	0.1817	5.5035	34.9399	46.4705	573.1976
81900.	0.0329	0.1813	5.5167	35.1083	46.6943	573.1976
82000.	0.0327	0.1808	5.5300	35.2774	46.9193	573.1976
82100.	0.0325	0.1804	5.5443	35.1382	46.7196	573.2931
82200.	0.0324	0.1799	5.5588	35.3148	46.9376	573.4140
82300.	0.0322	0.1794	5.5734	35.4923	47.1496	573.5349
82400.	0.0320	0.1790	5.5879	35.6706	47.3645	573.6558
82500.	0.0319	0.1785	5.6025	35.8497	47.5842	573.7766
82600.	0.0317	0.1780	5.6172	36.0296	47.8079	573.8975
82700.	0.0315	0.1776	5.6318	36.2104	48.0275	574.0183
82800.	0.0314	0.1771	5.6465	36.3919	48.2430	574.1390
82900.	0.0312	0.1766	5.6613	36.5743	48.4645	574.2598

$H_c$ (Feet)	$P_a$ ( $^{\circ}\text{Hg}$ )	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ ( $^{\circ}\text{K}$ )	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
83000.	0.707	0.0236	42.3038	217.56	14.750	0.7550	0.8689
83100.	0.706	0.0235	42.5067	217.65	14.753	0.7553	0.8691
83200.	0.704	0.0234	42.7105	217.74	14.756	0.7556	0.8693
83300.	0.697	0.0233	42.9153	217.83	14.759	0.7559	0.8694
83400.	0.694	0.0232	43.1209	217.92	14.762	0.7562	0.8696
83500.	0.691	0.0231	43.3274	218.01	14.765	0.7566	0.8698
83600.	0.687	0.0230	43.5348	218.10	14.768	0.7569	0.8700
83700.	0.684	0.0229	43.7431	218.20	14.771	0.7572	0.8702
83800.	0.681	0.0228	43.9523	218.29	14.775	0.7575	0.8704
83900.	0.679	0.0226	44.1625	218.38	14.778	0.7578	0.8705
84000.	0.674	0.0225	44.3735	218.47	14.781	0.7582	0.8707
84100.	0.671	0.0224	44.5855	218.56	14.784	0.7585	0.8709
84200.	0.668	0.0223	44.7984	218.65	14.787	0.7588	0.8711
84300.	0.665	0.0222	45.0122	218.74	14.790	0.7591	0.8713
84400.	0.662	0.0221	45.2269	218.84	14.793	0.7594	0.8714
84500.	0.658	0.0220	45.4426	218.93	14.796	0.7597	0.8716
84600.	0.655	0.0219	45.6592	219.02	14.799	0.7601	0.8718
84700.	0.652	0.0218	45.8768	219.11	14.802	0.7604	0.8720
84800.	0.649	0.0217	46.0953	219.20	14.805	0.7607	0.8722
84900.	0.646	0.0216	46.3148	219.29	14.809	0.7610	0.8724
85000.	0.643	0.0215	46.5352	219.38	14.812	0.7613	0.8725
85100.	0.640	0.0214	46.7566	219.48	14.815	0.7616	0.8727
85200.	0.637	0.0213	46.9789	219.57	14.818	0.7620	0.8729
85300.	0.634	0.0212	47.2022	219.66	14.821	0.7623	0.8731
85400.	0.631	0.0211	47.4264	219.75	14.824	0.7626	0.8733
85500.	0.628	0.0210	47.6517	219.84	14.827	0.7629	0.8734
85600.	0.625	0.0209	47.8779	219.93	14.830	0.7632	0.8736
85700.	0.622	0.0208	48.1051	220.02	14.833	0.7635	0.8738
85800.	0.619	0.0207	48.3332	220.12	14.836	0.7639	0.8740
85900.	0.616	0.0206	48.5624	220.21	14.839	0.7642	0.8742
86000.	0.613	0.0205	48.7925	220.30	14.842	0.7645	0.8744
86100.	0.610	0.0204	49.0237	220.39	14.846	0.7648	0.8745
86200.	0.607	0.0203	49.2558	220.48	14.849	0.7651	0.8747
86300.	0.605	0.0202	49.4890	220.57	14.852	0.7655	0.8749
86400.	0.602	0.0201	49.7231	220.66	14.855	0.7658	0.8751
86500.	0.599	0.0200	49.9583	220.76	14.858	0.7661	0.8753
86600.	0.596	0.0199	50.1945	220.85	14.861	0.7664	0.8754
86700.	0.593	0.0198	50.4316	220.94	14.864	0.7667	0.8756
86800.	0.591	0.0197	50.6698	221.03	14.867	0.7670	0.8758
86900.	0.588	0.0196	50.9091	221.12	14.870	0.7674	0.8760
87000.	0.585	0.0196	51.1494	221.21	14.873	0.7677	0.8762
87100.	0.582	0.0195	51.3907	221.30	14.876	0.7680	0.8764

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{h\sqrt{\theta}}$	$a$ (Knots)
83000.	0.0310	0.1762	5.6760	36.7576	48.6868	574.3805
83100.	0.0309	0.1757	5.6908	36.9417	48.9101	574.5012
83200.	0.0307	0.1751	5.7056	37.1266	49.1343	574.6219
83300.	0.0306	0.1748	5.7205	37.3124	49.3594	574.7425
83400.	0.0304	0.1744	5.7354	37.4990	49.5855	574.8631
83500.	0.0302	0.1739	5.7503	37.6865	49.8125	574.9837
83600.	0.0301	0.1735	5.7653	37.8743	50.0405	575.1043
83700.	0.0299	0.1730	5.7803	38.0641	50.2694	575.2248
83800.	0.0298	0.1726	5.7953	38.2542	50.4993	575.3454
83900.	0.0296	0.1721	5.8103	38.4451	50.7301	575.4659
84000.	0.0295	0.1717	5.8254	38.6369	50.9618	575.5863
84100.	0.0293	0.1712	5.8405	38.8296	51.1946	575.7068
84200.	0.0292	0.1708	5.8557	39.0232	51.4283	575.8272
84300.	0.0290	0.1703	5.8709	39.2176	51.6629	575.9476
84400.	0.0289	0.1699	5.8861	39.4130	51.8986	576.0679
84500.	0.0287	0.1695	5.9013	39.6092	52.1352	576.1883
84600.	0.0286	0.1690	5.9166	39.8063	52.3728	576.3086
84700.	0.0284	0.1686	5.9319	40.0044	52.6113	576.4289
84800.	0.0283	0.1681	5.9473	40.2033	52.8509	576.5492
84900.	0.0281	0.1677	5.9627	40.4031	53.0914	576.6694
85000.	0.0280	0.1673	5.9781	40.6034	53.3330	576.7896
85100.	0.0278	0.1668	5.9935	40.8055	53.5755	576.9098
85200.	0.0277	0.1664	6.0090	41.0091	53.8191	577.0300
85300.	0.0276	0.1660	6.0245	41.2116	54.0636	577.1501
85400.	0.0274	0.1656	6.0401	41.4160	54.3092	577.2702
85500.	0.0273	0.1651	6.0557	41.6213	54.5557	577.3903
85600.	0.0271	0.1647	6.0713	41.8276	54.8033	577.5104
85700.	0.0270	0.1643	6.0870	42.0343	55.0519	577.6304
85800.	0.0269	0.1639	6.1026	42.2430	55.3016	577.7505
85900.	0.0267	0.1634	6.1184	42.4521	55.5522	577.8704
86000.	0.0266	0.1630	6.1341	42.6621	55.8039	577.9904
86100.	0.0264	0.1626	6.1499	42.8731	56.0566	578.1104
86200.	0.0263	0.1622	6.1657	43.0851	56.3104	578.2303
86300.	0.0262	0.1618	6.1816	43.2980	56.5652	578.3502
86400.	0.0260	0.1614	6.1975	43.5113	56.8211	578.4700
86500.	0.0259	0.1609	6.2134	43.7267	57.0780	578.5899
86600.	0.0258	0.1605	6.2294	43.9425	57.3359	578.7097
86700.	0.0256	0.1601	6.2453	44.1593	57.5949	578.8295
86800.	0.0255	0.1597	6.2614	44.3770	57.8550	578.9492
86900.	0.0254	0.1593	6.2774	44.5958	58.1161	579.0690
87000.	0.0252	0.1589	6.2935	44.8155	58.3784	579.1887
87100.	0.0251	0.1585	6.3097	45.0363	58.6417	579.3084

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
87200.	0.579	0.0194	51.6330	221.40	14.879	0.7693	0.8765
87300.	0.577	0.0193	51.8764	221.49	14.882	0.7686	0.8767
87400.	0.574	0.0192	52.1208	221.58	14.886	0.7689	0.8769
87500.	0.571	0.0191	52.3663	221.67	14.889	0.7693	0.8771
87600.	0.569	0.0190	52.6128	221.76	14.892	0.7696	0.8773
87700.	0.566	0.0189	52.8604	221.85	14.895	0.7699	0.8774
87800.	0.563	0.0188	53.1091	221.94	14.898	0.7702	0.8776
87900.	0.561	0.0187	53.3588	222.04	14.901	0.7705	0.8778
88000.	0.559	0.0187	53.6096	222.13	14.904	0.7708	0.8780
88100.	0.556	0.0186	53.8614	222.22	14.907	0.7712	0.8782
88200.	0.553	0.0185	54.1144	222.31	14.910	0.7715	0.8783
88300.	0.550	0.0184	54.3684	222.40	14.913	0.7718	0.8785
88400.	0.548	0.0183	54.6235	222.49	14.916	0.7721	0.8787
88500.	0.545	0.0182	54.8797	222.58	14.919	0.7724	0.8789
88600.	0.543	0.0181	55.1370	222.68	14.922	0.7728	0.8791
88700.	0.540	0.0181	55.3954	222.77	14.925	0.7731	0.8792
88800.	0.538	0.0180	55.6549	222.86	14.928	0.7734	0.8794
88900.	0.535	0.0179	55.9156	222.95	14.932	0.7737	0.8796
89000.	0.533	0.0178	56.1773	223.04	14.935	0.7740	0.8798
89100.	0.530	0.0177	56.4401	223.13	14.938	0.7743	0.8800
89200.	0.529	0.0176	56.7041	223.22	14.941	0.7747	0.8801
89300.	0.525	0.0176	56.9692	223.32	14.944	0.7750	0.8803
89400.	0.523	0.0175	57.2354	223.41	14.947	0.7753	0.8805
89500.	0.520	0.0174	57.5028	223.50	14.950	0.7756	0.8807
89600.	0.518	0.0173	57.7713	223.59	14.953	0.7759	0.8809
89700.	0.516	0.0172	58.0409	223.68	14.956	0.7762	0.8810
89800.	0.513	0.0171	58.3117	223.77	14.959	0.7766	0.8812
89900.	0.511	0.0171	58.5836	223.86	14.962	0.7769	0.8814
90000.	0.509	0.0170	58.8567	223.96	14.965	0.7772	0.8816
90100.	0.506	0.0169	59.1310	224.05	14.968	0.7775	0.8818
90200.	0.504	0.0168	59.4064	224.14	14.971	0.7778	0.8819
90300.	0.501	0.0168	59.6830	224.23	14.974	0.7781	0.8821
90400.	0.499	0.0167	59.9607	224.32	14.977	0.7785	0.8823
90500.	0.497	0.0166	60.2397	224.41	14.980	0.7788	0.8825
90600.	0.494	0.0165	60.5198	224.50	14.983	0.7791	0.8827
90700.	0.492	0.0164	60.8011	224.60	14.987	0.7794	0.8828
90800.	0.490	0.0164	61.0836	224.69	14.990	0.7797	0.8830
90900.	0.488	0.0163	61.3673	224.78	14.993	0.7800	0.8832
91000.	0.485	0.0162	61.6522	224.87	14.996	0.7804	0.8834
91100.	0.483	0.0161	61.9383	224.96	14.999	0.7807	0.8836
91200.	0.481	0.0161	62.2257	225.05	15.002	0.7810	0.8837
91300.	0.479	0.0160	62.5142	225.14	15.005	0.7813	0.8839

$H_c$ (Feet)	$\sigma$ $p/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
87200.	0.0250	0.1581	6.3258	45.2580	58.9060	579.4281
87300.	0.0249	0.1577	6.3420	45.4807	59.1715	579.5477
87400.	0.0247	0.1573	6.3583	45.7044	59.4390	579.6673
87500.	0.0246	0.1569	6.3745	45.9292	59.7056	579.7869
87600.	0.0245	0.1565	6.3908	46.1549	59.9743	579.9065
87700.	0.0244	0.1561	6.4072	46.3817	60.2441	580.0260
87800.	0.0242	0.1557	6.4236	46.6094	60.5151	580.1456
87900.	0.0241	0.1553	6.4400	46.8382	60.7871	580.2651
88000.	0.0240	0.1549	6.4564	47.0681	61.0602	580.3845
88100.	0.0239	0.1545	6.4729	47.2987	61.3345	580.5040
88200.	0.0237	0.1541	6.4894	47.5303	61.6098	580.6234
88300.	0.0236	0.1537	6.5060	47.7639	61.8863	580.7428
88400.	0.0235	0.1533	6.5225	47.9978	62.1639	580.8622
88500.	0.0234	0.1529	6.5392	48.2328	62.4427	580.9815
88600.	0.0233	0.1525	6.5558	48.4689	62.7225	581.1009
88700.	0.0231	0.1521	6.5725	48.7060	63.0036	581.2201
88800.	0.0230	0.1518	6.5893	48.9443	63.2857	581.3394
88900.	0.0229	0.1514	6.6060	49.1835	63.5690	581.4587
89000.	0.0228	0.1510	6.6228	49.4239	63.8535	581.5779
89100.	0.0227	0.1506	6.6397	49.6653	64.1391	581.6971
89200.	0.0226	0.1502	6.6565	49.9078	64.4259	581.8163
89300.	0.0225	0.1498	6.6734	50.1514	64.7138	581.9354
89400.	0.0223	0.1495	6.6904	50.3961	65.0029	582.0546
89500.	0.0222	0.1491	6.7074	50.6418	65.2932	582.1737
89600.	0.0221	0.1487	6.7244	50.8887	65.5847	582.2927
89700.	0.0220	0.1483	6.7414	51.1367	65.8773	582.4118
89800.	0.0219	0.1480	6.7585	51.3858	66.1711	582.5308
89900.	0.0218	0.1476	6.7756	51.6359	66.4661	582.6498
90000.	0.0217	0.1472	6.7928	51.8872	66.7623	582.7688
90100.	0.0216	0.1468	6.8100	52.1396	67.0597	582.8878
90200.	0.0215	0.1465	6.8272	52.3932	67.3583	583.0067
90300.	0.0213	0.1461	6.8445	52.6479	67.6592	583.1256
90400.	0.0212	0.1457	6.8618	52.9037	67.9622	583.2445
90500.	0.0211	0.1454	6.8792	53.1606	68.2614	583.3634
90600.	0.0210	0.1450	6.8965	53.4187	68.5649	583.4822
90700.	0.0209	0.1446	6.9140	53.6779	68.8696	583.6010
90800.	0.0208	0.1443	6.9314	53.9383	69.1755	583.7198
90900.	0.0207	0.1439	6.9489	54.1999	69.4826	583.8386
91000.	0.0206	0.1435	6.9664	54.4626	69.7910	583.9573
91100.	0.0205	0.1432	6.9840	54.7264	70.1006	584.0760
91200.	0.0204	0.1428	7.0016	54.9915	70.4115	584.1947
91300.	0.0203	0.1425	7.0192	55.2577	70.7236	584.3134

$H_c$ (Feet)	$P_a$ (inHg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
91400.	0.476	0.0159	62.8040	225.24	15.008	0.7816	0.8841
91500.	0.475	0.0158	63.0949	225.33	15.011	0.7820	0.8843
91600.	0.474	0.0158	63.3871	225.42	15.014	0.7823	0.8845
91700.	0.473	0.0157	63.6806	225.51	15.017	0.7826	0.8846
91800.	0.472	0.0156	63.9753	225.60	15.020	0.7829	0.8848
91900.	0.471	0.0156	64.2712	225.69	15.023	0.7832	0.8850
92000.	0.470	0.0155	64.5684	225.78	15.026	0.7835	0.8852
92100.	0.469	0.0154	64.8668	225.88	15.029	0.7839	0.8854
92200.	0.468	0.0153	65.1665	225.97	15.032	0.7842	0.8855
92300.	0.467	0.0153	65.4674	226.06	15.035	0.7845	0.8857
92400.	0.466	0.0152	65.7696	226.15	15.038	0.7848	0.8859
92500.	0.465	0.0151	66.0731	226.24	15.041	0.7851	0.8861
92600.	0.464	0.0151	66.3779	226.33	15.044	0.7854	0.8863
92700.	0.463	0.0150	66.6839	226.42	15.047	0.7858	0.8864
92800.	0.462	0.0149	66.9913	226.52	15.050	0.7861	0.8866
92900.	0.461	0.0149	67.2999	226.61	15.053	0.7864	0.8868
93000.	0.460	0.0148	67.6098	226.70	15.057	0.7867	0.8870
93100.	0.459	0.0147	67.9210	226.79	15.060	0.7870	0.8871
93200.	0.458	0.0147	68.2336	226.88	15.063	0.7873	0.8873
93300.	0.457	0.0146	68.5474	226.97	15.066	0.7877	0.8875
93400.	0.456	0.0145	68.8625	227.06	15.069	0.7880	0.8877
93500.	0.455	0.0145	69.1790	227.16	15.072	0.7883	0.8879
93600.	0.454	0.0144	69.4968	227.25	15.075	0.7886	0.8880
93700.	0.453	0.0143	69.8160	227.34	15.078	0.7889	0.8882
93800.	0.452	0.0143	70.1364	227.43	15.081	0.7893	0.8884
93900.	0.451	0.0142	70.4582	227.52	15.084	0.7896	0.8886
94000.	0.450	0.0141	70.7814	227.61	15.087	0.7899	0.8888
94100.	0.449	0.0141	71.1059	227.71	15.090	0.7902	0.8889
94200.	0.448	0.0140	71.4318	227.80	15.093	0.7905	0.8891
94300.	0.447	0.0139	71.7590	227.89	15.096	0.7908	0.8893
94400.	0.446	0.0139	72.0876	227.98	15.099	0.7912	0.8895
94500.	0.445	0.0138	72.4176	228.07	15.102	0.7915	0.8896
94600.	0.444	0.0137	72.7489	228.16	15.105	0.7918	0.8898
94700.	0.443	0.0137	73.0816	228.25	15.108	0.7921	0.8900
94800.	0.442	0.0136	73.4157	228.35	15.111	0.7924	0.8902
94900.	0.441	0.0136	73.7512	228.44	15.114	0.7927	0.8904
95000.	0.440	0.0135	74.0881	228.53	15.117	0.7931	0.8905
95100.	0.439	0.0134	74.4265	228.62	15.120	0.7934	0.8907
95200.	0.438	0.0134	74.7662	228.71	15.123	0.7937	0.8909
95300.	0.437	0.0133	75.1073	228.80	15.126	0.7940	0.8911
95400.	0.436	0.0133	75.4498	228.89	15.129	0.7943	0.8913
95500.	0.435	0.0132	75.7938	228.99	15.132	0.7946	0.8914

$H_c$ (Feet)	$\sigma$ $\rho/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\theta}$	$\frac{1}{\Delta\sqrt{\sigma}}$	$a$ (Knots)
91400.	0.0202	0.1421	7.0369	55.5251	71.0370	584.4320
91500.	0.0201	0.1418	7.0546	55.7937	71.3517	584.5507
91600.	0.0200	0.1414	7.0724	56.0634	71.6676	584.6693
91700.	0.0199	0.1410	7.0902	56.3344	71.9848	584.7878
91800.	0.0198	0.1407	7.1080	56.6065	72.3032	584.9064
91900.	0.0197	0.1403	7.1259	56.8799	72.6229	585.0249
92000.	0.0196	0.1400	7.1438	57.1545	72.9440	585.1434
92100.	0.0195	0.1396	7.1617	57.4303	73.2662	585.2619
92200.	0.0194	0.1393	7.1797	57.7073	73.5899	585.3803
92300.	0.0193	0.1389	7.1977	57.9855	73.9147	585.4988
92400.	0.0192	0.1386	7.2157	58.2650	74.2409	585.6172
92500.	0.0191	0.1382	7.2338	58.5456	74.5684	585.7355
92600.	0.0190	0.1379	7.2520	58.8276	74.8973	585.8539
92700.	0.0189	0.1375	7.2701	59.1107	75.2274	585.9722
92800.	0.0188	0.1372	7.2883	59.3952	75.5588	586.0905
92900.	0.0187	0.1369	7.3066	59.6808	75.8916	586.2088
93000.	0.0186	0.1365	7.3249	59.9679	76.2257	586.3271
93100.	0.0185	0.1362	7.3432	60.2560	76.5612	586.4453
93200.	0.0185	0.1358	7.3615	60.5454	76.8979	586.5635
93300.	0.0184	0.1355	7.3799	60.8361	77.2361	586.6817
93400.	0.0183	0.1352	7.3984	61.1282	77.5755	586.7999
93500.	0.0182	0.1348	7.4168	61.4215	77.9164	586.9180
93600.	0.0181	0.1345	7.4354	61.7160	78.2586	587.0361
93700.	0.0180	0.1342	7.4539	62.0119	78.6021	587.1542
93800.	0.0179	0.1338	7.4725	62.3091	78.9470	587.2723
93900.	0.0178	0.1335	7.4911	62.6076	79.2933	587.3904
94000.	0.0177	0.1332	7.5098	62.9074	79.6410	587.5084
94100.	0.0176	0.1328	7.5285	63.2084	79.9901	587.6264
94200.	0.0176	0.1325	7.5472	63.5109	80.3405	587.7444
94300.	0.0175	0.1322	7.5660	63.8146	80.6924	587.8623
94400.	0.0174	0.1318	7.5849	64.1197	81.0456	587.9802
94500.	0.0173	0.1315	7.6037	64.4261	81.4003	588.0981
94600.	0.0172	0.1312	7.6226	64.7338	81.7563	588.2160
94700.	0.0171	0.1309	7.6416	65.0429	82.1138	588.3339
94800.	0.0170	0.1305	7.6605	65.3534	82.4727	588.4517
94900.	0.0170	0.1302	7.6796	65.6652	82.8330	588.5695
95000.	0.0169	0.1299	7.6986	65.9784	83.1947	588.6873
95100.	0.0168	0.1296	7.7177	66.2929	83.5579	588.8051
95200.	0.0167	0.1293	7.7369	66.6088	83.9225	588.9228
95300.	0.0166	0.1289	7.7561	66.9261	84.2886	589.0405
95400.	0.0165	0.1286	7.7753	67.2448	84.6561	589.1582
95500.	0.0165	0.1283	7.7945	67.5648	85.0251	589.2759



$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\rho}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
95600.	0.393	0.0131	76.1392	229.08	15.135	0.7950	0.8916
95700.	0.391	0.0131	76.4861	229.17	15.138	0.7953	0.8918
95800.	0.389	0.0130	76.8343	229.26	15.141	0.7956	0.8920
95900.	0.388	0.0130	77.1841	229.35	15.144	0.7959	0.8921
96000.	0.386	0.0129	77.5352	229.44	15.147	0.7962	0.8923
96100.	0.384	0.0128	77.8879	229.53	15.150	0.7965	0.8925
96200.	0.382	0.0128	78.2420	229.63	15.153	0.7969	0.8927
96300.	0.381	0.0127	78.5975	229.72	15.156	0.7972	0.8929
96400.	0.379	0.0127	78.9546	229.81	15.159	0.7975	0.8930
96500.	0.377	0.0126	79.3131	229.90	15.162	0.7978	0.8932
96600.	0.376	0.0126	79.6731	229.99	15.165	0.7981	0.8934
96700.	0.374	0.0125	80.0346	230.08	15.168	0.7985	0.8936
96800.	0.372	0.0124	80.3976	230.17	15.171	0.7988	0.8937
96900.	0.370	0.0124	80.7620	230.27	15.174	0.7991	0.8939
97000.	0.369	0.0123	81.1280	230.36	15.178	0.7994	0.8941
97100.	0.367	0.0123	81.4955	230.45	15.181	0.7997	0.8943
97200.	0.365	0.0122	81.8646	230.54	15.184	0.8000	0.8944
97300.	0.364	0.0122	82.2351	230.63	15.187	0.8004	0.8946
97400.	0.362	0.0121	82.6072	230.72	15.190	0.8007	0.8948
97500.	0.361	0.0121	82.9808	230.81	15.193	0.8010	0.8950
97600.	0.359	0.0120	83.3560	230.91	15.196	0.8013	0.8952
97700.	0.357	0.0119	83.7327	231.00	15.199	0.8016	0.8953
97800.	0.356	0.0119	84.1109	231.09	15.202	0.8019	0.8955
97900.	0.354	0.0118	84.4907	231.18	15.205	0.8023	0.8957
98000.	0.353	0.0118	84.8721	231.27	15.208	0.8026	0.8959
98100.	0.351	0.0117	85.2550	231.36	15.211	0.8029	0.8960
98200.	0.349	0.0117	85.6396	231.45	15.214	0.8032	0.8962
98300.	0.348	0.0116	86.0257	231.55	15.217	0.8035	0.8964
98400.	0.346	0.0116	86.4133	231.64	15.220	0.8038	0.8966
98500.	0.345	0.0115	86.8026	231.73	15.223	0.8042	0.8968
98600.	0.343	0.0115	87.1935	231.82	15.226	0.8045	0.8969
98700.	0.342	0.0114	87.5860	231.91	15.229	0.8048	0.8971
98800.	0.340	0.0114	87.9801	232.00	15.232	0.8051	0.8973
98900.	0.339	0.0113	88.3758	232.09	15.235	0.8054	0.8975
99000.	0.337	0.0113	88.7731	232.19	15.238	0.8058	0.8976
99100.	0.336	0.0112	89.1721	232.28	15.241	0.8061	0.8978
99200.	0.334	0.0112	89.5727	232.37	15.244	0.8064	0.8980
99300.	0.333	0.0111	89.9749	232.46	15.247	0.8067	0.8982
99400.	0.331	0.0111	90.3788	232.55	15.250	0.8070	0.8983
99500.	0.330	0.0110	90.7843	232.64	15.253	0.8073	0.8985
99600.	0.328	0.0110	91.1916	232.73	15.256	0.8077	0.8987
99700.	0.327	0.0109	91.6004	232.83	15.259	0.8080	0.8989

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{\lambda\sqrt{\theta}}$	$a$ (Knots)
95600.	0.0164	0.1280	7.8138	67.8863	85.3955	589.3935
95700.	0.0163	0.1277	7.8332	68.2091	85.7674	589.5111
95800.	0.0162	0.1273	7.8526	68.5334	86.1407	589.6287
95900.	0.0161	0.1270	7.8720	68.8591	86.5156	589.7463
96000.	0.0161	0.1267	7.8914	69.1861	86.8919	589.8639
96100.	0.0160	0.1264	7.9109	69.5146	87.2697	589.9814
96200.	0.0159	0.1261	7.9305	69.8446	87.6489	590.0989
96300.	0.0158	0.1258	7.9501	70.1760	88.0297	590.2164
96400.	0.0157	0.1255	7.9697	70.5088	88.4120	590.3339
96500.	0.0157	0.1252	7.9893	70.8430	88.7958	590.4513
96600.	0.0156	0.1249	8.0090	71.1787	89.1811	590.5687
96700.	0.0155	0.1246	8.0298	71.5159	89.5680	590.6861
96800.	0.0154	0.1242	8.0486	71.8545	89.9563	590.8034
96900.	0.0154	0.1239	8.0684	72.1946	90.3462	590.9208
97000.	0.0153	0.1236	8.0883	72.5362	90.7376	591.0381
97100.	0.0152	0.1233	8.1082	72.8792	91.1306	591.1554
97200.	0.0151	0.1230	8.1281	73.2237	91.5250	591.2727
97300.	0.0151	0.1227	8.1481	73.5698	91.9211	591.3899
97400.	0.0150	0.1224	8.1681	73.9173	92.3187	591.5071
97500.	0.0149	0.1221	8.1882	74.2663	92.7179	591.6243
97600.	0.0148	0.1218	8.2083	74.6168	93.1186	591.7415
97700.	0.0148	0.1215	8.2285	74.9689	93.5209	591.8587
97800.	0.0147	0.1212	8.2487	75.3225	93.9248	591.9758
97900.	0.0146	0.1209	8.2689	75.6775	94.3302	592.0929
98000.	0.0146	0.1206	8.2892	76.0342	94.7373	592.2100
98100.	0.0145	0.1203	8.3095	76.3923	95.1459	592.3271
98200.	0.0144	0.1200	8.3299	76.7521	95.5562	592.4441
98300.	0.0143	0.1198	8.3503	77.1133	95.9680	592.5611
98400.	0.0143	0.1195	8.3707	77.4761	96.3815	592.6781
98500.	0.0142	0.1192	8.3912	77.8405	96.7966	592.7951
98600.	0.0141	0.1189	8.4118	78.2064	97.2133	592.9120
98700.	0.0141	0.1186	8.4323	78.5740	97.6316	593.0290
98800.	0.0140	0.1183	8.4529	78.9431	98.0516	593.1459
98900.	0.0139	0.1180	8.4736	79.3139	98.4732	593.2627
99000.	0.0139	0.1177	8.4943	79.6860	98.8964	593.3796
99100.	0.0138	0.1174	8.5150	80.0599	99.3214	593.4964
99200.	0.0137	0.1172	8.5358	80.4354	99.7479	593.6132
99300.	0.0137	0.1169	8.5567	80.8125	100.1761	593.7300
99400.	0.0136	0.1166	8.5775	81.1912	100.6060	593.8468
99500.	0.0135	0.1163	8.5984	81.5716	101.0376	593.9635
99600.	0.0135	0.1160	8.6194	81.9536	101.4709	594.0802
99700.	0.0134	0.1157	8.6404	82.3372	101.9058	594.1969

$H_c$ (feet)	$P_s$ (mmHg)	$\delta$ $P_s/P_{sSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
97800.	0.325	0.0109	92.0109	232.92	15.262	0.8083	0.8991
99900.	0.324	0.0108	92.4232	233.01	15.265	0.8086	0.8992
100000.	0.322	0.0108	92.8371	233.10	15.268	0.8089	0.8994
100100.	0.321	0.0107	93.2527	233.19	15.271	0.8092	0.8996
100200.	0.319	0.0107	93.6699	233.28	15.274	0.8096	0.8998
100300.	0.318	0.0106	94.0889	233.37	15.277	0.8099	0.8999
100400.	0.317	0.0106	94.5096	233.47	15.280	0.8102	0.9001
100500.	0.315	0.0105	94.9320	233.56	15.283	0.8105	0.9003
100600.	0.314	0.0105	95.3562	233.65	15.286	0.8108	0.9005
100700.	0.312	0.0104	95.7820	233.74	15.289	0.8111	0.9006
100800.	0.311	0.0104	96.2096	233.83	15.292	0.8115	0.9008
100900.	0.310	0.0103	96.6389	233.92	15.295	0.8118	0.9010
101000.	0.309	0.0103	97.0700	234.01	15.298	0.8121	0.9012
101100.	0.307	0.0103	97.5029	234.11	15.301	0.8124	0.9013
101200.	0.306	0.0102	97.9375	234.20	15.304	0.8127	0.9015
101300.	0.304	0.0102	98.3738	234.29	15.306	0.8131	0.9017
101400.	0.303	0.0101	98.8120	234.38	15.309	0.8134	0.9019
101500.	0.301	0.0101	99.2519	234.47	15.312	0.8137	0.9020
101600.	0.300	0.0100	99.6936	234.56	15.315	0.8140	0.9022
101700.	0.299	0.0100	100.1371	234.65	15.318	0.8143	0.9024
101800.	0.297	0.0099	100.5823	234.75	15.321	0.8146	0.9026
101900.	0.296	0.0099	101.0295	234.84	15.324	0.8150	0.9027
102000.	0.295	0.0099	101.4784	234.93	15.327	0.8153	0.9029
102100.	0.294	0.0098	101.9291	235.02	15.330	0.8156	0.9031
102200.	0.292	0.0098	102.3816	235.11	15.333	0.8159	0.9033
102300.	0.291	0.0097	102.8360	235.20	15.336	0.8162	0.9035
102400.	0.290	0.0097	103.2922	235.29	15.339	0.8165	0.9036
102500.	0.288	0.0096	103.7503	235.39	15.342	0.8169	0.9038
102600.	0.287	0.0096	104.2102	235.48	15.345	0.8172	0.9040
102700.	0.286	0.0096	104.6720	235.57	15.348	0.8175	0.9042
102800.	0.285	0.0095	105.1357	235.66	15.351	0.8178	0.9043
102900.	0.283	0.0095	105.6012	235.75	15.354	0.8181	0.9045
103000.	0.282	0.0094	106.0686	235.84	15.357	0.8184	0.9047
103100.	0.281	0.0094	106.5379	235.93	15.360	0.8188	0.9049
103200.	0.280	0.0093	107.0090	236.03	15.363	0.8191	0.9050
103300.	0.278	0.0093	107.4821	236.12	15.366	0.8194	0.9052
103400.	0.277	0.0093	107.9571	236.21	15.369	0.8197	0.9054
103500.	0.276	0.0092	108.4340	236.30	15.372	0.8200	0.9056
103600.	0.275	0.0092	108.9128	236.39	15.375	0.8203	0.9057
103700.	0.274	0.0091	109.3936	236.48	15.378	0.8207	0.9059
103800.	0.272	0.0091	109.8763	236.57	15.381	0.8210	0.9061
103900.	0.271	0.0091	110.3609	236.67	15.384	0.8213	0.9063

$H_0$ (Feet)	$\frac{1}{\sqrt{H_0}}$ (ft/ft)	$\frac{1}{\sqrt{H_0}}$ (ft/ft)	$\frac{1}{\sqrt{H_0}}$ (ft/ft)	$\frac{1}{\sqrt{H_0}}$ (ft/ft)	$\frac{1}{\sqrt{H_0}}$ (ft/ft)	$a$ (Knots)
9700.0	0.0101	0.111	8.6619	82.7224	102.3424	594.3131
9800.0	0.0101	0.111	8.6621	83.1093	102.7800	594.4301
9900.0	0.0101	0.111	8.7032	83.4977	103.2220	594.5467
10000.0	0.0101	0.1114	8.7248	83.8882	103.6625	594.6635
10100.0	0.0101	0.1114	8.7467	84.2801	104.1061	594.7801
10200.0	0.0101	0.1114	8.7677	84.6735	104.5513	594.8966
10300.0	0.0101	0.1114	8.7886	85.0680	104.9980	595.0131
10400.0	0.0101	0.1115	8.8097	85.4658	105.4467	595.1297
10500.0	0.0101	0.1115	8.8313	85.8669	105.8971	595.2461
10600.0	0.0101	0.1115	8.8527	86.2644	106.3492	595.3627
10700.0	0.0101	0.1115	8.8742	86.6669	106.8031	595.4790
10800.0	0.0101	0.1116	8.8957	87.0706	107.2587	595.5955
10900.0	0.0101	0.1116	8.9173	87.4761	107.7161	595.7119
11000.0	0.0101	0.1116	8.9389	87.8834	108.1753	595.8282
11100.0	0.0101	0.1116	8.9606	88.2923	108.6362	595.9446
11200.0	0.0101	0.1117	8.9822	88.7030	109.0992	596.0609
11300.0	0.0101	0.1117	9.0040	89.1155	109.5635	596.1772
11400.0	0.0101	0.1117	9.0258	89.5297	110.0298	596.2935
11500.0	0.0101	0.1117	9.0476	89.9456	110.4979	596.4098
11600.0	0.0101	0.1118	9.0695	90.3634	110.9679	596.5260
11700.0	0.0101	0.1118	9.0914	90.7820	111.4396	596.6422
11800.0	0.0101	0.1118	9.1133	91.2042	111.9132	596.7584
11900.0	0.0101	0.1118	9.1353	91.6273	112.3886	596.8746
12000.0	0.0101	0.1119	9.1574	92.0521	112.8658	596.9907
12100.0	0.0101	0.1119	9.1795	92.4788	113.3448	597.1069
12200.0	0.0101	0.1119	9.2016	92.9073	113.8258	597.2230
12300.0	0.0101	0.1119	9.2238	93.3376	114.3089	597.3390
12400.0	0.0101	0.1119	9.2460	93.7696	114.7931	597.4551
12500.0	0.0101	0.1119	9.2683	94.2037	115.2776	597.5711
12600.0	0.0101	0.1119	9.2906	94.6396	115.7680	597.6871
12700.0	0.0101	0.1119	9.3130	95.0772	116.2582	597.8031
12800.0	0.0101	0.1119	9.3354	95.5167	116.7503	597.9191
12900.0	0.0101	0.1119	9.3578	95.9581	117.2444	598.0351
13000.0	0.0101	0.1119	9.3803	96.4013	117.7403	598.1510
13100.0	0.0101	0.1119	9.4029	96.8464	118.2381	598.2669
13200.0	0.0101	0.1119	9.4254	97.2934	118.7378	598.3826
13300.0	0.0101	0.1119	9.4481	97.7423	119.2394	598.4986
13400.0	0.0101	0.1119	9.4708	98.1931	119.7430	598.6144
13500.0	0.0101	0.1119	9.4935	98.6458	120.2485	598.7302
13600.0	0.0101	0.1119	9.5162	99.1003	120.7559	598.8460
13700.0	0.0101	0.1119	9.5391	99.5569	121.2653	598.9618
13800.0	0.0101	0.1119	9.5619	100.0153	121.7766	599.0775

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
104000.	0.270	0.0090	110.8475	236.76	15.387	0.8216	0.9064
104100.	0.269	0.0090	111.3360	236.85	15.390	0.8219	0.9066
104200.	0.268	0.0089	111.8265	236.94	15.393	0.8223	0.9068
104300.	0.266	0.0089	112.3190	237.03	15.396	0.8226	0.9070
104400.	0.265	0.0089	112.8134	237.12	15.399	0.8229	0.9071
104500.	0.264	0.0088	113.3098	237.21	15.402	0.8232	0.9073
104600.	0.263	0.0088	113.8082	237.31	15.405	0.8235	0.9075
104700.	0.262	0.0087	114.3087	237.40	15.408	0.8238	0.9077
104800.	0.261	0.0087	114.8111	237.49	15.411	0.8242	0.9078
104900.	0.259	0.0087	115.3155	237.58	15.414	0.8245	0.9080
105000.	0.258	0.0086	115.8220	237.67	15.417	0.8248	0.9082
105100.	0.257	0.0086	116.3305	237.76	15.420	0.8251	0.9084
105200.	0.256	0.0086	116.8410	237.85	15.423	0.8254	0.9085
105300.	0.255	0.0085	117.3535	237.95	15.426	0.8257	0.9087
105400.	0.254	0.0085	117.8682	238.04	15.428	0.8261	0.9089
105500.	0.253	0.0084	118.3848	238.13	15.431	0.8264	0.9091
105600.	0.252	0.0084	118.9036	238.22	15.434	0.8267	0.9092
105700.	0.251	0.0084	119.4244	238.31	15.437	0.8270	0.9094
105800.	0.249	0.0083	119.9473	238.40	15.440	0.8273	0.9096
105900.	0.248	0.0083	120.4723	238.49	15.443	0.8276	0.9098
106000.	0.247	0.0083	120.9993	238.59	15.446	0.8280	0.9099
106100.	0.246	0.0082	121.5285	238.68	15.449	0.8283	0.9101
106200.	0.245	0.0082	122.0598	238.77	15.452	0.8286	0.9103
106300.	0.244	0.0082	122.5932	238.86	15.455	0.8289	0.9104
106400.	0.243	0.0081	123.1287	238.95	15.458	0.8292	0.9106
106500.	0.242	0.0081	123.6664	239.04	15.461	0.8296	0.9108
106600.	0.241	0.0081	124.2062	239.14	15.464	0.8299	0.9110
106700.	0.240	0.0080	124.7481	239.23	15.467	0.8302	0.9111
106800.	0.239	0.0080	125.2922	239.32	15.470	0.8305	0.9113
106900.	0.238	0.0079	125.8385	239.41	15.473	0.8308	0.9115
107000.	0.237	0.0079	126.3870	239.50	15.476	0.8311	0.9117
107100.	0.236	0.0079	126.9376	239.59	15.479	0.8315	0.9118
107200.	0.235	0.0078	127.4904	239.69	15.482	0.8318	0.9120
107300.	0.234	0.0078	128.0454	239.78	15.485	0.8321	0.9122
107400.	0.233	0.0078	128.6026	239.87	15.488	0.8324	0.9124
107500.	0.232	0.0077	129.1620	239.96	15.491	0.8327	0.9125
107600.	0.231	0.0077	129.7237	240.05	15.494	0.8330	0.9127
107700.	0.230	0.0077	130.2875	240.14	15.496	0.8334	0.9129
107800.	0.229	0.0076	130.8536	240.23	15.499	0.8337	0.9131
107900.	0.228	0.0076	131.4220	240.32	15.502	0.8340	0.9132
108000.	0.227	0.0076	131.9926	240.42	15.505	0.8343	0.9134
109100.	0.226	0.0075	132.5654	240.51	15.508	0.8346	0.9136

$H_c$ (Feet)	$\sigma$ $p/PSL$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\sigma\sqrt{\sigma}}$	$a$ (Knots)
104000.	0.0107	0.1034	9.5848	100.4757	122.2899	599.1933
104100.	0.0108	0.1041	9.6078	100.9380	122.8051	599.3090
104200.	0.0109	0.1038	9.6308	101.4022	123.3224	599.4246
104300.	0.0107	0.1036	9.6538	101.8684	123.8416	599.5403
104400.	0.0107	0.1033	9.6769	102.3366	124.3628	599.6559
104500.	0.0106	0.1031	9.7001	102.8067	124.8859	599.7715
104600.	0.0106	0.1028	9.7232	103.2789	125.4111	599.8871
104700.	0.0105	0.1026	9.7465	103.7530	125.9383	600.0027
104800.	0.0105	0.1024	9.7697	104.2291	126.4675	600.1182
104900.	0.0104	0.1021	9.7931	104.7071	126.9987	600.2337
105000.	0.0104	0.1019	9.8164	105.1872	127.5319	600.3492
105100.	0.0103	0.1016	9.8399	105.6694	128.0672	600.4647
105200.	0.0103	0.1014	9.8633	106.1535	128.6045	600.5802
105300.	0.0102	0.1011	9.8868	106.6397	129.1438	600.6956
105400.	0.0102	0.1009	9.9104	107.1279	129.6852	600.8110
105500.	0.0101	0.1007	9.9340	107.6182	130.2297	600.9264
105600.	0.0101	0.1004	9.9576	108.1105	130.7762	601.0418
105700.	0.0100	0.1002	9.9813	108.6048	131.3218	601.1571
105800.	0.0100	0.0999	10.0051	109.1013	131.8715	601.2724
105900.	0.0099	0.0997	10.0289	109.5999	132.4233	601.3877
106000.	0.0099	0.0995	10.0527	110.1004	132.9771	601.5030
106100.	0.0098	0.0992	10.0766	110.6031	133.5331	601.6183
106200.	0.0098	0.0990	10.1006	111.1077	134.0912	601.7335
106300.	0.0098	0.0988	10.1245	111.6143	134.6514	601.8487
106400.	0.0097	0.0985	10.1486	112.1233	135.2137	601.9639
106500.	0.0097	0.0983	10.1726	112.6350	135.7782	602.0791
106600.	0.0097	0.0981	10.1968	113.1483	136.3448	602.1942
106700.	0.0096	0.0979	10.2209	113.6637	136.9135	602.3093
106800.	0.0096	0.0976	10.2452	114.1813	137.4844	602.4244
106900.	0.0096	0.0974	10.2694	114.7010	138.0575	602.5395
107000.	0.0094	0.0971	10.2938	115.2229	138.6327	602.6546
107100.	0.0094	0.0969	10.3181	115.7470	139.2101	602.7696
107200.	0.0093	0.0967	10.3425	116.2733	139.7897	602.8846
107300.	0.0093	0.0965	10.3670	116.8017	140.3714	602.9996
107400.	0.0093	0.0962	10.3915	117.3323	140.9554	603.1146
107500.	0.0092	0.0960	10.4161	117.8652	141.5416	603.2295
107600.	0.0092	0.0959	10.4407	118.4003	142.1300	603.3444
107700.	0.0091	0.0956	10.4654	118.9376	142.7206	603.4593
107800.	0.0091	0.0953	10.4901	119.4771	143.3134	603.5742
107900.	0.0090	0.0951	10.5148	120.0187	143.9085	603.6891
108000.	0.0090	0.0949	10.5396	120.5623	144.5059	603.8039
108100.	0.0089	0.0947	10.5645	121.1092	145.1054	603.9187

$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
108200.	0.225	0.0075	133.1406	240.60	15.511	0.8349	0.9138
108300.	0.224	0.0075	133.7180	240.69	15.514	0.8353	0.9139
108400.	0.223	0.0074	134.2977	240.78	15.517	0.8356	0.9141
108500.	0.222	0.0074	134.8796	240.87	15.520	0.8359	0.9143
108600.	0.221	0.0074	135.4639	240.96	15.523	0.8362	0.9144
108700.	0.220	0.0074	136.0504	241.06	15.526	0.8365	0.9146
108800.	0.219	0.0073	136.6393	241.15	15.529	0.8369	0.9148
108900.	0.218	0.0073	137.2306	241.24	15.532	0.8372	0.9150
109000.	0.217	0.0073	137.8241	241.33	15.535	0.8375	0.9151
109100.	0.216	0.0072	138.4200	241.42	15.538	0.8378	0.9153
109200.	0.215	0.0072	139.0183	241.51	15.541	0.8381	0.9155
109300.	0.214	0.0072	139.6189	241.60	15.544	0.8384	0.9157
109400.	0.213	0.0071	140.2218	241.70	15.547	0.8388	0.9158
109500.	0.212	0.0071	140.8272	241.79	15.549	0.8391	0.9160
109600.	0.212	0.0071	141.4349	241.88	15.552	0.8394	0.9162
109700.	0.211	0.0070	142.0450	241.97	15.555	0.8397	0.9164
109800.	0.210	0.0070	142.6575	242.06	15.556	0.8400	0.9165
109900.	0.209	0.0070	143.2724	242.15	15.561	0.8403	0.9167
110000.	0.209	0.0069	143.8898	242.24	15.564	0.8407	0.9169
110100.	0.207	0.0069	144.5095	242.34	15.567	0.8410	0.9170
110200.	0.206	0.0069	145.1317	242.43	15.570	0.8413	0.9172
110300.	0.205	0.0069	145.7564	242.52	15.573	0.8416	0.9174
110400.	0.204	0.0068	146.3835	242.61	15.576	0.8419	0.9176
110500.	0.204	0.0068	147.0130	242.70	15.579	0.8422	0.9177
110600.	0.203	0.0068	147.6450	242.79	15.582	0.8426	0.9179
110700.	0.202	0.0067	148.2796	242.88	15.585	0.8429	0.9181
110800.	0.201	0.0067	148.9165	242.98	15.588	0.8432	0.9182
110900.	0.200	0.0067	149.5560	243.07	15.591	0.8435	0.9184
111000.	0.199	0.0067	150.1980	243.16	15.594	0.8438	0.9186
111100.	0.198	0.0066	150.8425	243.25	15.596	0.8441	0.9188
111200.	0.198	0.0066	151.4895	243.34	15.599	0.8445	0.9189
111300.	0.197	0.0066	152.1391	243.43	15.602	0.8448	0.9191
111400.	0.196	0.0065	152.7912	243.52	15.605	0.8451	0.9193
111500.	0.195	0.0065	153.4458	243.62	15.608	0.8454	0.9195
111600.	0.194	0.0065	154.1030	243.71	15.611	0.8457	0.9196
111700.	0.193	0.0065	154.7628	243.80	15.614	0.8461	0.9198
111800.	0.193	0.0064	155.4251	243.89	15.617	0.8464	0.9200
111900.	0.192	0.0064	156.0900	243.98	15.620	0.8467	0.9202
112000.	0.191	0.0064	156.7575	244.07	15.623	0.8470	0.9203
112100.	0.190	0.0064	157.4277	244.16	15.626	0.8473	0.9205
112200.	0.189	0.0063	158.1004	244.26	15.629	0.8476	0.9207
112300.	0.188	0.0063	158.7757	244.35	15.632	0.8480	0.9208

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\sigma}}{\sigma}$	$\frac{1}{\lambda\sqrt{\sigma}}$	$a$ (Knots)
106200.	0.0944	0.0944	10.5894	121.6577	145.7072	604.0335
106300.	0.0942	0.0942	10.6143	122.2085	146.3113	604.1483
106400.	0.0940	0.0940	10.6393	122.7616	146.9177	604.2630
106500.	0.0938	0.0938	10.6644	123.3170	147.5264	604.3778
106600.	0.0935	0.0935	10.6895	123.8747	148.1373	604.4925
106700.	0.0933	0.0933	10.7146	124.4347	148.7505	604.6072
106800.	0.0931	0.0931	10.7398	124.9970	149.3661	604.7218
106900.	0.0929	0.0929	10.7651	125.5617	149.9839	604.8365
107000.	0.0927	0.0927	10.7904	126.1286	150.6041	604.9511
107100.	0.0925	0.0925	10.8157	126.6980	151.2266	605.0657
107200.	0.0922	0.0922	10.8411	127.2696	151.8514	605.1803
107300.	0.0920	0.0920	10.8666	127.8437	152.4786	605.2948
107400.	0.0918	0.0918	10.8921	128.4201	153.1082	605.4093
107500.	0.0916	0.0916	10.9176	128.9989	153.7400	605.5238
107600.	0.0914	0.0914	10.9432	129.5800	154.3743	605.6383
107700.	0.0912	0.0912	10.9689	130.1636	155.0109	605.7528
107800.	0.0910	0.0910	10.9946	130.7496	155.6500	605.8673
107900.	0.0907	0.0907	11.0204	131.3380	156.2914	605.9817
108000.	0.0905	0.0905	11.0462	131.9288	156.9352	606.0961
110100.	0.0903	0.0903	11.0720	132.5220	157.5814	606.2105
110200.	0.0901	0.0901	11.0979	133.1177	158.2300	606.3248
110300.	0.0899	0.0899	11.1239	133.7159	158.8811	606.4392
110400.	0.0897	0.0897	11.1499	134.3165	159.5345	606.5535
110500.	0.0895	0.0895	11.1759	134.9196	160.1905	606.6678
110600.	0.0893	0.0893	11.2020	135.5251	160.8498	606.7820
110700.	0.0891	0.0891	11.2282	136.1332	161.5097	606.8963
110800.	0.0889	0.0889	11.2544	136.7437	162.1710	607.0105
110900.	0.0886	0.0886	11.2807	137.3567	162.8348	607.1247
111000.	0.0884	0.0884	11.3070	137.9723	163.5000	607.2389
111100.	0.0882	0.0882	11.3333	138.5904	164.1777	607.3531
111200.	0.0880	0.0880	11.3598	139.2110	164.8510	607.4672
111300.	0.0878	0.0878	11.3862	139.8342	165.5267	607.5814
111400.	0.0876	0.0876	11.4127	140.4599	166.2050	607.6955
111500.	0.0874	0.0874	11.4393	141.0882	166.8858	607.8095
111600.	0.0872	0.0872	11.4659	141.7191	167.5691	607.9236
111700.	0.0870	0.0870	11.4926	142.3525	168.2549	608.0376
111800.	0.0868	0.0868	11.5193	142.9885	168.9433	608.1516
111900.	0.0866	0.0866	11.5461	143.6272	169.6343	608.2656
112000.	0.0864	0.0864	11.5729	144.2684	170.3278	608.3796
112100.	0.0862	0.0862	11.5998	144.9123	171.0239	608.4936
112200.	0.0860	0.0860	11.6268	145.5589	171.7226	608.6075
112300.	0.0858	0.0858	11.6537	146.2079	172.4239	608.7214



$H_c$ (Feet)	$P_a$ ("Hg)	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
112400.	0.188	0.0063	159.4537	244.44	15.635	0.8483	0.9210
112500.	0.187	0.0062	160.1343	244.53	15.637	0.8486	0.9212
112600.	0.186	0.0062	160.8176	244.62	15.640	0.8489	0.9214
112700.	0.185	0.0062	161.5036	244.71	15.643	0.8492	0.9215
112800.	0.184	0.0062	162.1922	244.80	15.646	0.8495	0.9217
112900.	0.184	0.0061	162.8834	244.90	15.649	0.8499	0.9219
113000.	0.183	0.0061	163.5774	244.99	15.652	0.8502	0.9221
113100.	0.182	0.0061	164.2741	245.08	15.655	0.8505	0.9222
113200.	0.181	0.0061	164.9734	245.17	15.658	0.8508	0.9224
113300.	0.181	0.0060	165.6755	245.26	15.661	0.8511	0.9226
113400.	0.180	0.0060	166.3803	245.35	15.664	0.8514	0.9227
113500.	0.179	0.0060	167.0878	245.44	15.667	0.8518	0.9229
113600.	0.179	0.0060	167.7981	245.54	15.670	0.8521	0.9231
113700.	0.178	0.0059	168.5112	245.63	15.673	0.8524	0.9233
113800.	0.177	0.0059	169.2269	245.72	15.675	0.8527	0.9234
113900.	0.176	0.0059	169.9455	245.81	15.679	0.8530	0.9236
114000.	0.175	0.0059	170.6669	245.90	15.681	0.8534	0.9238
114100.	0.175	0.0058	171.3910	245.99	15.684	0.8537	0.9239
114200.	0.174	0.0058	172.1180	246.08	15.687	0.8540	0.9241
114300.	0.173	0.0058	172.8477	246.18	15.690	0.8543	0.9243
114400.	0.172	0.0058	173.5803	246.27	15.693	0.8546	0.9245
114500.	0.172	0.0057	174.3157	246.36	15.696	0.8549	0.9246
114600.	0.171	0.0057	175.0540	246.45	15.699	0.8553	0.9248
114700.	0.170	0.0057	175.7951	246.54	15.702	0.8556	0.9250
114800.	0.169	0.0057	176.5390	246.63	15.705	0.8559	0.9251
114900.	0.169	0.0056	177.2859	246.72	15.707	0.8562	0.9253
115000.	0.168	0.0056	178.0356	246.82	15.710	0.8565	0.9255
115100.	0.167	0.0056	178.7882	246.91	15.713	0.8568	0.9257
115200.	0.167	0.0056	179.5437	247.00	15.716	0.8572	0.9258
115300.	0.166	0.0055	180.3021	247.09	15.719	0.8575	0.9260
115400.	0.165	0.0055	181.0635	247.18	15.722	0.8578	0.9262
115500.	0.165	0.0055	181.8277	247.27	15.725	0.8581	0.9263
115600.	0.164	0.0055	182.5949	247.36	15.728	0.8584	0.9265
115700.	0.163	0.0055	183.3651	247.46	15.731	0.8587	0.9267
115800.	0.162	0.0054	184.1382	247.55	15.734	0.8591	0.9269
115900.	0.162	0.0054	184.9143	247.64	15.737	0.8594	0.9270
116000.	0.161	0.0054	185.6934	247.73	15.739	0.8597	0.9272
116100.	0.160	0.0054	186.4755	247.82	15.742	0.8600	0.9274
116200.	0.160	0.0053	187.2605	247.91	15.745	0.8603	0.9275
116300.	0.159	0.0053	188.0487	248.00	15.748	0.8606	0.9277
116400.	0.158	0.0053	188.8398	248.10	15.751	0.8610	0.9279
116500.	0.158	0.0053	189.6339	248.19	15.754	0.8613	0.9281

$H_c$ (Feet)	$\sigma$ $\rho/\text{PSI}$	$\sqrt{f}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{h\sqrt{\theta}}$	$a$ (Knots)
112400.	0.0073	0.0856	11.6808	146.8597	173.1277	608.8353
112500.	0.0073	0.0854	11.7079	147.5142	173.8342	608.9492
112600.	0.0073	0.0852	11.7350	148.1713	174.5473	609.0630
112700.	0.0072	0.0850	11.7622	148.8311	175.2550	609.1768
112800.	0.0072	0.0848	11.7895	149.4936	175.9694	609.2906
112900.	0.0072	0.0846	11.8168	150.1588	176.6864	609.4044
113000.	0.0071	0.0844	11.8441	150.8267	177.4061	609.5182
113100.	0.0071	0.0842	11.8715	151.4973	178.1284	609.6319
113200.	0.0071	0.0840	11.8990	152.1705	178.8533	609.7456
113300.	0.0070	0.0838	11.9265	152.8467	179.5810	609.8593
113400.	0.0070	0.0837	11.9541	153.5256	180.3114	609.9730
113500.	0.0070	0.0835	11.9817	154.2072	181.0444	610.0867
113600.	0.0069	0.0833	12.0094	154.8915	181.7802	610.2003
113700.	0.0069	0.0831	12.0371	155.5787	182.5196	610.3139
113800.	0.0069	0.0829	12.0649	156.2686	183.2598	610.4275
113900.	0.0068	0.0827	12.0927	156.9614	184.0037	610.5411
114000.	0.0068	0.0825	12.1206	157.6569	184.7504	610.6546
114100.	0.0068	0.0823	12.1486	158.3553	185.4998	610.7681
114200.	0.0067	0.0821	12.1766	159.0565	186.2520	610.8816
114300.	0.0067	0.0819	12.2046	159.7606	187.0069	610.9951
114400.	0.0067	0.0817	12.2327	160.4675	187.7647	611.1086
114500.	0.0067	0.0816	12.2609	161.1772	188.5252	611.2220
114600.	0.0066	0.0814	12.2891	161.8899	189.2885	611.3355
114700.	0.0066	0.0812	12.3174	162.6054	190.0546	611.4489
114800.	0.0066	0.0810	12.3457	163.3238	190.8235	611.5622
114900.	0.0065	0.0808	12.3741	164.0452	191.5953	611.6756
115000.	0.0065	0.0806	12.4025	164.7694	192.3698	611.7889
115100.	0.0065	0.0804	12.4310	165.4966	193.1473	611.9023
115200.	0.0064	0.0803	12.4595	166.2267	193.9275	612.0155
115300.	0.0064	0.0801	12.4881	166.9597	194.7107	612.1288
115400.	0.0064	0.0799	12.5168	167.6958	195.4967	612.2421
115500.	0.0064	0.0797	12.5455	168.4348	196.2856	612.3553
115600.	0.0063	0.0795	12.5743	169.1767	197.0774	612.4685
115700.	0.0063	0.0793	12.6031	169.9217	197.8720	612.5817
115800.	0.0063	0.0792	12.6320	170.6697	198.6696	612.6949
115900.	0.0062	0.0790	12.6609	171.4207	199.4702	612.8080
116000.	0.0062	0.0788	12.6899	172.1747	200.2736	612.9212
116100.	0.0062	0.0786	12.7189	172.9317	201.0800	613.0343
116200.	0.0062	0.0784	12.7480	173.6919	201.8893	613.1474
116300.	0.0061	0.0783	12.7772	174.4550	202.7016	613.2604
116400.	0.0061	0.0781	12.8064	175.2212	203.5168	613.3735
116500.	0.0061	0.0779	12.8356	175.9905	204.3350	613.4865

$H_c$ (Feet)	$P_a$ ( $^{\circ}\text{Hg}$ )	$\delta$ $P_a/P_{aSL}$	$\frac{1}{\delta}$	$T_a$ ( $^{\circ}\text{K}$ )	$\sqrt{T_a}$	$\theta$ $T_a/T_{aSL}$	$\sqrt{\theta}$
116000.	0.157	0.0053	190.4311	248.28	15.757	0.8616	0.9282
116700.	0.156	0.0052	191.2314	248.37	15.760	0.8619	0.9284
116800.	0.156	0.0052	192.0347	248.46	15.763	0.8622	0.9286
116900.	0.155	0.0052	192.8411	248.55	15.766	0.8626	0.9287
117000.	0.155	0.0052	193.6506	248.64	15.768	0.8629	0.9289
117100.	0.154	0.0051	194.4631	248.74	15.771	0.8632	0.9291
117200.	0.153	0.0051	195.2789	248.83	15.774	0.8635	0.9292
117300.	0.153	0.0051	196.0977	248.92	15.777	0.8638	0.9294
117400.	0.152	0.0051	196.9196	249.01	15.780	0.8641	0.9296
117500.	0.151	0.0051	197.7447	249.10	15.783	0.8645	0.9298
117600.	0.151	0.0050	198.5729	249.19	15.786	0.8648	0.9299
117700.	0.150	0.0050	199.4043	249.28	15.789	0.8651	0.9301
117800.	0.149	0.0050	200.2389	249.38	15.792	0.8654	0.9303
117900.	0.149	0.0050	201.0766	249.47	15.795	0.8657	0.9304
118000.	0.148	0.0050	201.9176	249.56	15.797	0.8660	0.9306
118100.	0.148	0.0049	202.7618	249.65	15.800	0.8664	0.9308
118200.	0.147	0.0049	203.6091	249.74	15.803	0.8667	0.9310
118300.	0.146	0.0049	204.4597	249.83	15.806	0.8670	0.9311
118400.	0.146	0.0049	205.3136	249.92	15.809	0.8673	0.9313
118500.	0.145	0.0049	206.1707	250.02	15.812	0.8676	0.9315
118600.	0.145	0.0048	207.0311	250.11	15.815	0.8679	0.9316
118700.	0.144	0.0048	207.8947	250.20	15.818	0.8683	0.9318
118800.	0.143	0.0048	208.7616	250.29	15.821	0.8686	0.9320
118900.	0.143	0.0048	209.6318	250.38	15.823	0.8689	0.9321
119000.	0.142	0.0048	210.5054	250.47	15.826	0.8692	0.9323
119100.	0.142	0.0047	211.3822	250.57	15.829	0.8695	0.9325
119200.	0.141	0.0047	212.2624	250.66	15.832	0.8699	0.9327
119300.	0.140	0.0047	213.1459	250.75	15.835	0.8702	0.9328
119400.	0.140	0.0047	214.0328	250.84	15.838	0.8705	0.9330
119500.	0.139	0.0047	214.9230	250.93	15.841	0.8708	0.9332
119600.	0.139	0.0046	215.8166	251.02	15.844	0.8711	0.9333
119700.	0.138	0.0046	216.7136	251.11	15.847	0.8714	0.9335
119800.	0.137	0.0046	217.6140	251.21	15.849	0.8718	0.9337
119900.	0.137	0.0046	218.5178	251.30	15.852	0.8721	0.9338
120000.	0.136	0.0046	219.4251	251.39	15.855	0.8724	0.9340
121000.	0.131	0.0044	228.6883	252.30	15.884	0.8756	0.9357
122000.	0.126	0.0042	238.3069	253.22	15.913	0.8787	0.9374
123000.	0.121	0.0040	248.2931	254.13	15.941	0.8819	0.9391
124000.	0.116	0.0039	258.6597	255.05	15.970	0.8851	0.9408
125000.	0.111	0.0037	269.4198	255.96	15.999	0.8883	0.9425
126000.	0.107	0.0036	280.5986	256.87	16.027	0.8914	0.9442
127000.	0.102	0.0034	292.1741	257.79	16.056	0.8946	0.9458

$H_c$ (Feet)	$\sigma$ $p/PSI$	$\sqrt{x}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{A\sqrt{\theta}}$	$a$ (Knots)
116600.	0.0057	0.0777	12.8650	176.7629	205.1562	613.5995
116700.	0.0057	0.0776	12.8943	177.5384	205.9804	613.7125
116800.	0.0057	0.0774	12.9238	178.3170	206.8077	613.8254
116900.	0.0057	0.0772	12.9533	179.0987	207.6379	613.9384
117000.	0.0057	0.0770	12.9828	179.8836	208.4711	614.0513
117100.	0.0057	0.0768	13.0124	180.6716	209.3074	614.1642
117200.	0.0057	0.0767	13.0421	181.4628	210.1468	614.2771
117300.	0.0057	0.0765	13.0718	182.2572	210.9891	614.3899
117400.	0.0057	0.0763	13.1016	183.0547	211.8346	614.5028
117500.	0.0057	0.0762	13.1314	183.8555	212.6831	614.6156
117600.	0.0057	0.0760	13.1613	184.6594	213.5347	614.7284
117700.	0.0057	0.0758	13.1912	185.4666	214.3895	614.8412
117800.	0.0057	0.0756	13.2212	186.2770	215.2473	614.9539
117900.	0.0057	0.0755	13.2513	187.0906	216.1082	615.0666
118000.	0.0057	0.0753	13.2814	187.9075	216.9722	615.1794
118100.	0.0057	0.0751	13.3116	188.7277	217.8395	615.2920
118200.	0.0057	0.0750	13.3418	189.5511	218.7078	615.4047
118300.	0.0056	0.0748	13.3721	190.3778	219.5833	615.5174
118400.	0.0056	0.0746	13.4024	191.2078	220.4600	615.6300
118500.	0.0056	0.0744	13.4328	192.0411	221.3398	615.7426
118600.	0.0056	0.0743	13.4633	192.8778	222.2229	615.8552
118700.	0.0056	0.0741	13.4938	193.7178	223.1091	615.9678
118800.	0.0056	0.0739	13.5244	194.5612	223.9985	616.0803
118900.	0.0056	0.0738	13.5550	195.4079	224.8911	616.1928
119000.	0.0056	0.0736	13.5857	196.2580	225.7870	616.3054
119100.	0.0056	0.0734	13.6165	197.1114	226.6862	616.4178
119200.	0.0056	0.0733	13.6473	197.9683	227.5886	616.5303
119300.	0.0056	0.0731	13.6781	199.8286	228.4942	616.6427
119400.	0.0056	0.0729	13.7091	199.6923	229.4031	616.7552
119500.	0.0056	0.0728	13.7400	200.5594	230.3153	616.8676
119600.	0.0056	0.0726	13.7711	201.4300	231.2308	616.9800
119700.	0.0056	0.0725	13.8022	202.3040	232.1496	617.0923
119800.	0.0056	0.0723	13.8333	203.1815	233.0717	617.2047
119900.	0.0056	0.0721	13.8646	204.0625	233.9971	617.3170
120000.	0.0056	0.0720	13.8958	204.9471	234.9259	617.4293
121000.	0.0056	0.0704	14.2119	213.9872	244.3994	618.5512
122000.	0.0047	0.0688	14.5340	223.3912	254.2185	619.6711
123000.	0.0042	0.0673	14.8621	233.1723	264.3946	620.7889
124000.	0.0044	0.0658	15.1965	243.3442	274.9393	621.9048
125000.	0.0041	0.0644	15.5371	253.9210	285.8645	623.0186
126000.	0.0040	0.0630	15.8841	264.9174	297.1876	624.1304
127000.	0.0038	0.0616	16.2376	276.3483	308.9061	625.2403

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\rho}{P_a/P_{aSL}}$	$\frac{1}{\rho}$	$T_a$ ("K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
128000.	0.098	0.0033	304.1965	258.70	16.084	0.8978	0.9475
129000.	0.094	0.0032	316.6685	259.62	16.113	0.9009	0.9492
130000.	0.091	0.0030	329.6054	260.53	16.141	0.9041	0.9509
131000.	0.087	0.0029	343.0227	261.45	16.169	0.9073	0.9525
132000.	0.084	0.0028	356.9363	262.36	16.198	0.9105	0.9542
133000.	0.081	0.0027	371.3631	263.28	16.226	0.9136	0.9558
134000.	0.077	0.0026	386.3197	264.19	16.254	0.9168	0.9575
135000.	0.074	0.0025	401.8240	265.10	16.282	0.9200	0.9592
136000.	0.072	0.0024	417.8939	266.02	16.310	0.9232	0.9609
137000.	0.069	0.0023	434.5480	266.93	16.338	0.9263	0.9625
138000.	0.066	0.0022	451.8053	267.85	16.366	0.9295	0.9641
139000.	0.064	0.0021	469.6858	268.76	16.394	0.9327	0.9658
140000.	0.061	0.0020	488.2094	269.68	16.422	0.9359	0.9674
141000.	0.059	0.0020	507.3972	270.59	16.450	0.9390	0.9690
142000.	0.057	0.0019	527.2705	271.50	16.477	0.9422	0.9707
143000.	0.055	0.0018	547.8514	272.42	16.505	0.9454	0.9723
144000.	0.053	0.0018	569.1626	273.33	16.533	0.9485	0.9739
145000.	0.051	0.0017	591.2274	274.25	16.560	0.9517	0.9756
146000.	0.049	0.0016	614.0700	275.16	16.588	0.9549	0.9772
147000.	0.047	0.0016	637.7148	276.08	16.616	0.9581	0.9788
148000.	0.045	0.0015	662.1873	276.99	16.643	0.9612	0.9804
149000.	0.044	0.0015	687.5136	277.91	16.671	0.9644	0.9820
150000.	0.042	0.0014	713.7206	278.82	16.698	0.9676	0.9837
151000.	0.040	0.0013	740.8358	279.73	16.725	0.9708	0.9853
152000.	0.039	0.0013	768.8876	280.65	16.753	0.9739	0.9869
153000.	0.037	0.0013	797.9051	281.56	16.780	0.9771	0.9885
154000.	0.036	0.0012	827.9183	282.48	16.807	0.9803	0.9901
155000.	0.032	0.0011	941.2201	282.66	16.812	0.9809	0.9904
156000.	0.031	0.0010	976.5421	282.66	16.812	0.9809	0.9904
157000.	0.030	0.0010	1013.1896	282.66	16.812	0.9809	0.9904
158000.	0.028	0.0010	1051.2125	282.66	16.812	0.9809	0.9904
159000.	0.027	0.0009	1090.6622	282.66	16.812	0.9809	0.9904
160000.	0.026	0.0009	1131.5925	282.66	16.812	0.9809	0.9904
161000.	0.025	0.0009	1174.0587	282.66	16.812	0.9809	0.9904
162000.	0.025	0.0008	1218.1186	282.66	16.812	0.9809	0.9904
163000.	0.024	0.0008	1263.8320	282.66	16.812	0.9809	0.9904
164000.	0.023	0.0008	1311.2609	282.66	16.812	0.9809	0.9904
165000.	0.022	0.0007	1360.4698	282.66	16.812	0.9809	0.9904
166000.	0.021	0.0007	1411.5253	282.66	16.812	0.9809	0.9904
167000.	0.020	0.0007	1464.4968	282.66	16.812	0.9809	0.9904
168000.	0.020	0.0007	1519.4563	282.66	16.812	0.9809	0.9904
169000.	0.019	0.0006	1576.4782	282.66	16.812	0.9809	0.9904

$H_c$ (Feet)	$\sigma$ $\rho/\rho_{SL}$	$\sqrt{F}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{h\sqrt{\theta}}$	$a$ (Knots)
128000.	0.0036	0.0602	16.5977	288.2294	321.0481	626.3482
129000.	0.0035	0.0589	16.9644	300.5766	333.6220	627.4542
130000.	0.0033	0.0577	17.3379	313.4065	346.6416	628.5582
131000.	0.0032	0.0564	17.7183	326.7362	360.1209	629.6603
132000.	0.0031	0.0552	18.1057	340.5833	374.0745	630.7604
133000.	0.0029	0.0541	18.5001	354.9661	388.5175	631.8587
134000.	0.0028	0.0529	18.9017	369.9030	403.4650	632.9550
135000.	0.0027	0.0518	19.3106	385.4137	418.9330	634.0494
136000.	0.0026	0.0507	19.7269	401.5180	434.9377	635.1419
137000.	0.0025	0.0496	20.1507	418.2364	451.4957	636.2326
138000.	0.0024	0.0486	20.5821	435.5901	468.6241	637.3214
139000.	0.0023	0.0476	21.0212	453.6012	486.3407	638.4084
140000.	0.0022	0.0466	21.4681	472.2919	504.6635	639.4935
141000.	0.0021	0.0456	21.9230	491.6855	523.6109	640.5767
142000.	0.0020	0.0447	22.3859	511.8060	543.2022	641.6582
143000.	0.0019	0.0438	22.8570	532.6780	563.4570	642.7378
144000.	0.0018	0.0429	23.3364	554.3270	584.3952	643.8156
145000.	0.0018	0.0420	23.8242	576.7790	606.0377	644.8916
146000.	0.0017	0.0411	24.3205	600.0612	628.4058	645.9658
147000.	0.0016	0.0403	24.8255	624.2012	651.5209	647.0382
148000.	0.0016	0.0395	25.3392	649.2276	675.4057	648.1088
149000.	0.0015	0.0387	25.8618	675.1697	700.0829	649.1777
150000.	0.0014	0.0379	26.3934	702.0586	725.5764	650.2449
151000.	0.0014	0.0371	26.9342	729.9247	751.9100	651.3102
152000.	0.0013	0.0364	27.4842	758.8005	779.1088	652.3739
153000.	0.0013	0.0357	28.0436	788.7191	807.1982	653.4358
154000.	0.0012	0.0349	28.6125	819.7145	836.2041	654.4960
155000.	0.0012	0.0343	29.1935	852.1945	866.3331	654.7072
156000.	0.0011	0.0337	29.6955	885.1777	895.9971	654.7072
157000.	0.0011	0.0331	30.2476	918.4739	925.9995	654.7072
158000.	0.0011	0.0325	30.8099	952.1321	956.3905	654.7072
159000.	0.0010	0.0319	31.3827	986.2036	987.1222	654.7072
160000.	0.0010	0.0313	31.9661	1020.7413	1018.2547	654.7072
161000.	0.0009	0.0307	32.5604	1055.8003	1049.7261	654.7072
162000.	0.0009	0.0302	33.1658	1091.4377	1081.5976	654.7072
163000.	0.0009	0.0296	33.7823	1127.7128	1113.9086	654.7072
164000.	0.0008	0.0291	34.4104	1164.6869	1146.6587	654.7072
165000.	0.0008	0.0285	35.0501	1202.4238	1179.8470	654.7072
166000.	0.0008	0.0280	35.7017	1240.9898	1213.4919	654.7072
167000.	0.0007	0.0275	36.3655	1280.4533	1247.6763	654.7072
168000.	0.0007	0.0270	37.0416	1320.8858	1282.4179	654.7072
169000.	0.0007	0.0265	37.7302	1362.3609	1317.7419	654.7072

$H_c$ (Feet)	$P_a$ ("Hg)	$\frac{\delta}{P_a/P_{aSL}}$	$\frac{1}{\delta}$	$T_a$ (°K)	$\sqrt{T_a}$	$\frac{\theta}{T_a/T_{aSL}}$	$\sqrt{\theta}$
170000.	0.018	0.0006	1635.6401	282.66	16.812	0.9809	0.9904
171000.	0.018	0.0006	1697.0222	282.66	16.812	0.9809	0.9904
172000.	0.017	0.0006	1760.7078	282.66	16.812	0.9809	0.9904
173000.	0.016	0.0005	1826.7834	282.66	16.812	0.9809	0.9904
174000.	0.015	0.0005	1958.1702	282.50	16.808	0.9904	0.9901
175000.	0.015	0.0005	2031.8815	281.13	16.767	0.9756	0.9877
176000.	0.014	0.0005	2108.7486	279.76	16.726	0.9708	0.9853
177000.	0.014	0.0005	2188.9229	278.39	16.685	0.9661	0.9829
178000.	0.013	0.0004	2272.5643	277.02	16.644	0.9613	0.9805
179000.	0.013	0.0004	2359.8410	275.64	16.603	0.9566	0.9780
180000.	0.012	0.0004	2450.9300	274.27	16.561	0.9518	0.9756

$H_c$ (Feet)	$\frac{\sigma}{\rho/\rho_{SL}}$	$\sqrt{\sigma}$	$\frac{1}{\sqrt{\sigma}}$	$\frac{\sqrt{\theta}}{\theta}$	$\frac{1}{A\sqrt{\theta}}$	$\frac{a}{\text{(Knots)}}$
170000.	0.0007	0.0260	38.4316	1619.9555	1651.4766	654.7072
171000.	0.0007	0.0255	39.1461	1680.7489	1713.4530	654.7072
172000.	0.0006	0.0251	39.9739	1743.8239	1777.7552	654.7072
173000.	0.0006	0.0246	40.6152	1809.2659	1844.4706	654.7072
174000.	0.0005	0.0242	41.3588	1938.8493	1977.6837	654.5238
175000.	0.0006	0.0238	42.0276	2006.9433	2057.1294	652.9329
176000.	0.0005	0.0234	42.7106	2077.7798	2140.1790	651.3382
177000.	0.0005	0.0230	43.4082	2151.4830	2227.0142	649.7395
178000.	0.0005	0.0227	44.1206	2228.1844	2317.8281	648.1369
179000.	0.0005	0.0223	44.8484	2308.0215	2412.8239	646.5303
180000.	0.0005	0.0219	45.5919	2391.1388	2512.2162	644.9198

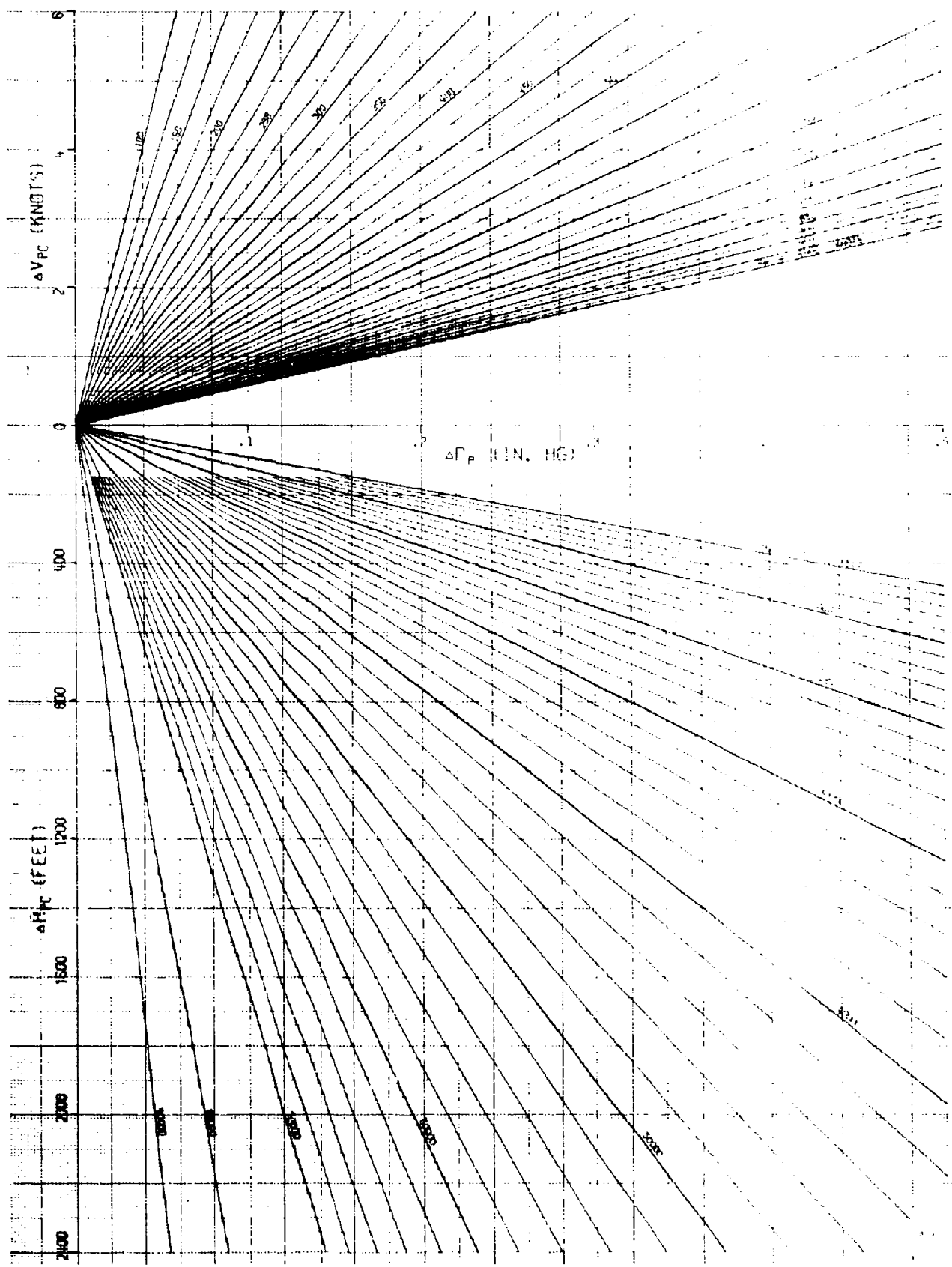


## APPENDIX B

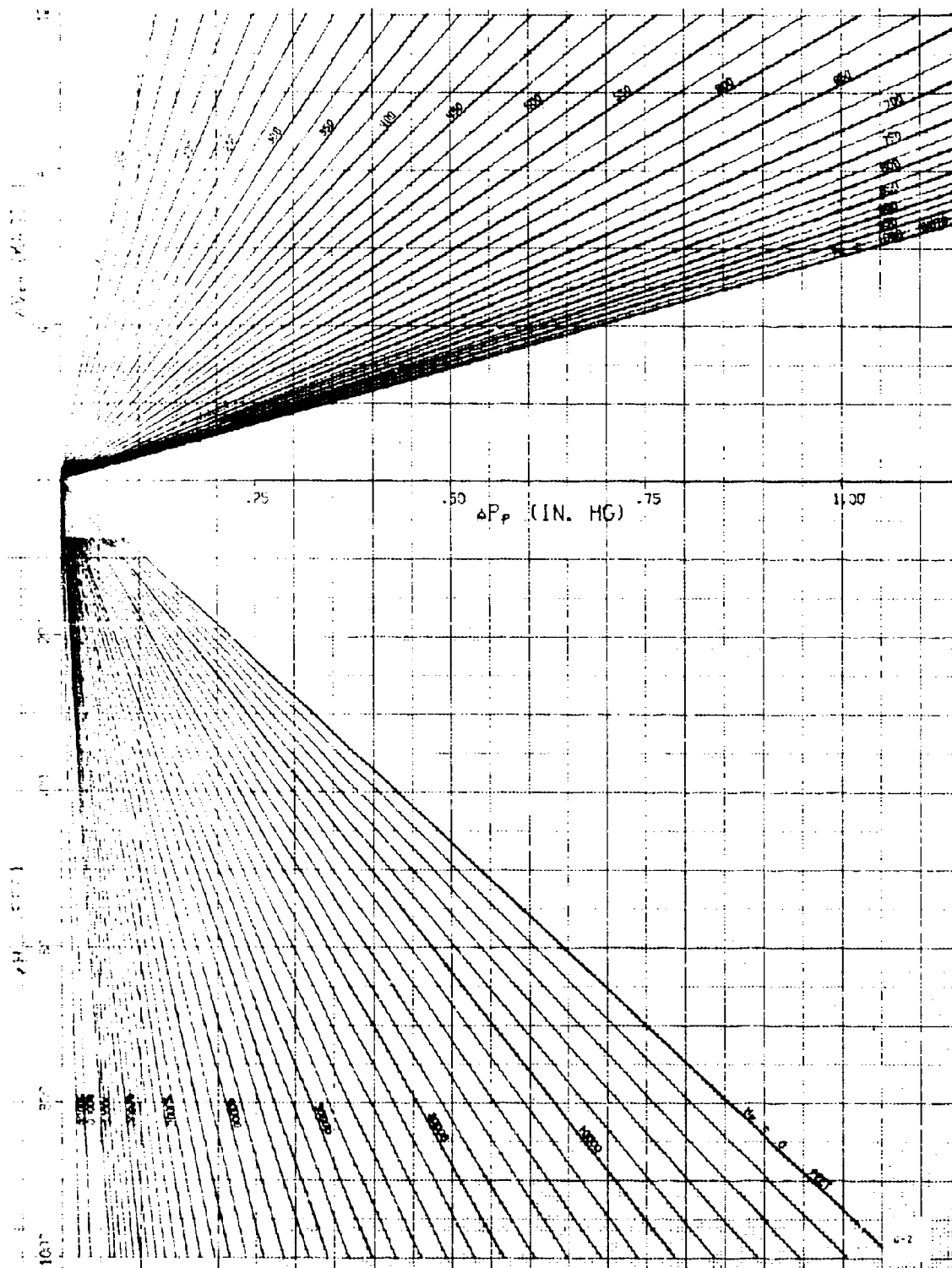
### PITOT-STATIC POSITION ERROR RELATIONS

<u>PAGE NUMBER</u>	<u>TITLE</u>
B-1 - B-4	$\Delta VPC, \Delta HPC$ vs $\Delta PP$
B-5 - B-8	$-\Delta VPC, -\Delta HPC$ vs $-\Delta PP$
B-9 - B-12	$\Delta MPC, \Delta HPC$ vs $\Delta PP/PS$
B-13 - B-16	$-\Delta MPC, -\Delta HPC$ vs $-\Delta PP/PS$
B-17 - B-19	$\Delta VPC$ vs $\Delta VIC$ at $\Delta PP/QCIC = \text{Const}$
B-20	$\Delta MPC$ vs $\Delta PP/QCIC$
B-21	$-\Delta MPC$ vs $-\Delta PP/QCIC$

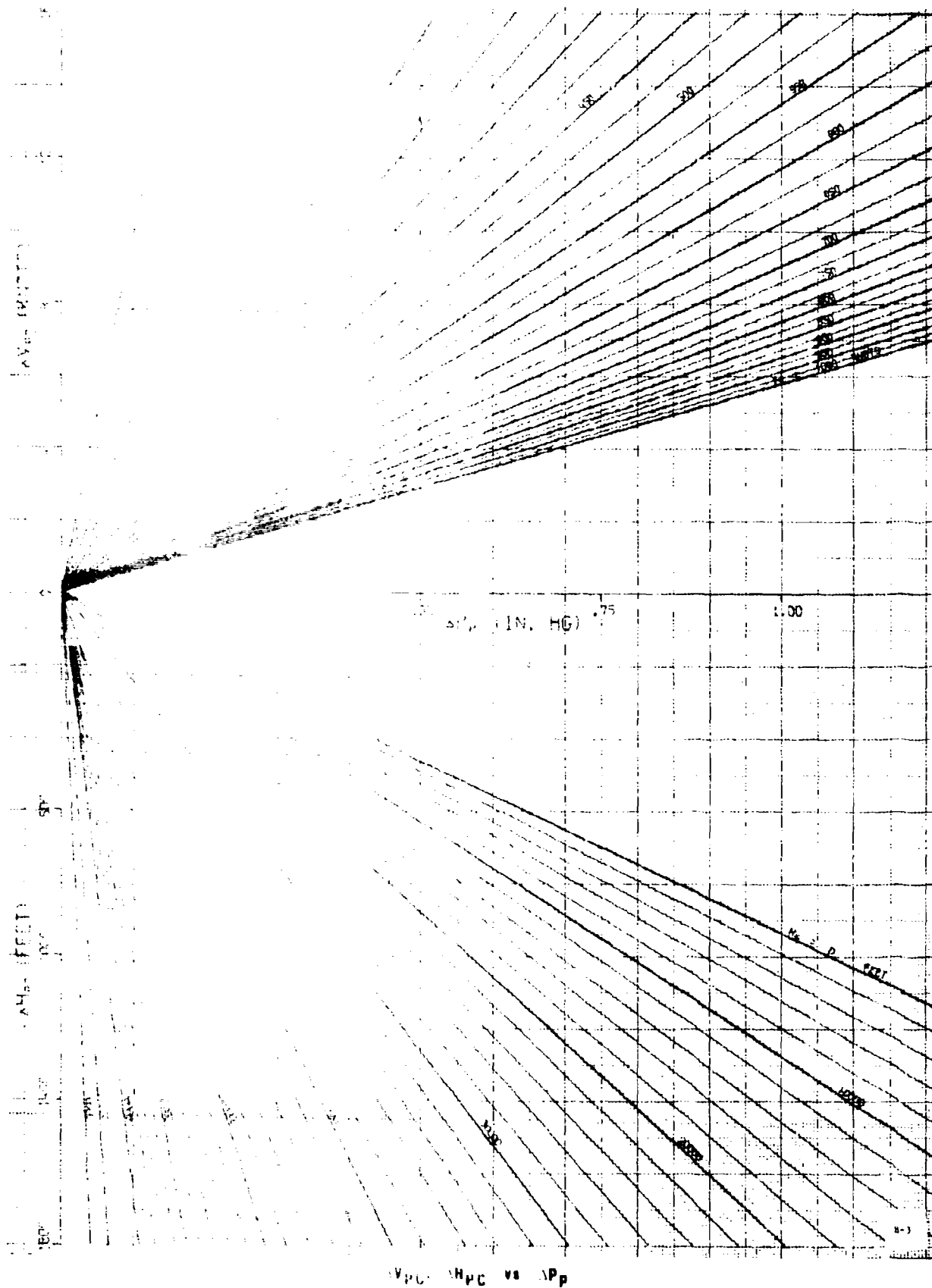
APRIL 1967

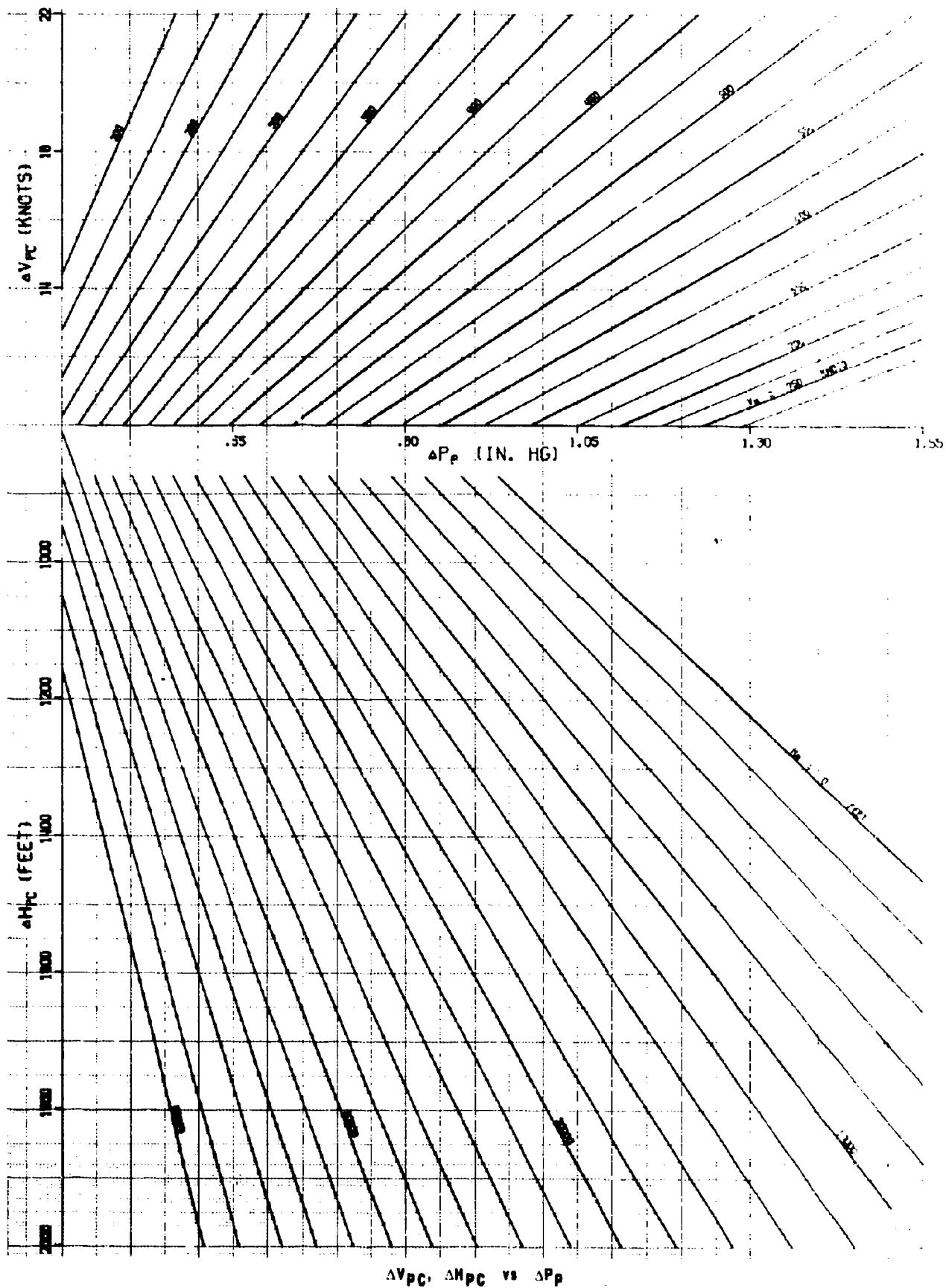


$\Delta V_{pc}$ ,  $\Delta H_{pc}$  vs  $\Delta P_p$

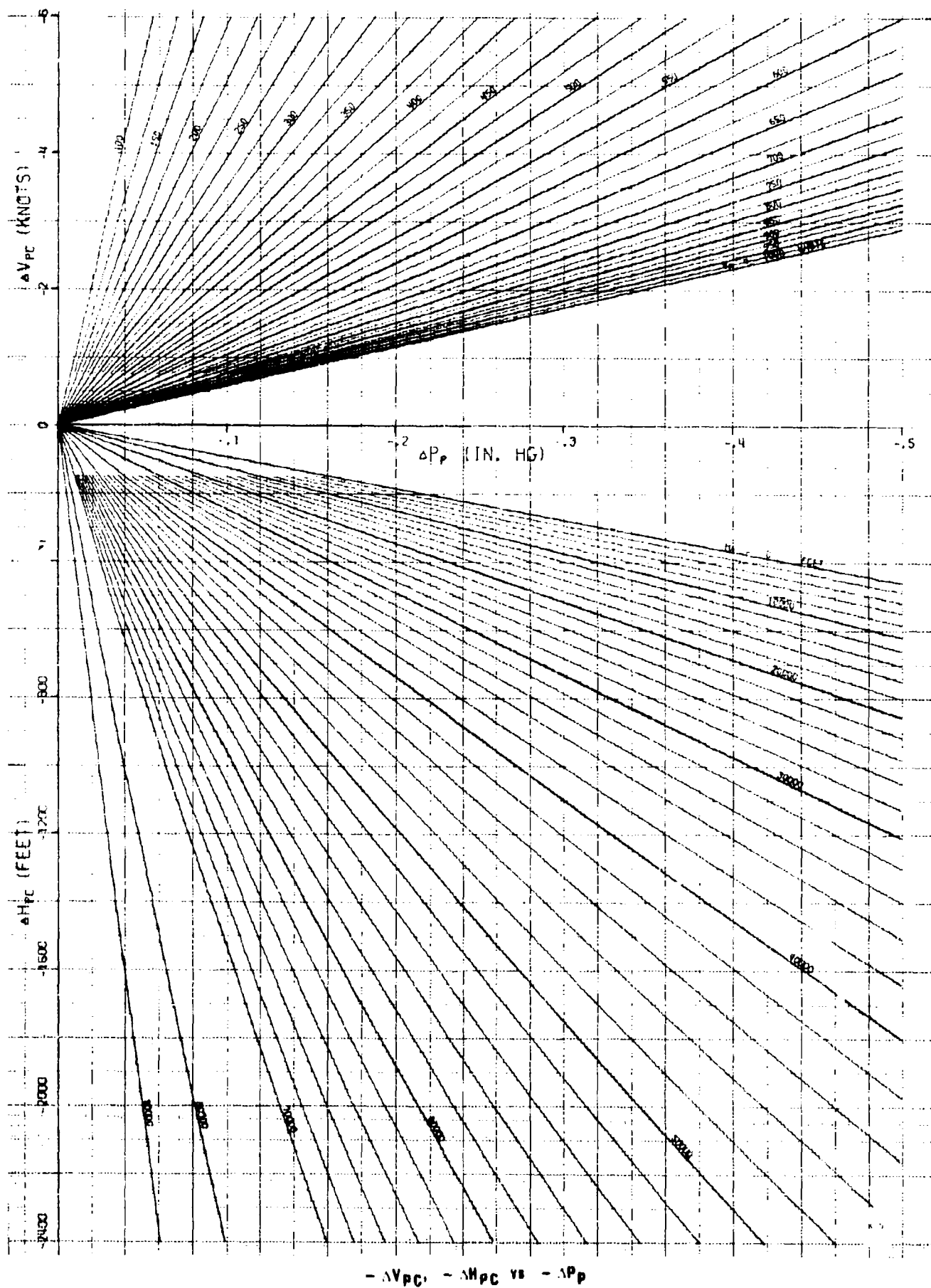


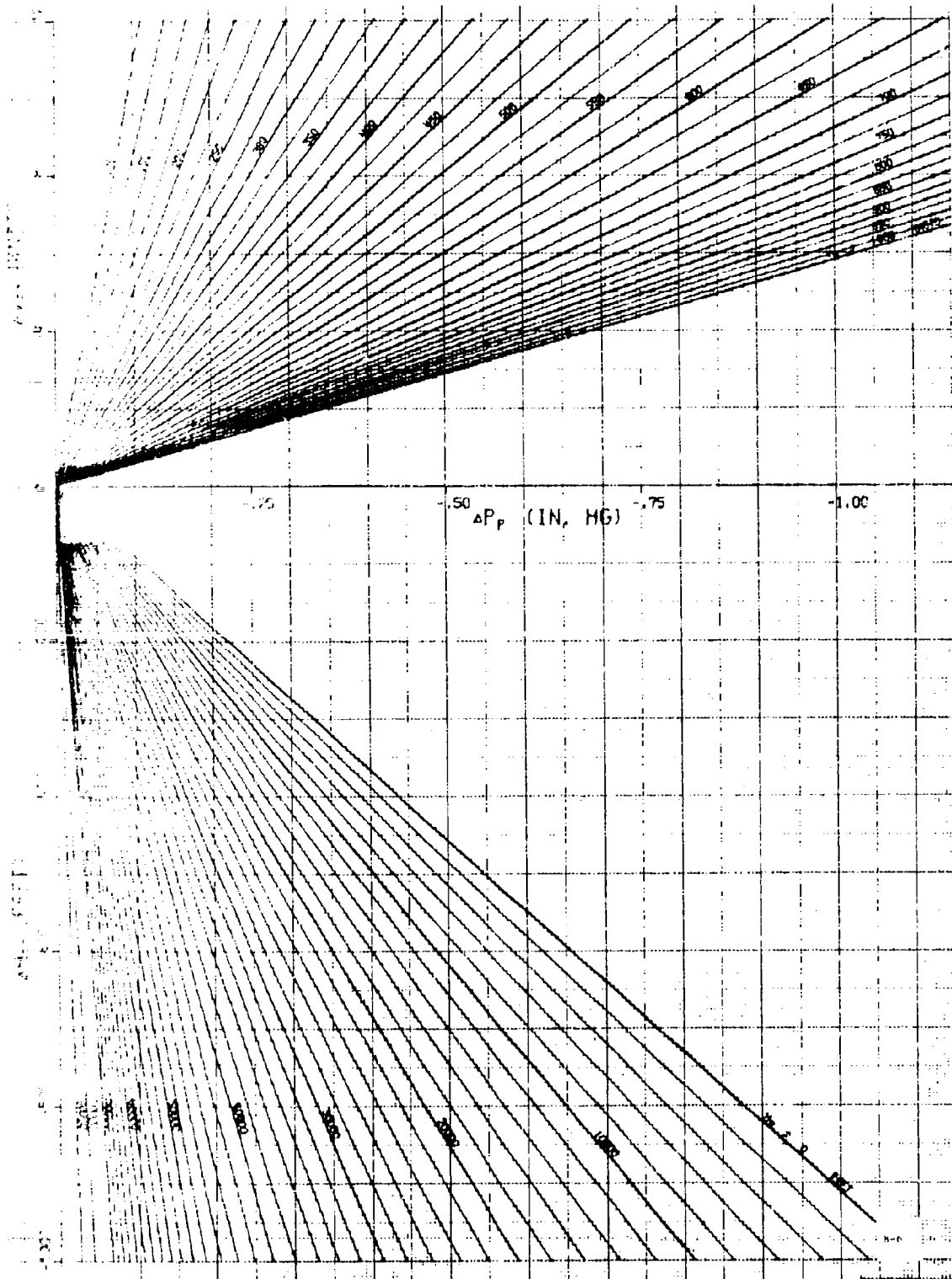
$\Delta V_{PC}, \Delta H_{PC}$  vs  $\Delta P_p$



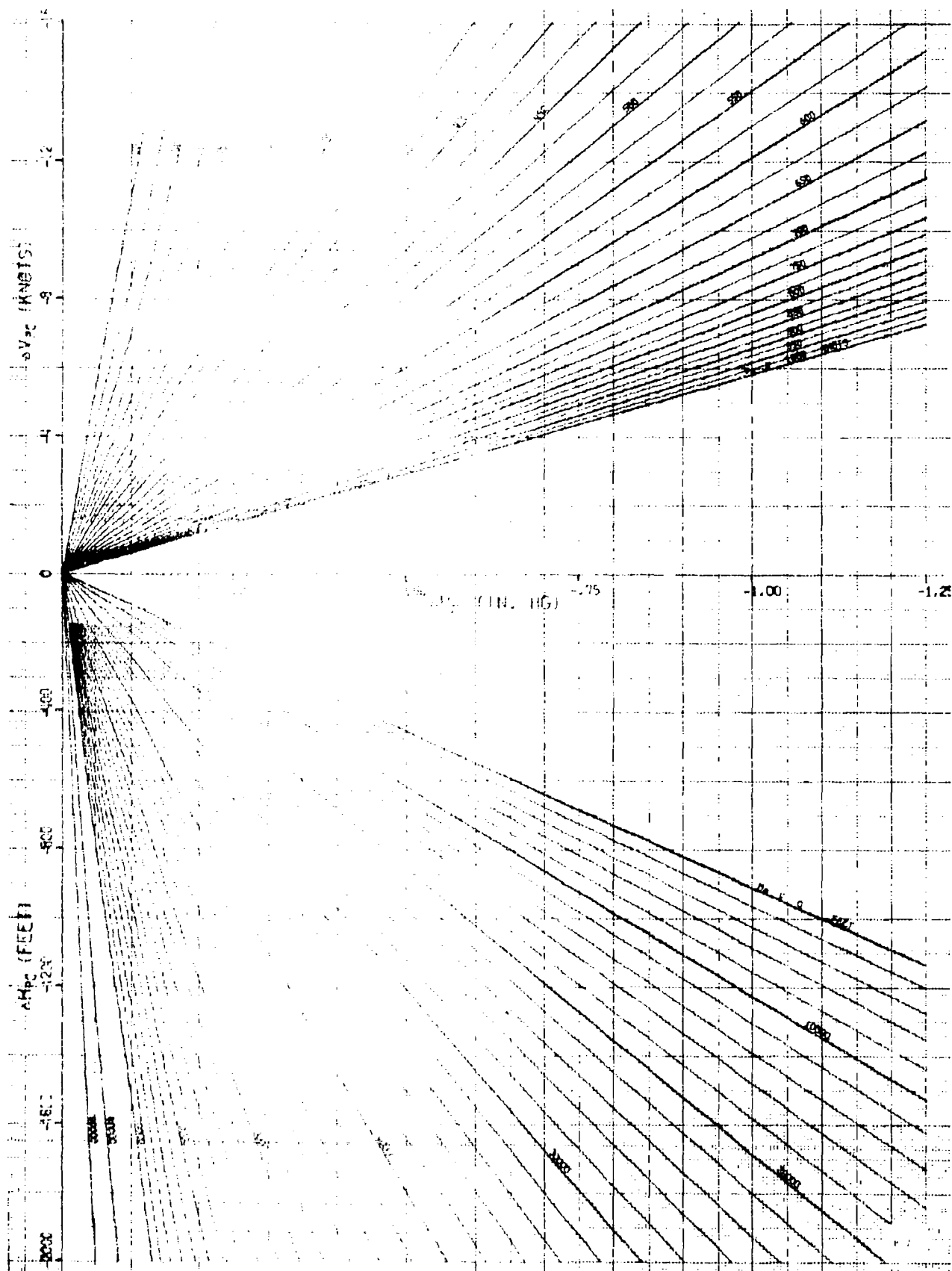


$\Delta V_{pc}$ ,  $\Delta H_{pc}$  vs  $\Delta P_p$



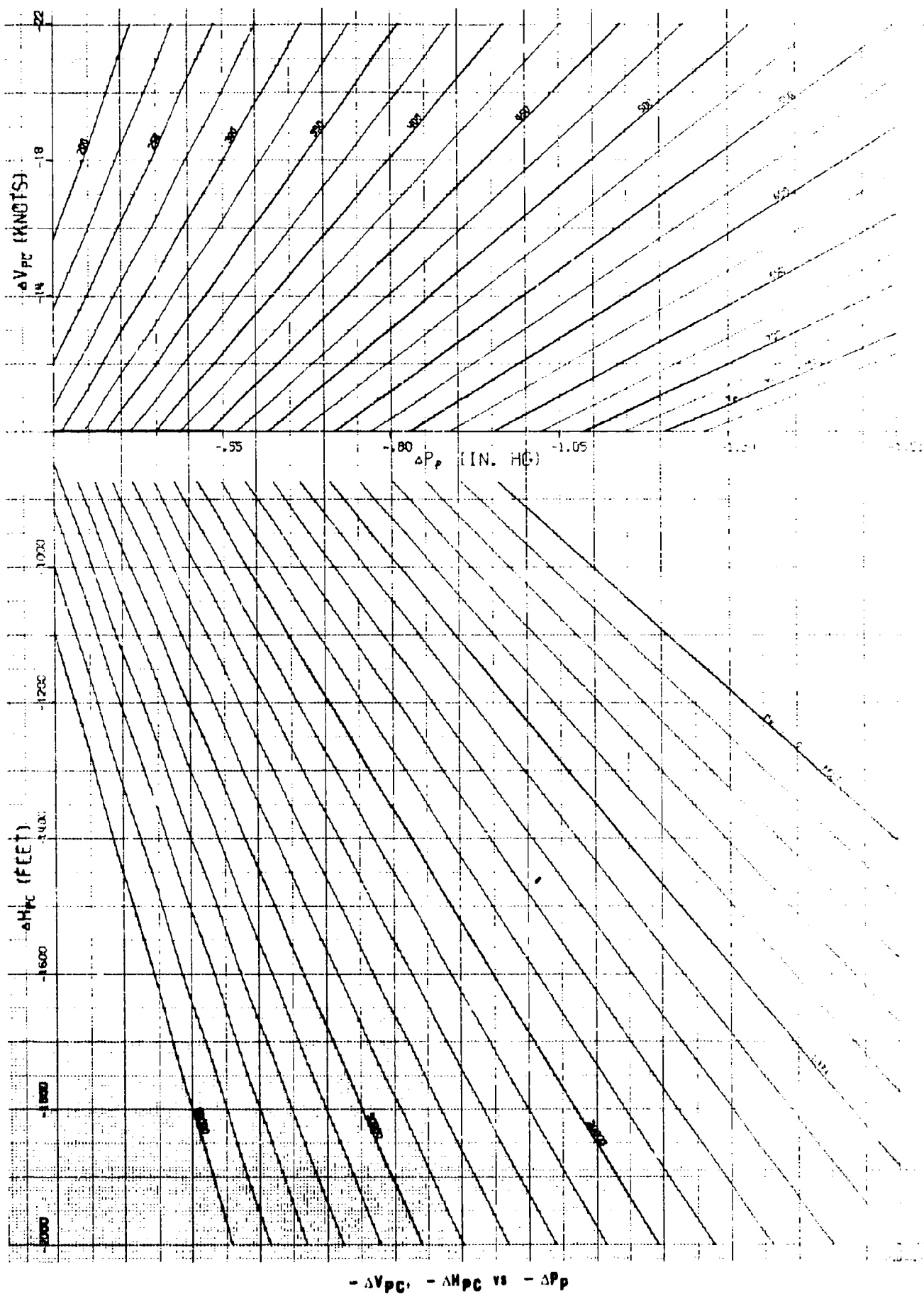


-  $\Delta V_{PC}$ , -  $\Delta H_{PC}$  vs -  $\Delta P_p$

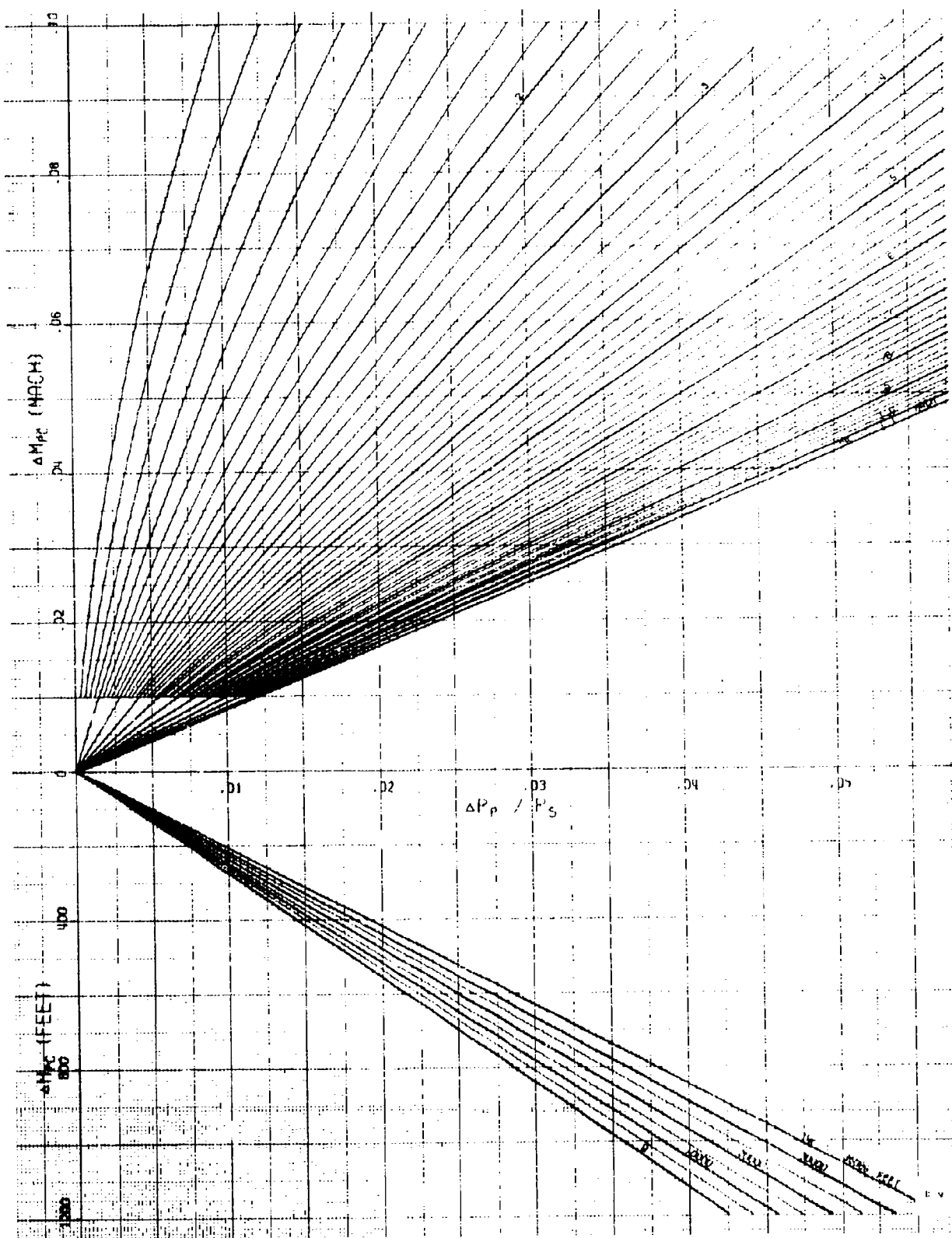


$q = \frac{1}{2} \rho V^2$

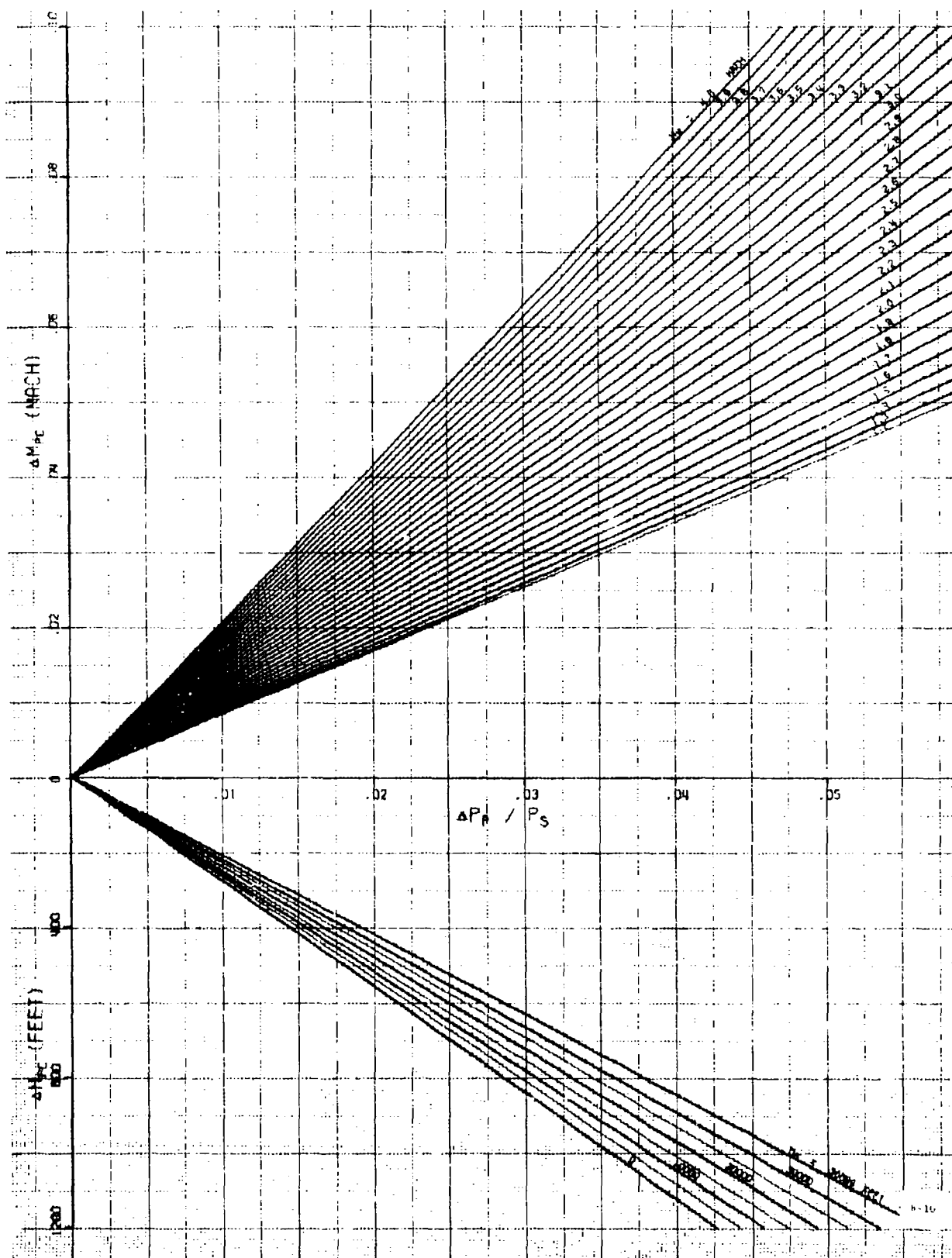




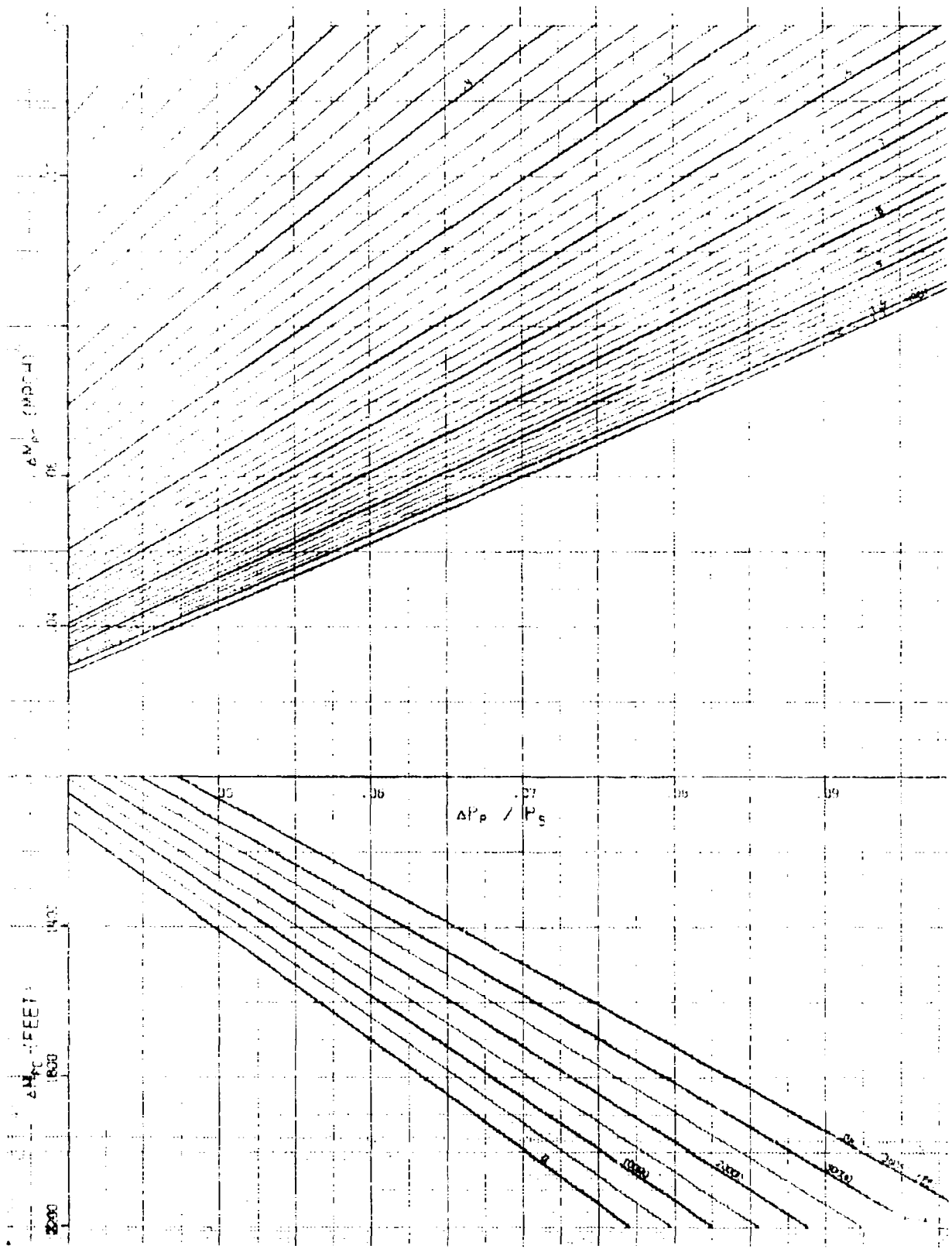
$-\Delta V_{pc}, -\Delta H_{pc}$  vs  $-\Delta P_p$



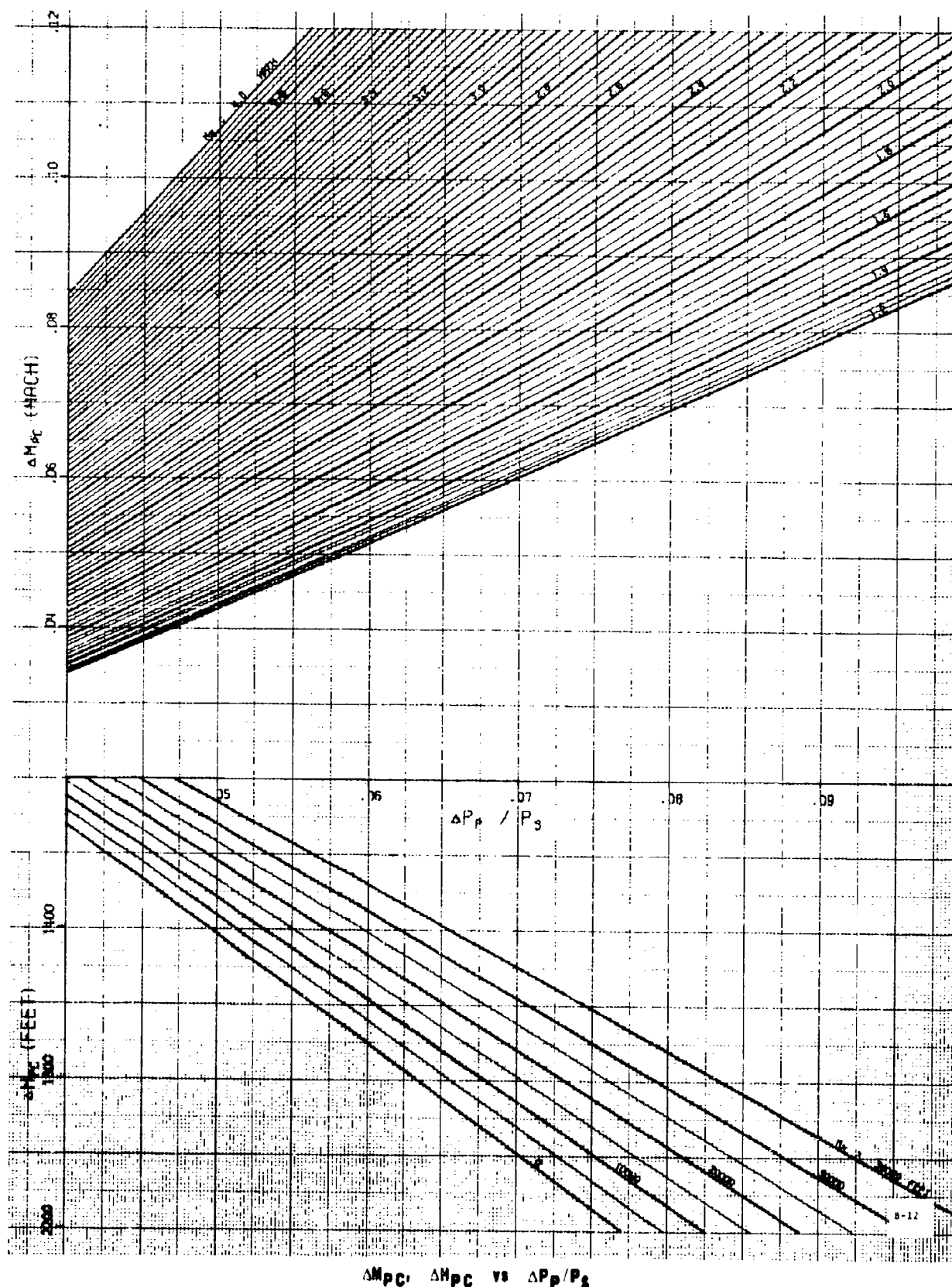
$\Delta M_{pc}, \Delta H_{pc}$  vs  $\Delta P_p / P_s$

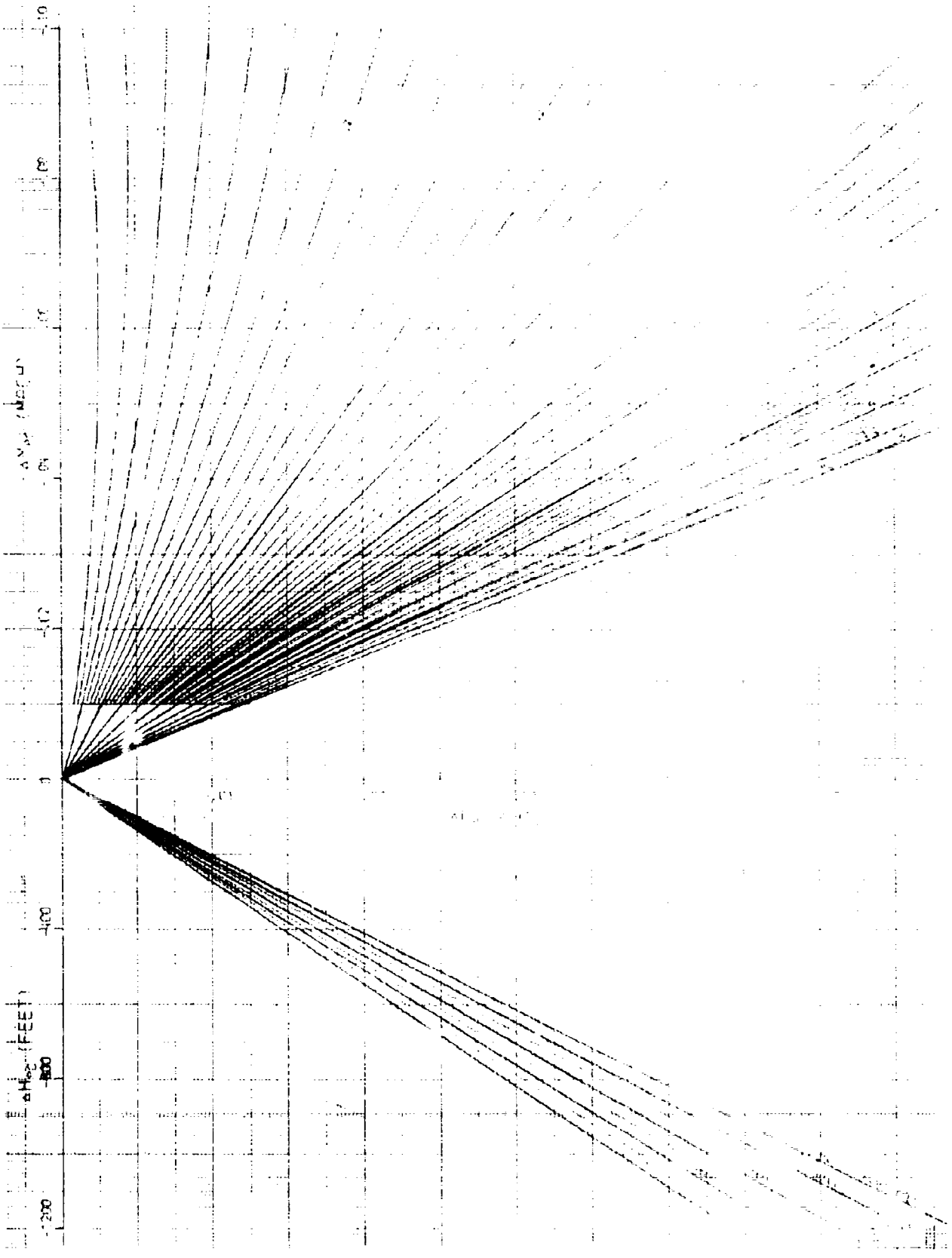


$\Delta H_{pc}$ ,  $\Delta H_{pc}$  vs  $\Delta P_p / P_s$

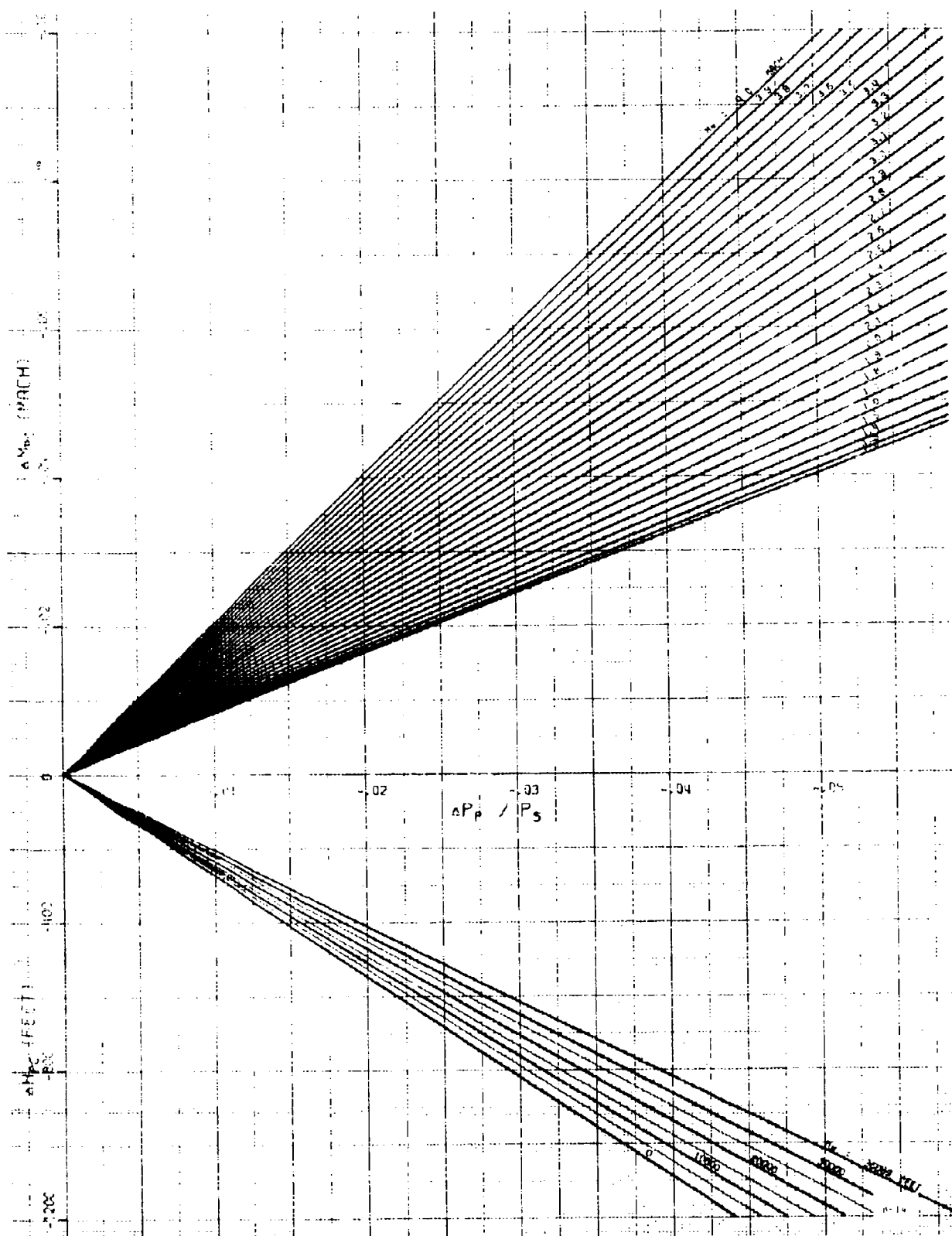


$\Delta P_p$ ,  $\Delta H_p$  vs  $\Delta P_p / P_s$

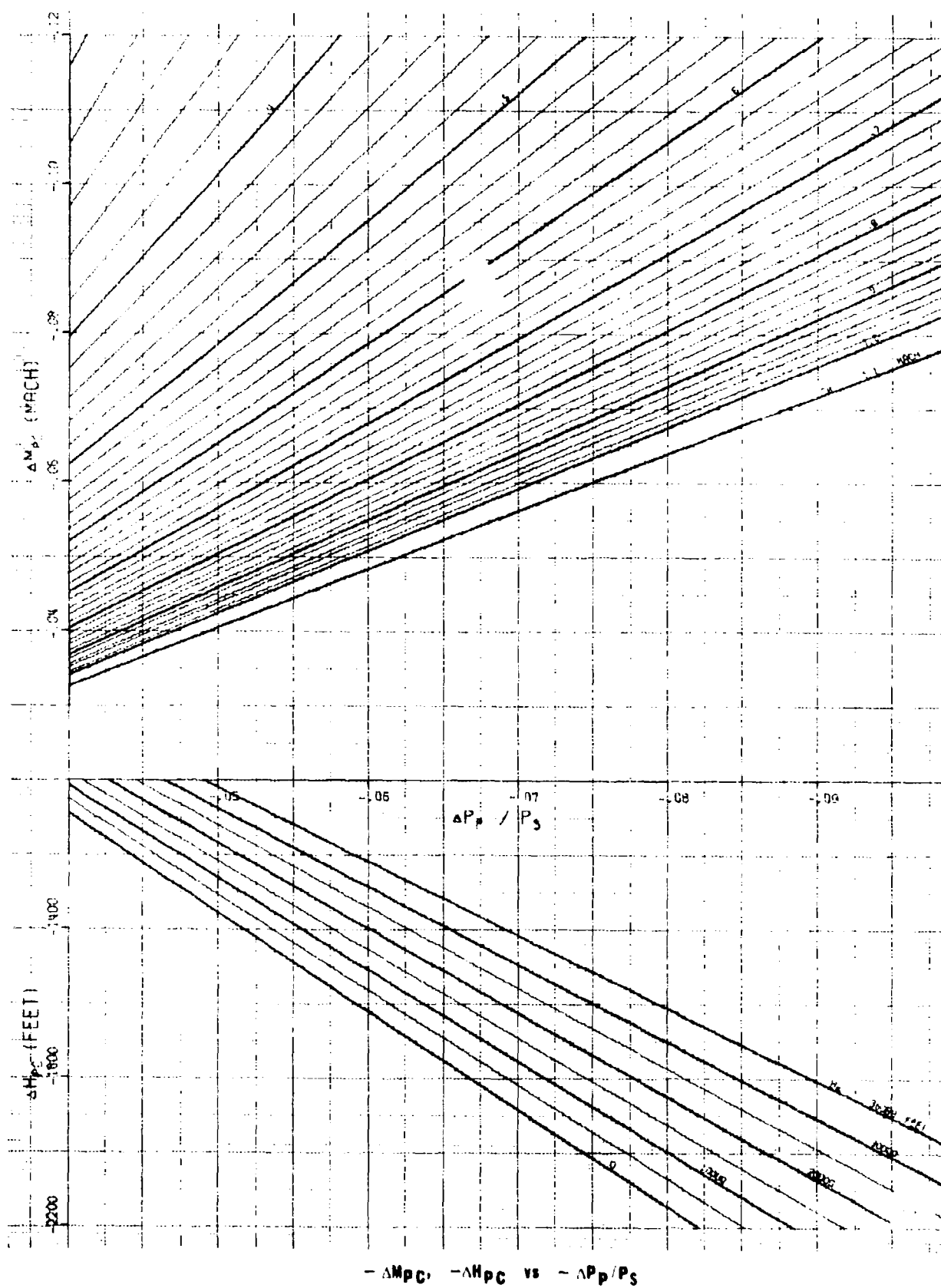




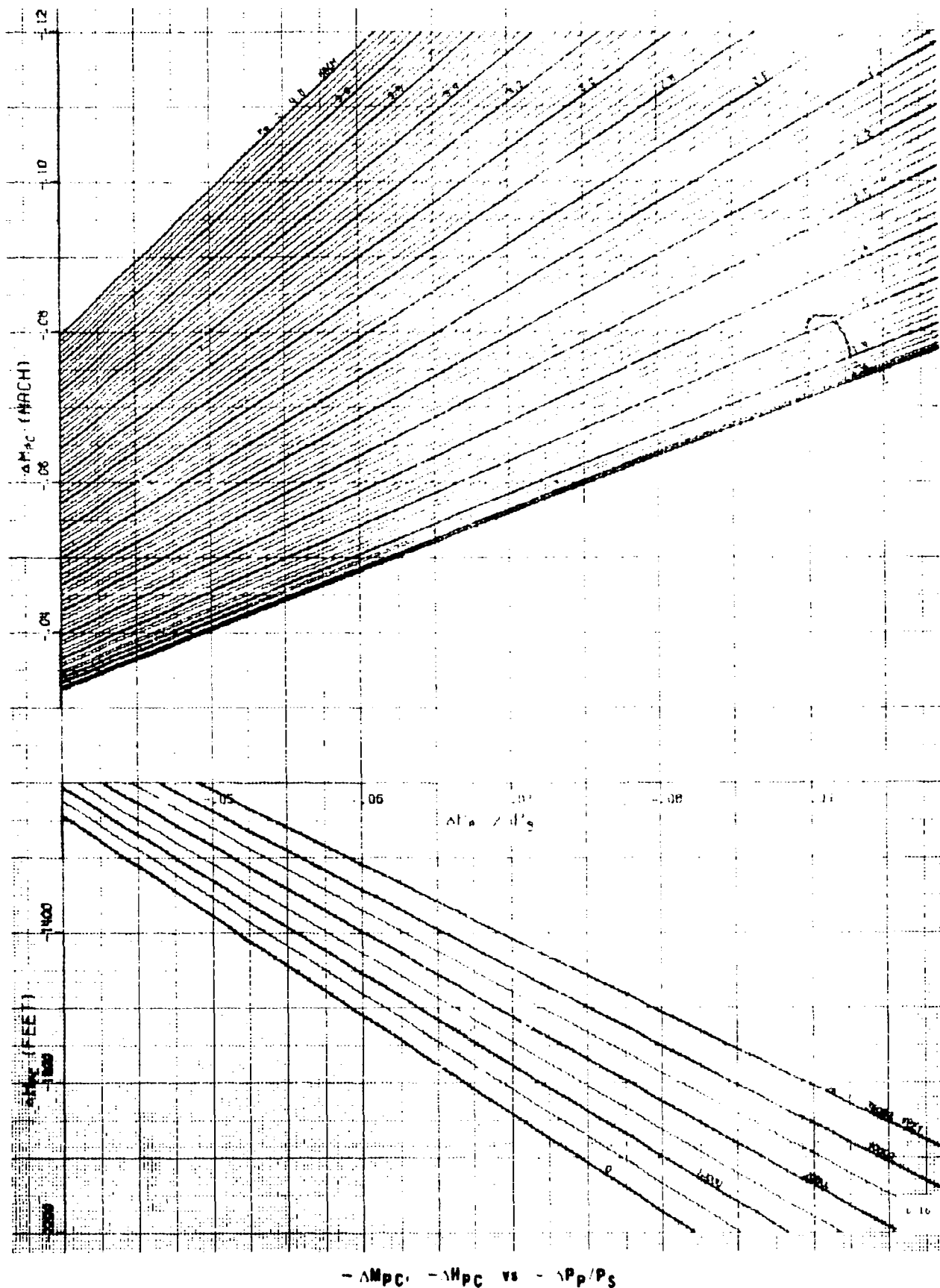
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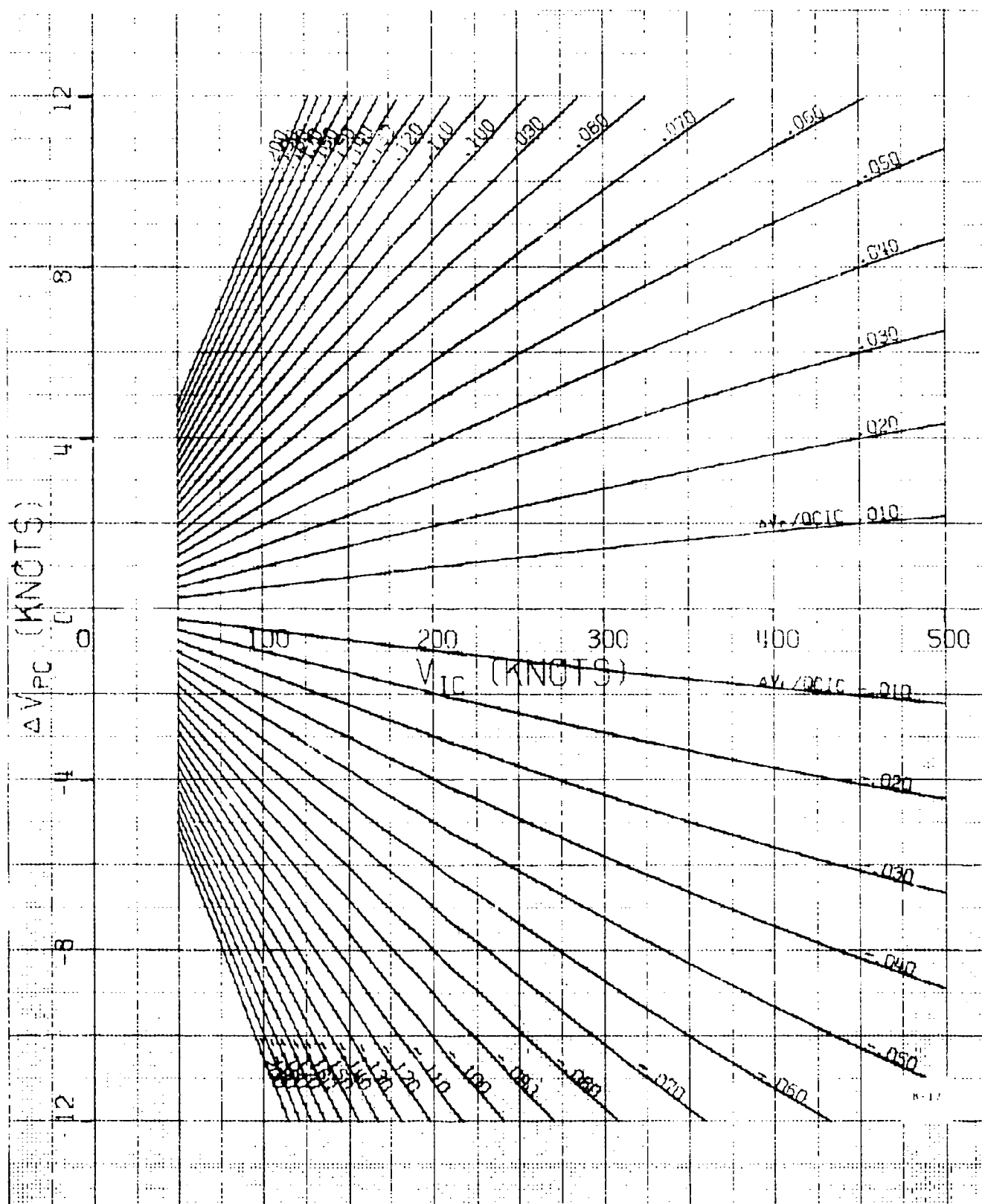
$-\Delta M_{pc}$ ,  $-\Delta H_{pc}$  vs  $-\Delta P_p/P_s$



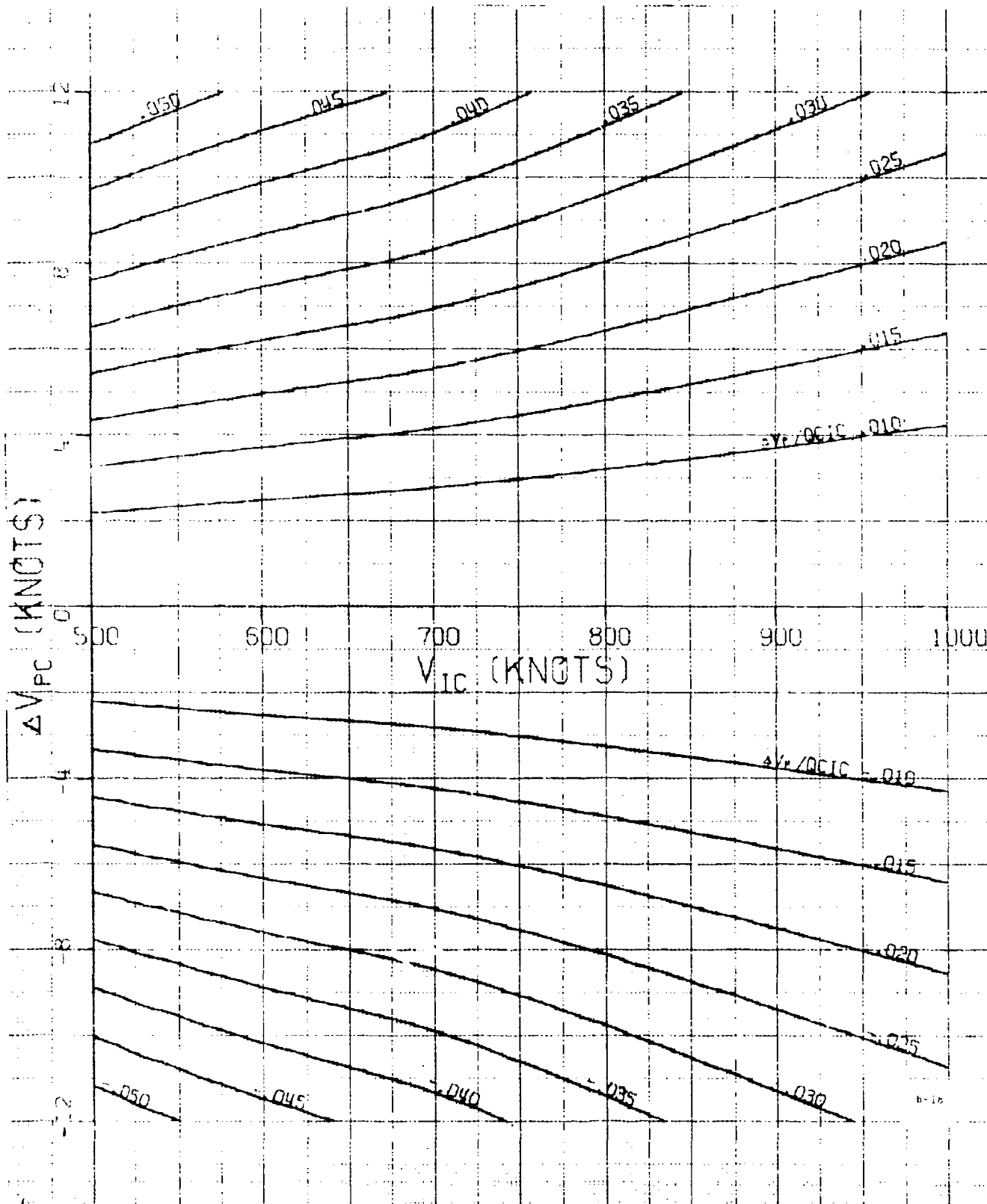




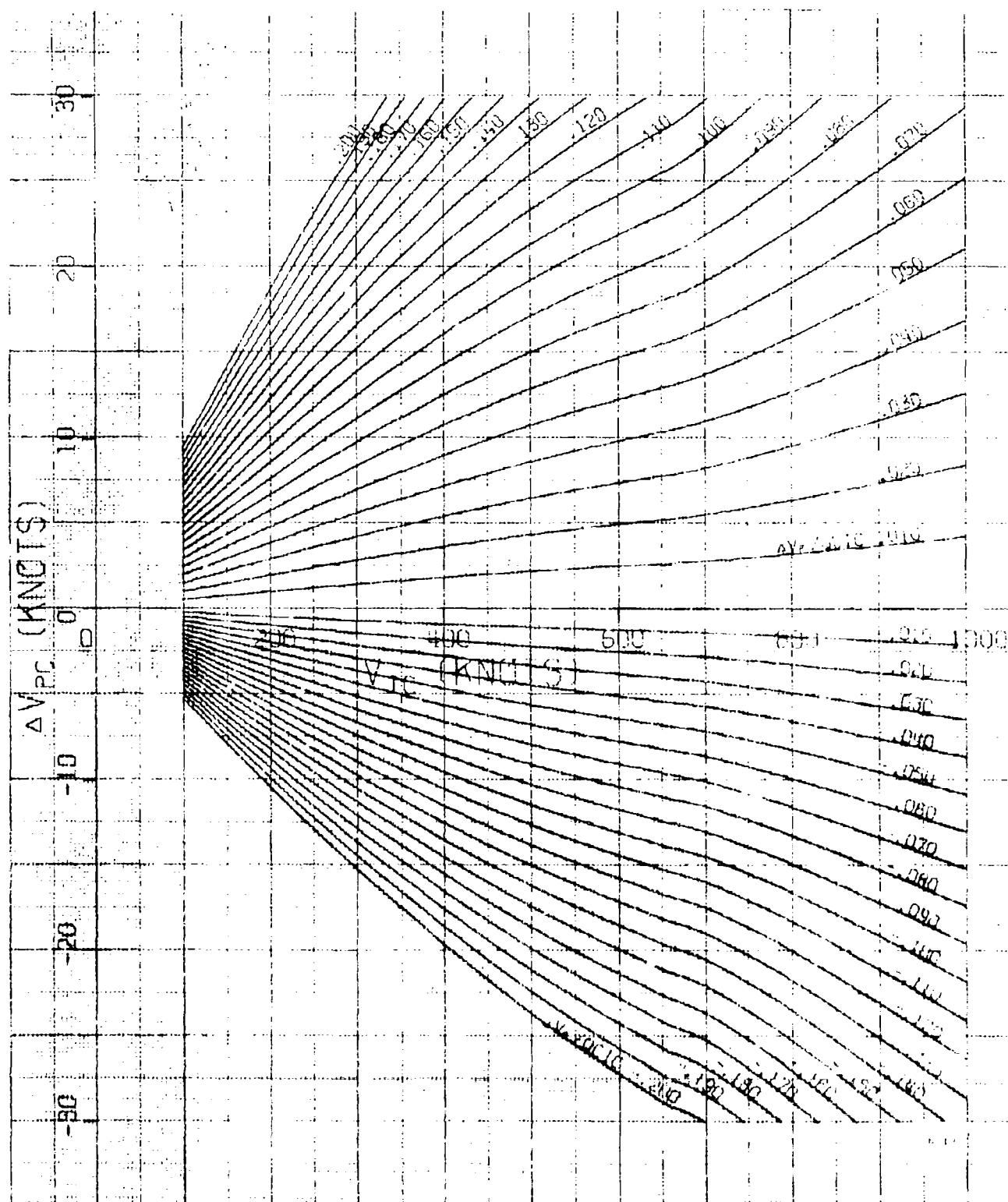
$-\Delta H_{pc}$ ,  $-\Delta H_{pc}$  vs  $-\Delta P_p / P_s$



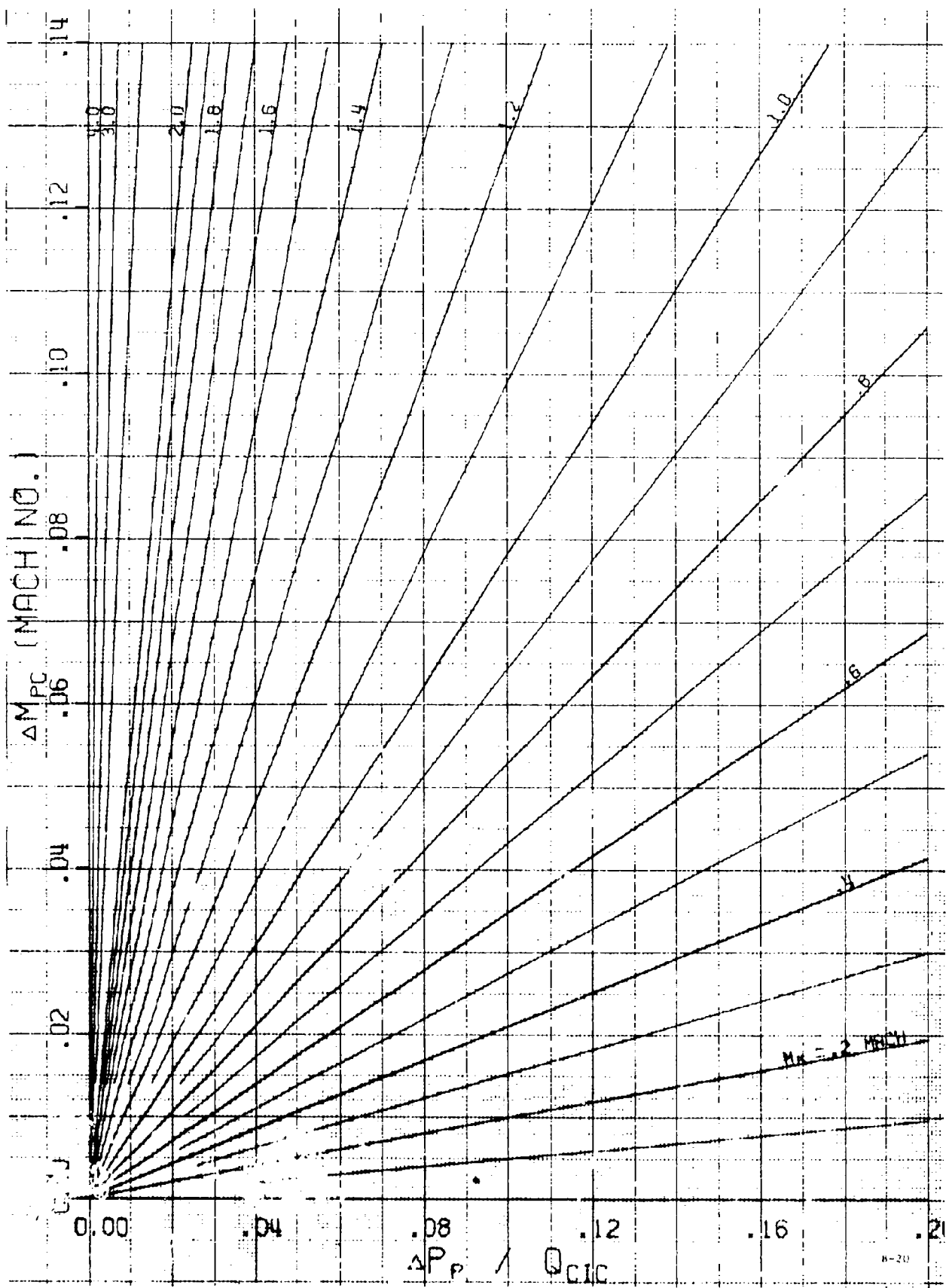
$$\Delta V_{PC} \text{ vs } V_{IC} \quad \frac{\Delta P_P}{q_{CIC}} = \text{CONST}$$



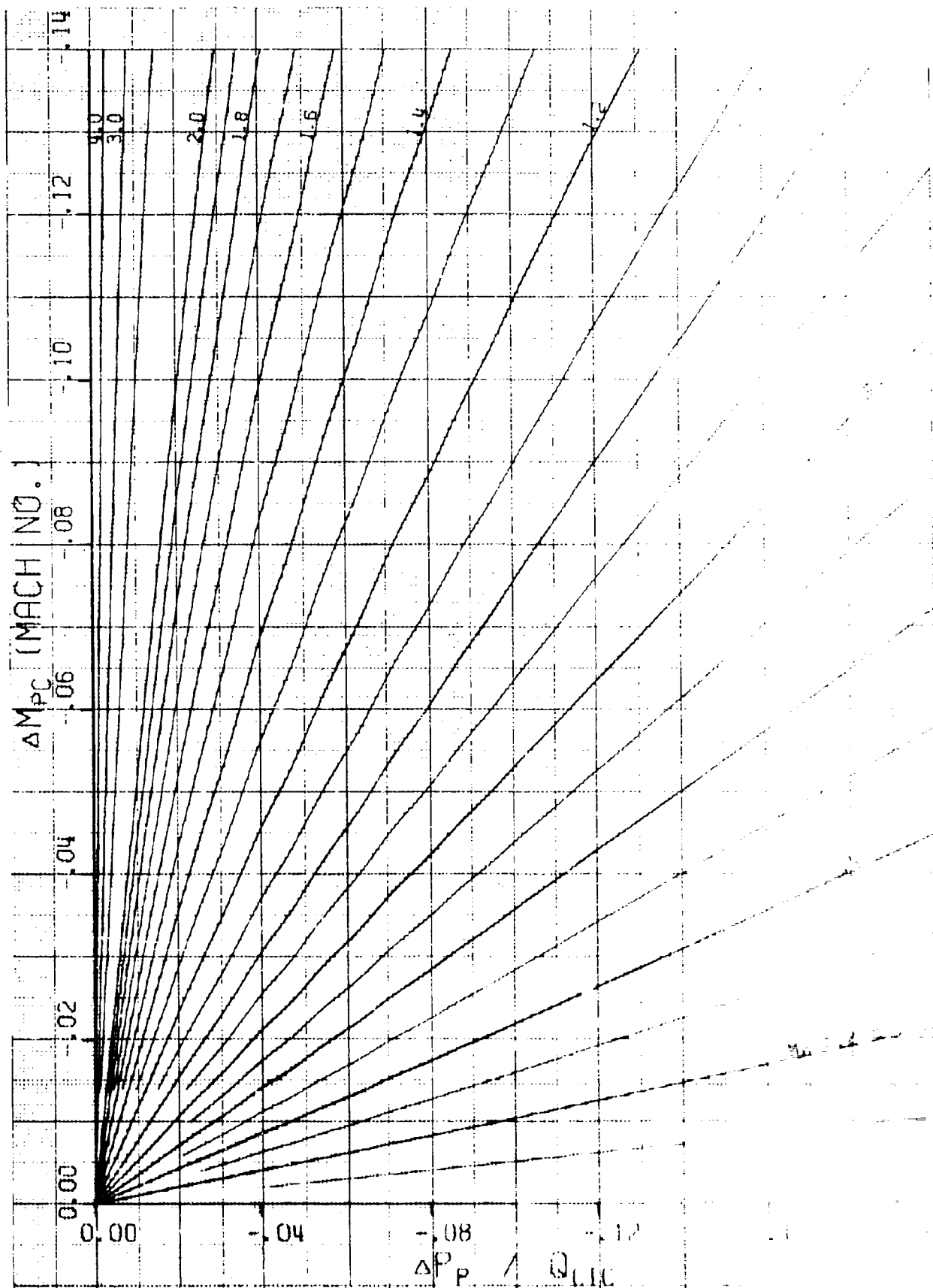
$\Delta V_{PC}$  vs  $V_{IC}$  -  $\frac{\Delta P_P}{q_{CIC}}$  - CONST



$$\Delta V_{PC} = V_{TC} \cdot \frac{\Delta V_{PC}}{V_{TC}} \quad \text{CONST}$$



C

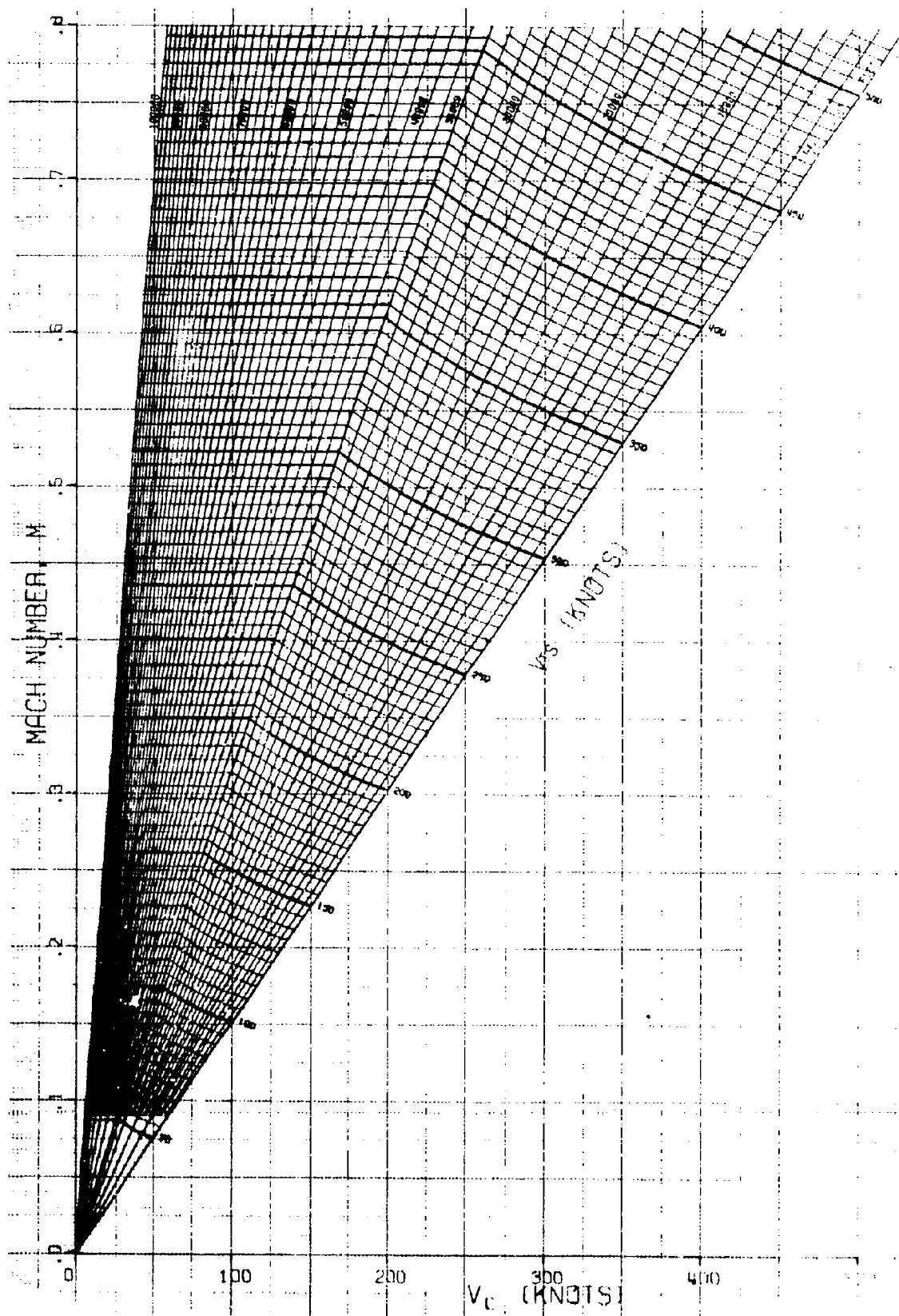


## APPENDIX C

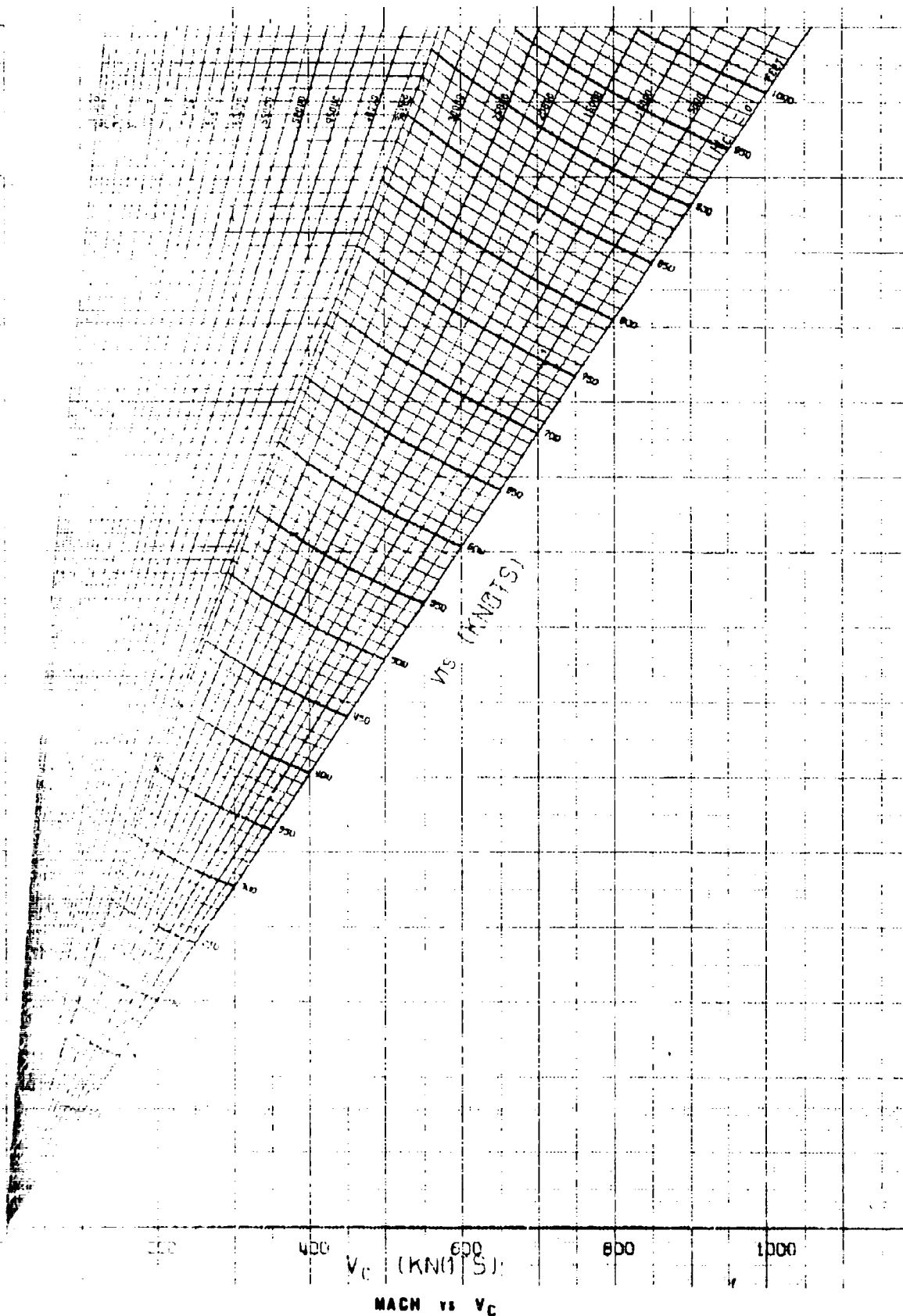
Mach Number  $M$  versus Calibrated Airspeed  $V_c$  for  
Pressure Altitude  $H_c = \text{Constant}$  with lines of  
Standard Day True Speed  $V_e = \text{Constant}$ .

(Also  $M_{ic}$  versus  $V_{ic}$  for  $H_{ic} = \text{Constant}$ )

APRIL 1967

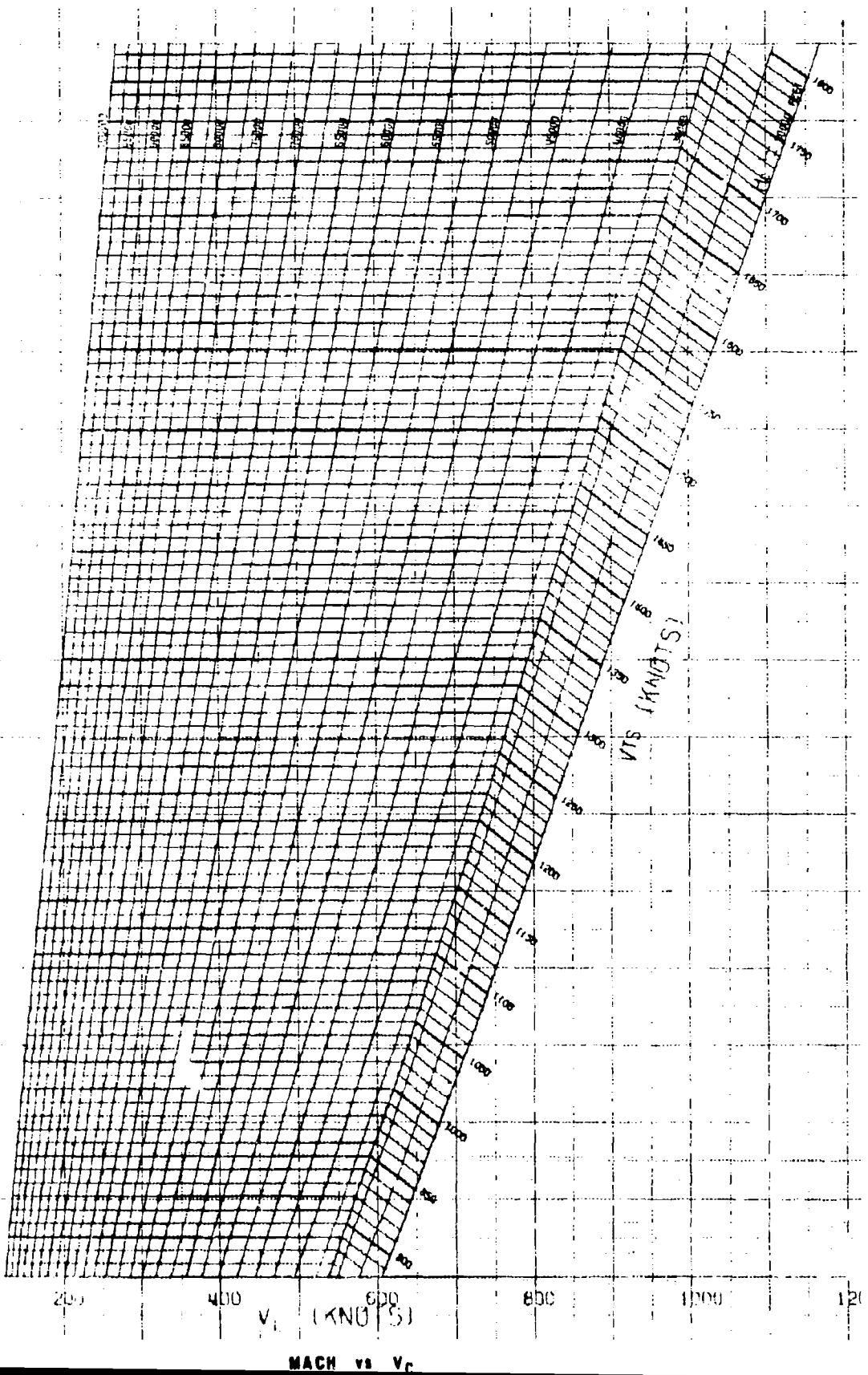


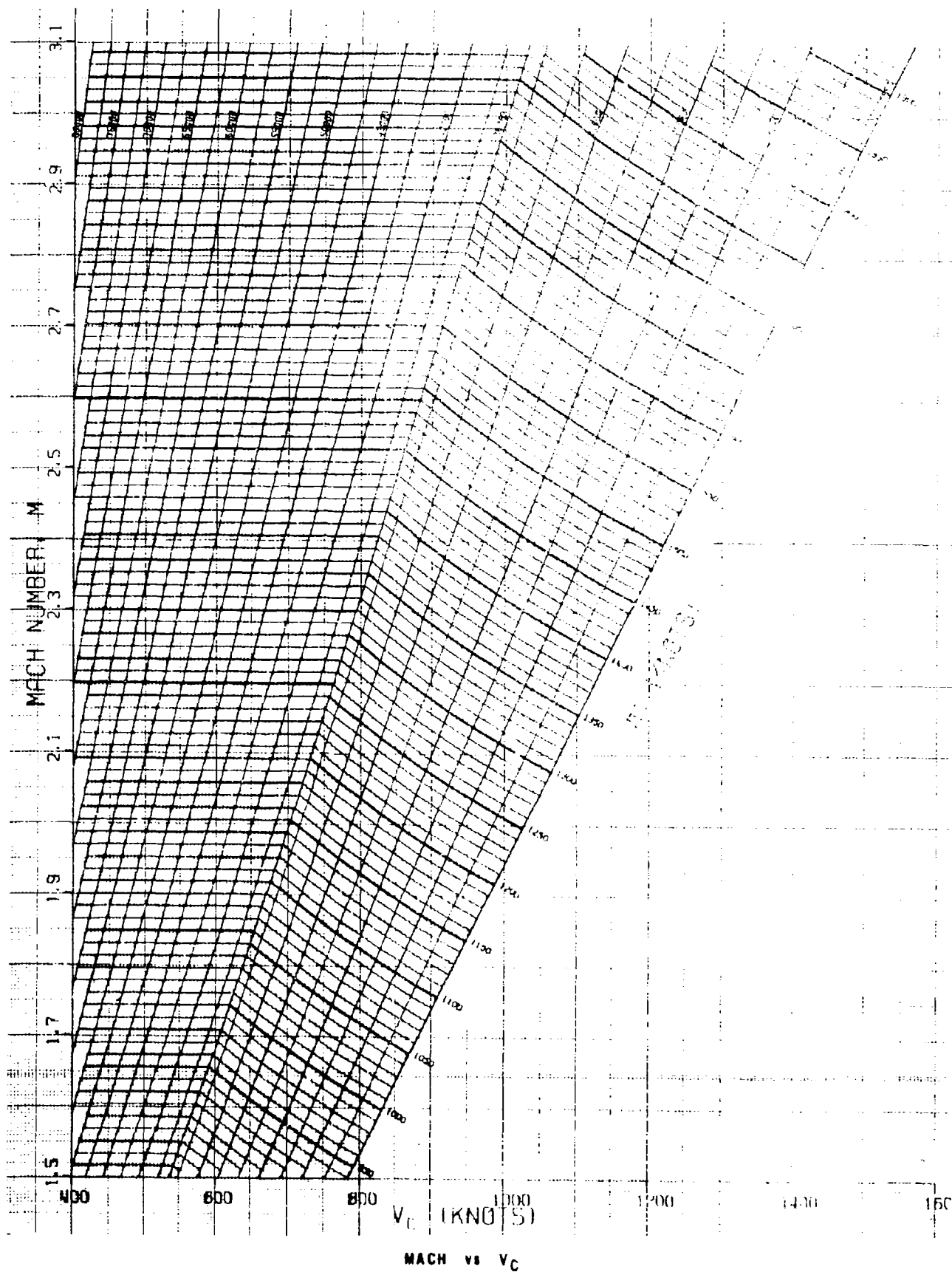


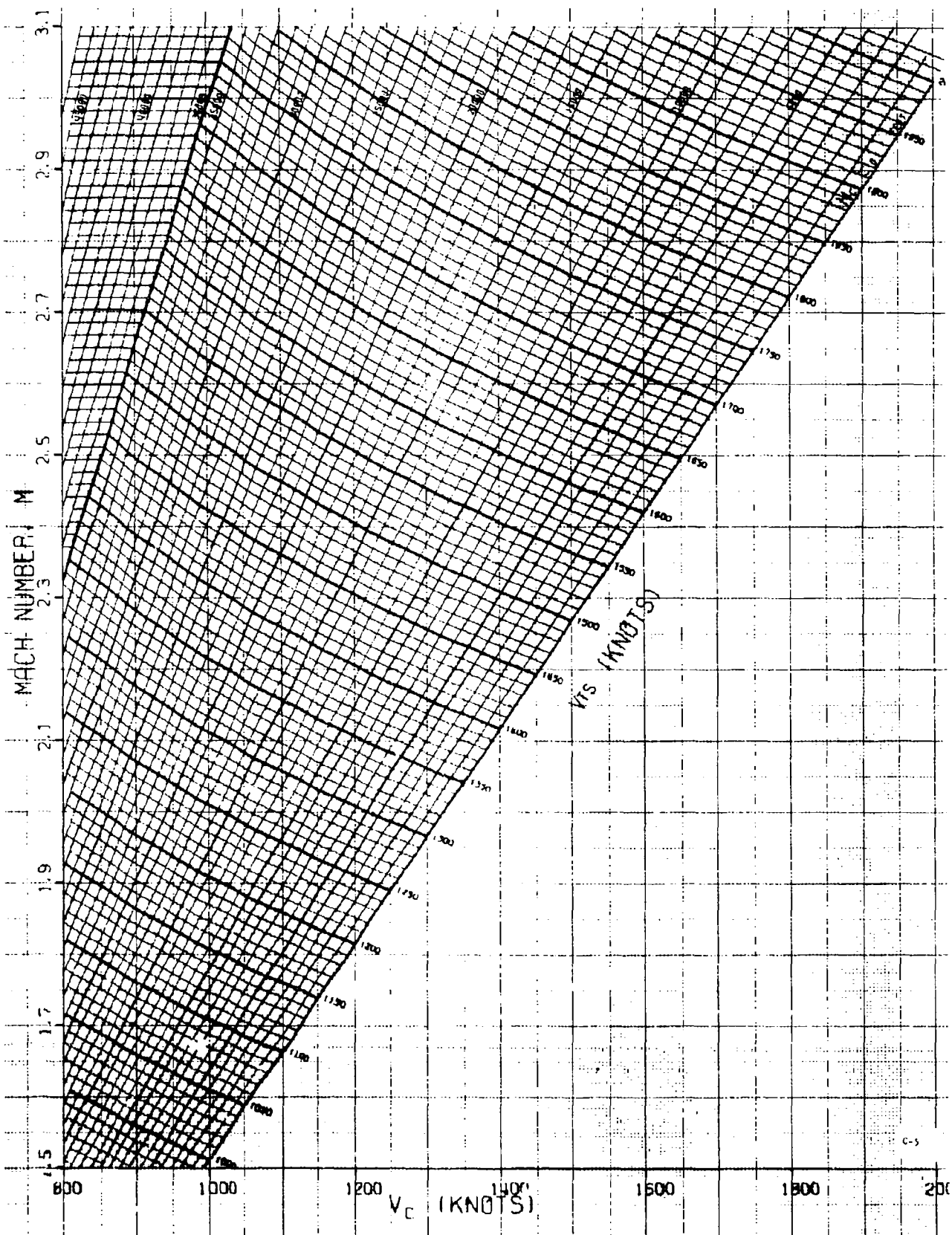


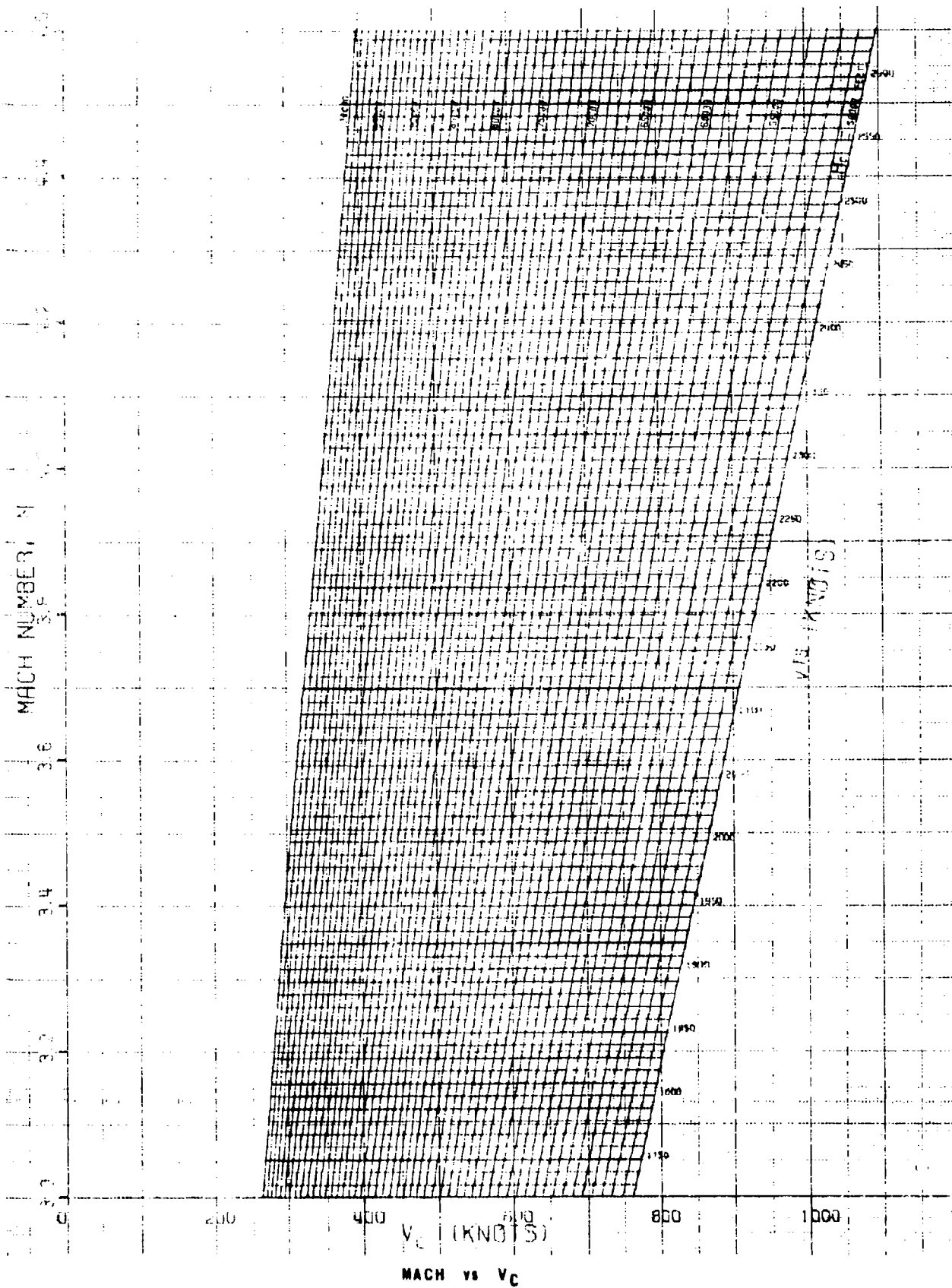
C

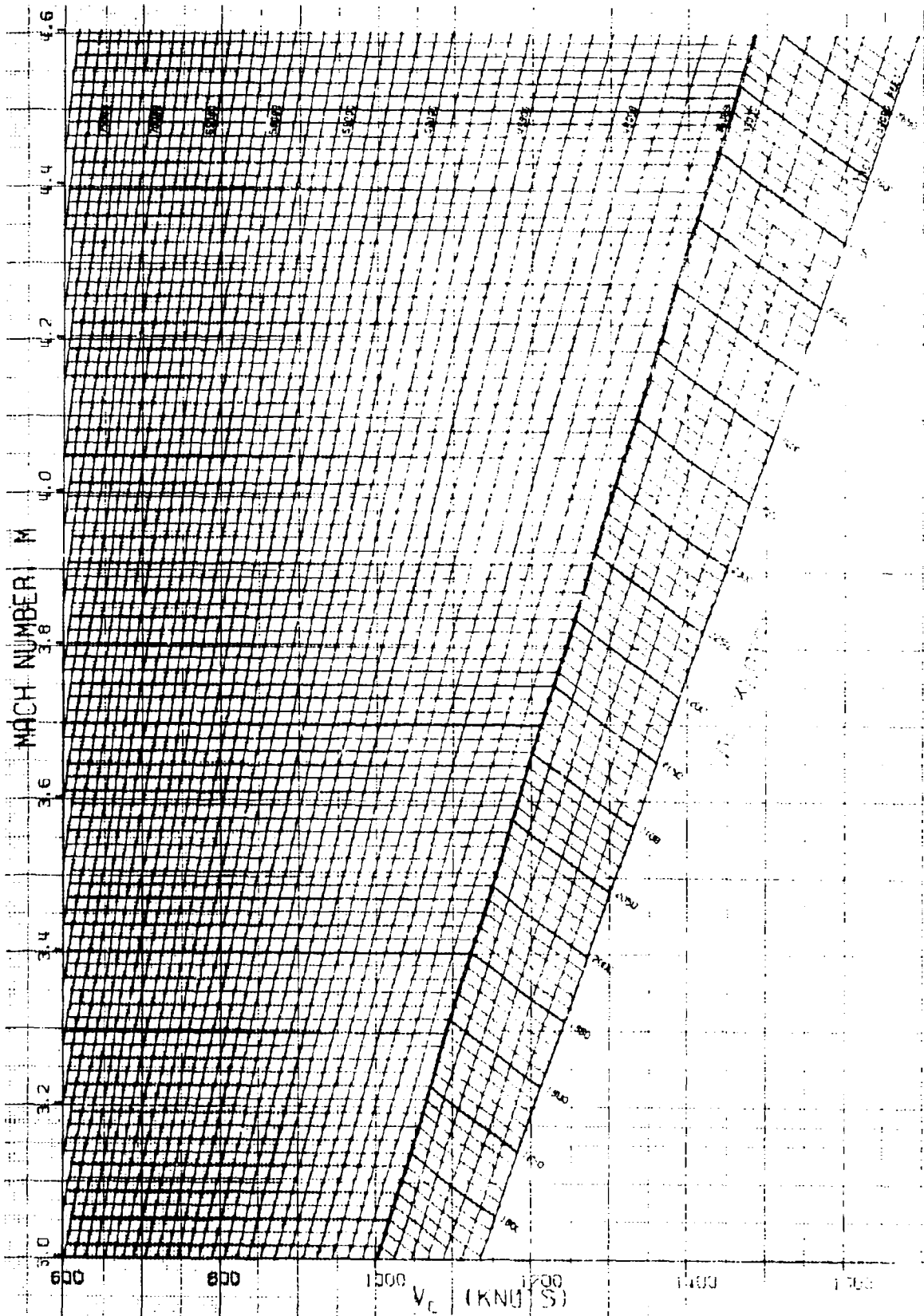
WIND SPEED, K

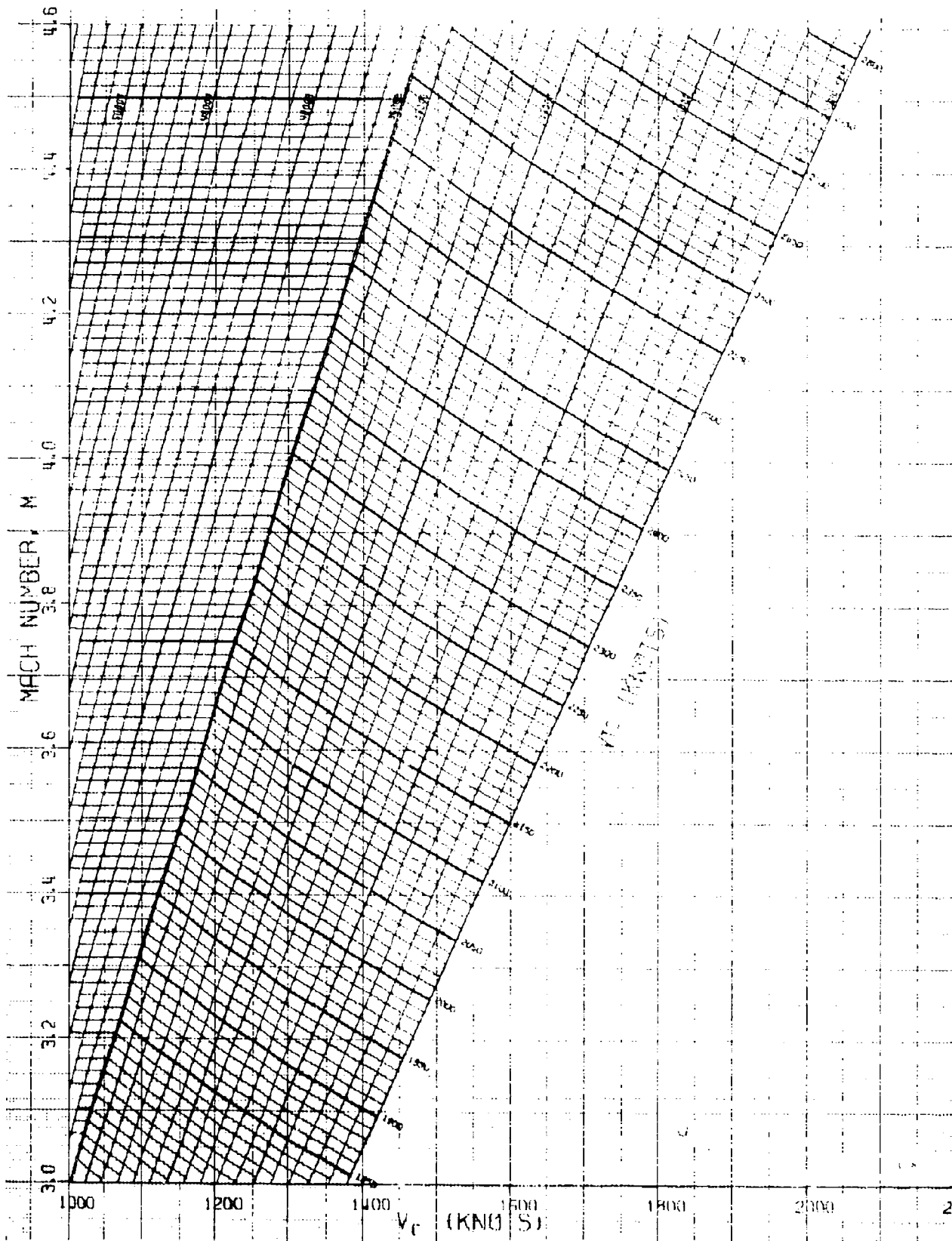


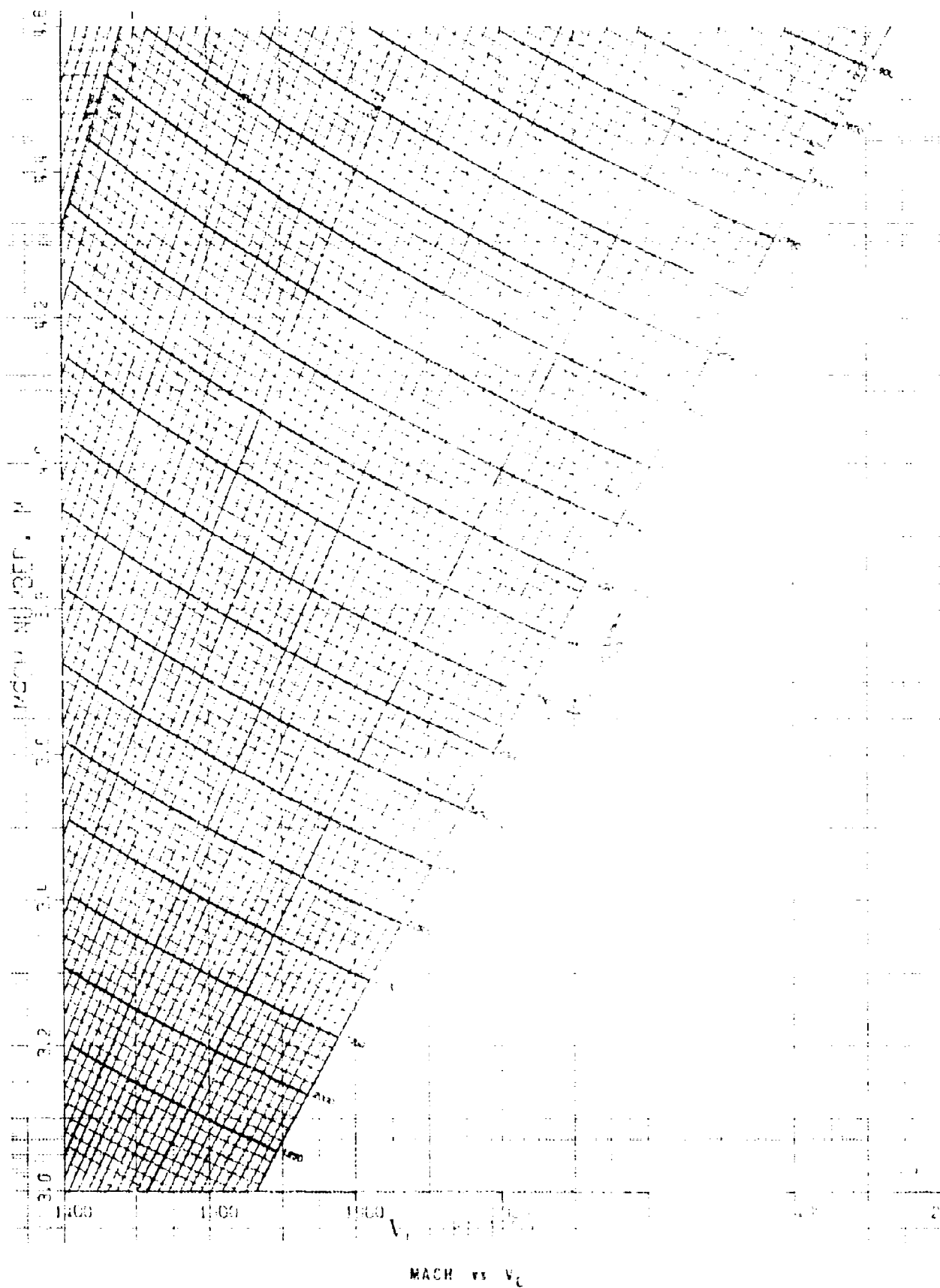




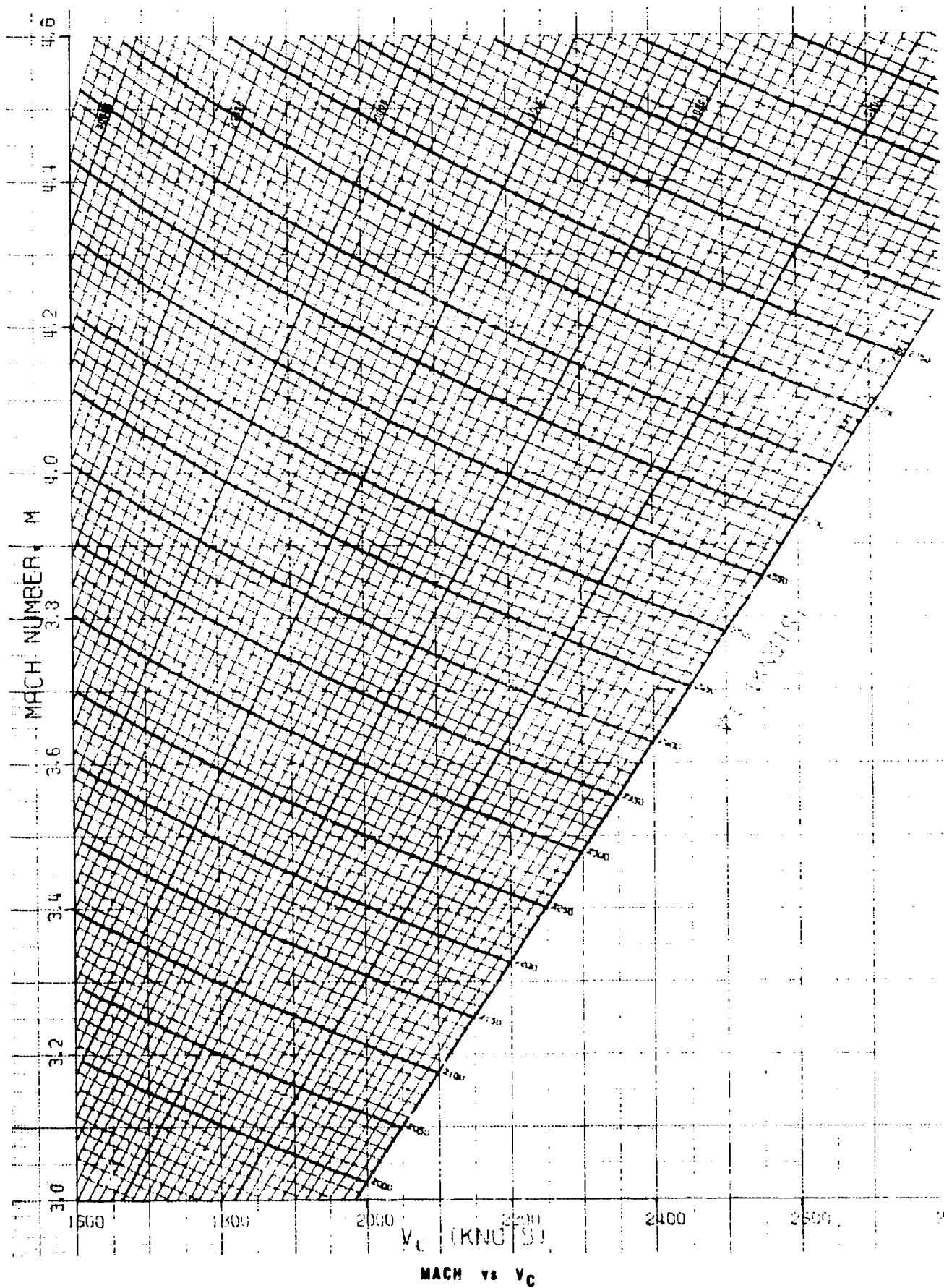












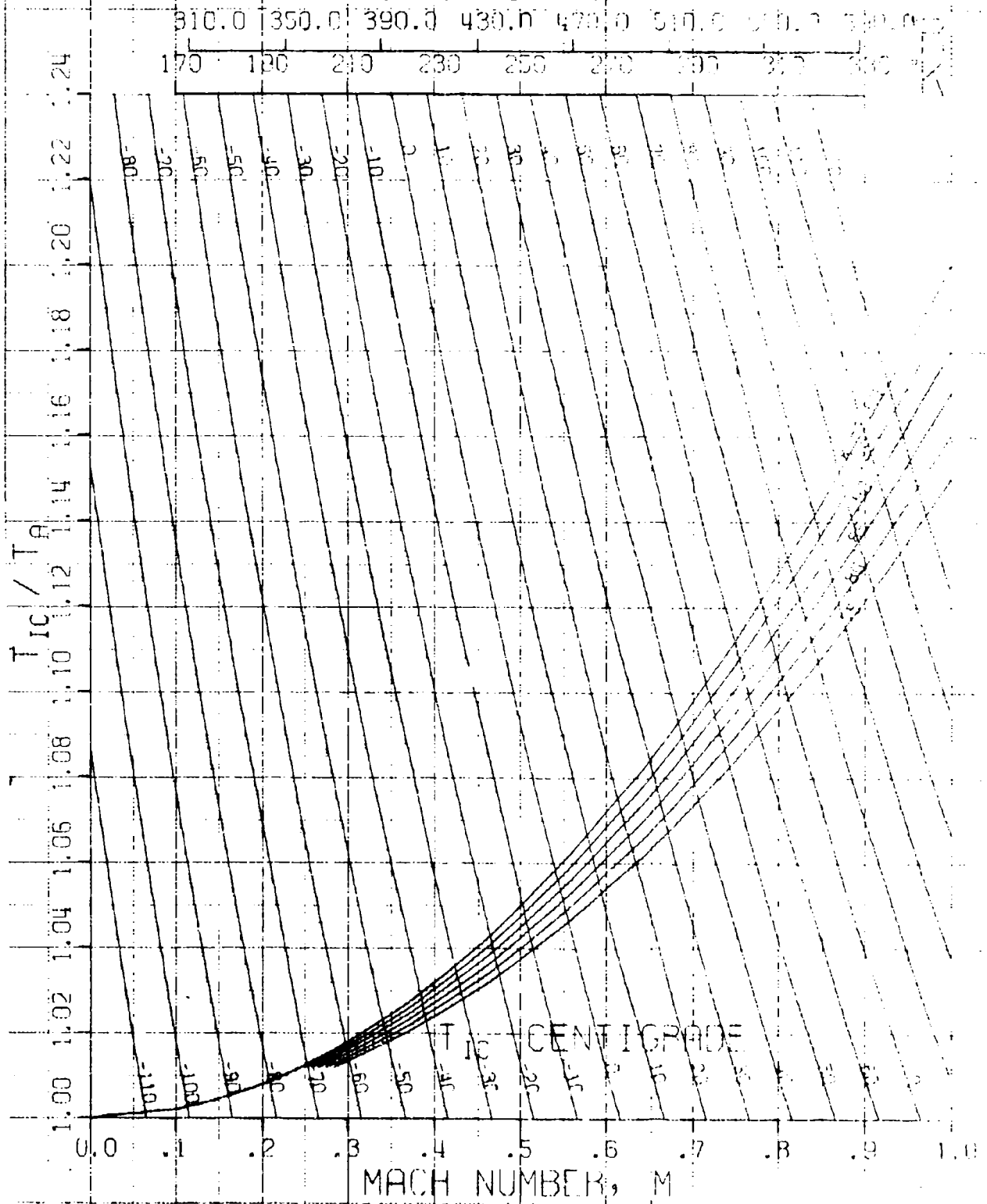
APPENDIX D

ATMOSPHERE CHARTS

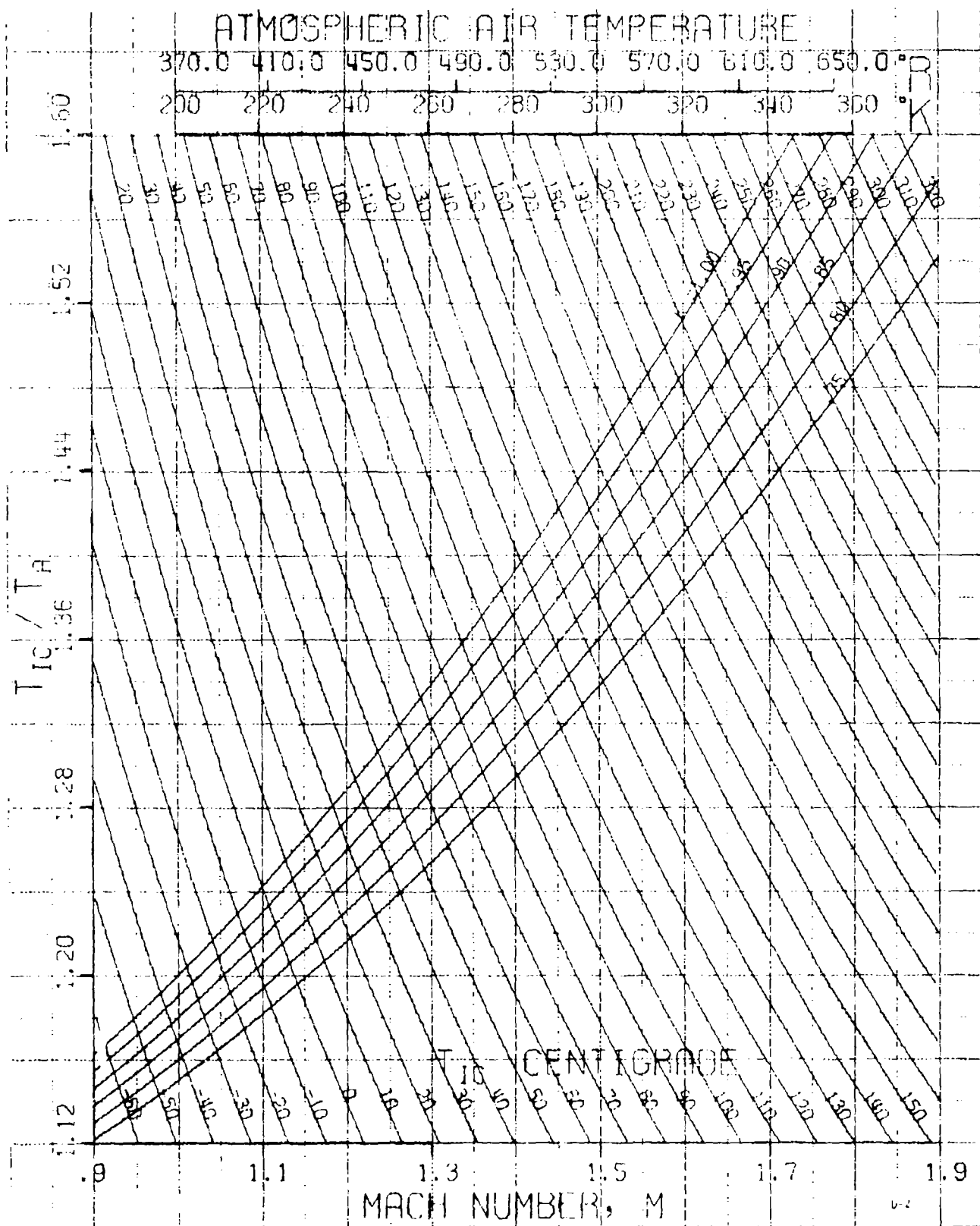
<u>PAGE NUMBER</u>	<u>TITLE</u>
D-1 - D-5	TIC/TA vs MACH
D-6 - D-13	V <sub>True</sub> vs TA

APRIL 1967

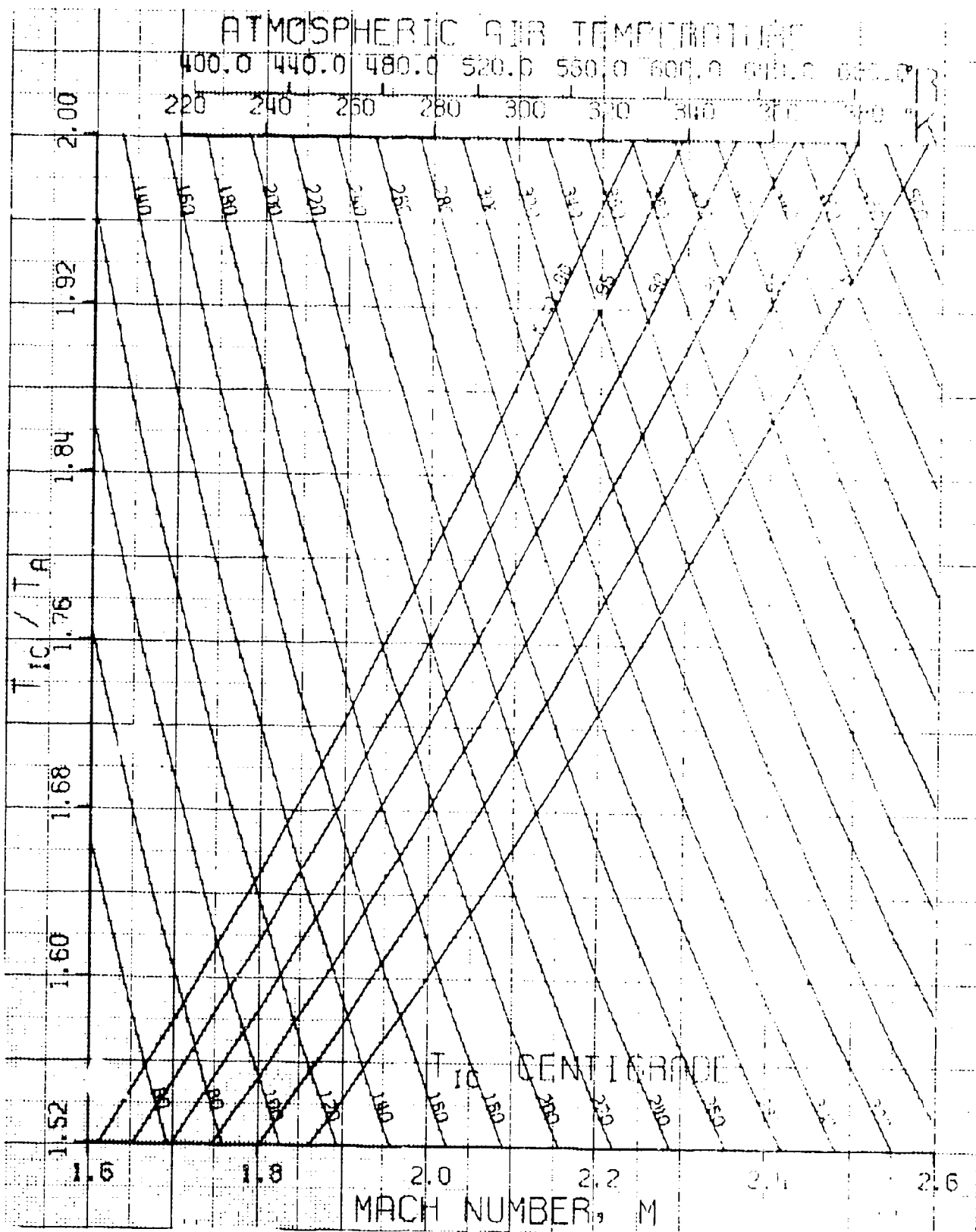
# ATMOSPHERIC AIR TEMPERATURE



$T_{IC} / T_A$  vs MACH



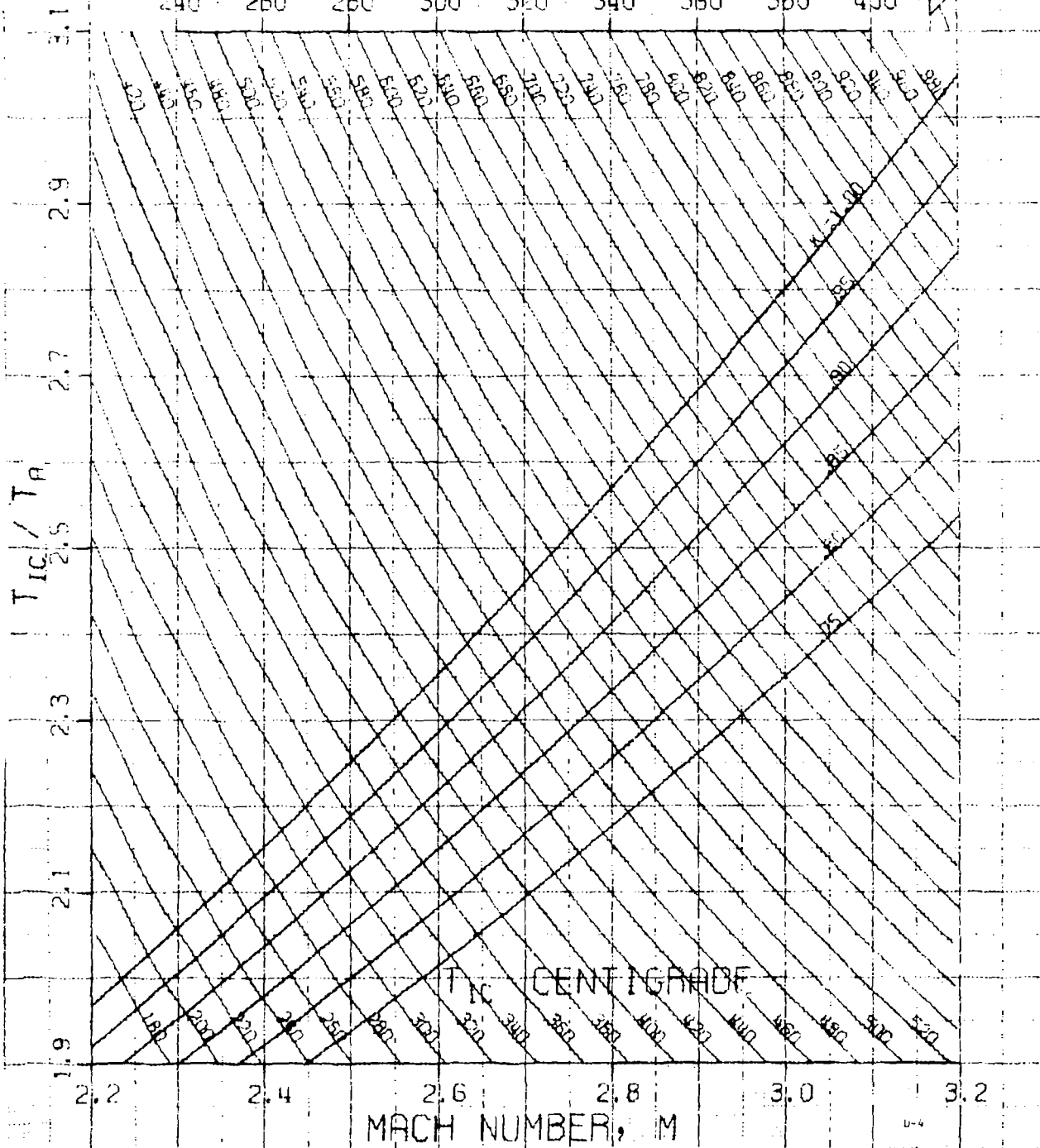
$T_{IC} / T_A$  vs MACH



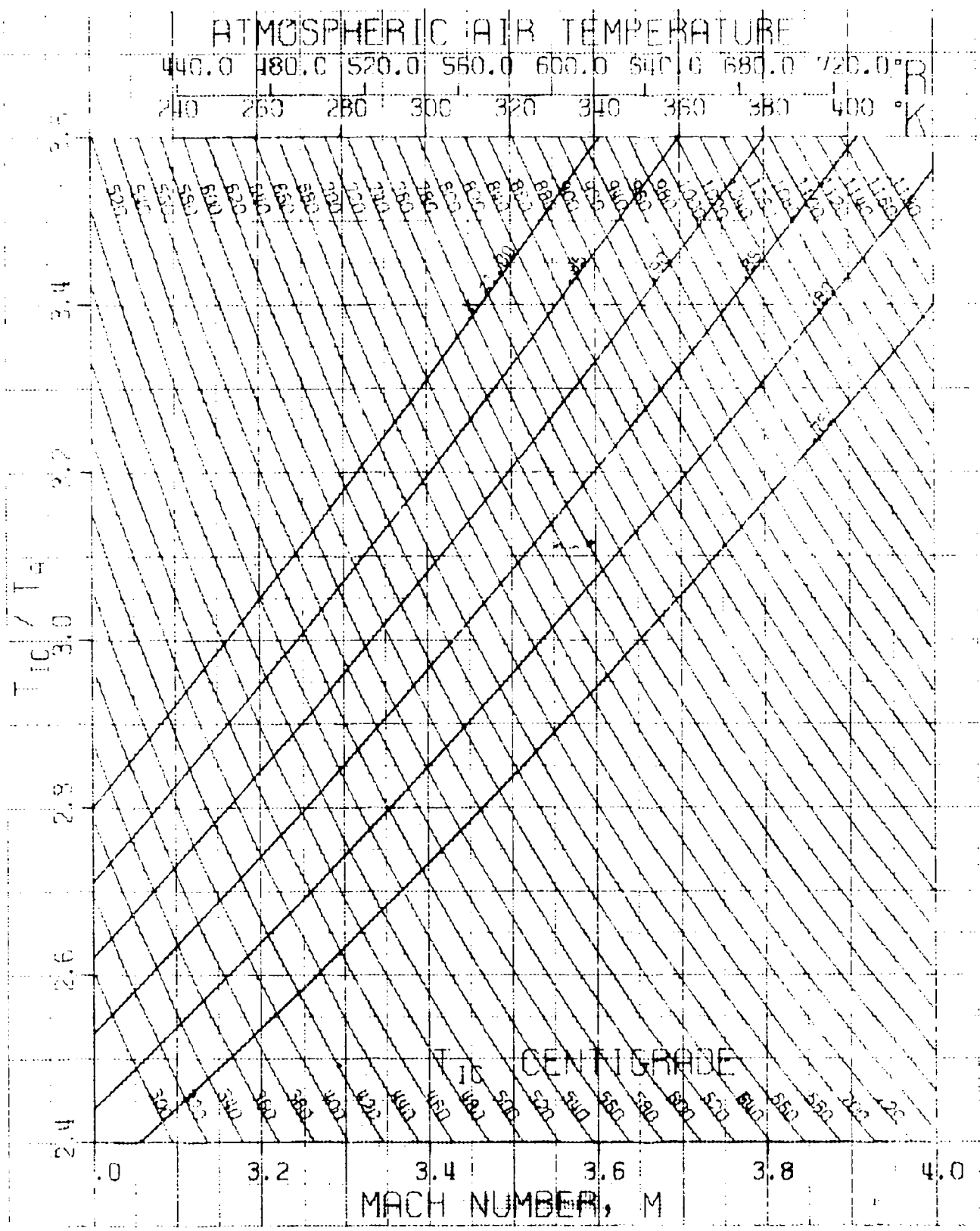
$T_{IC} / T_A$  vs MACH

# ATMOSPHERIC AIR TEMPERATURE

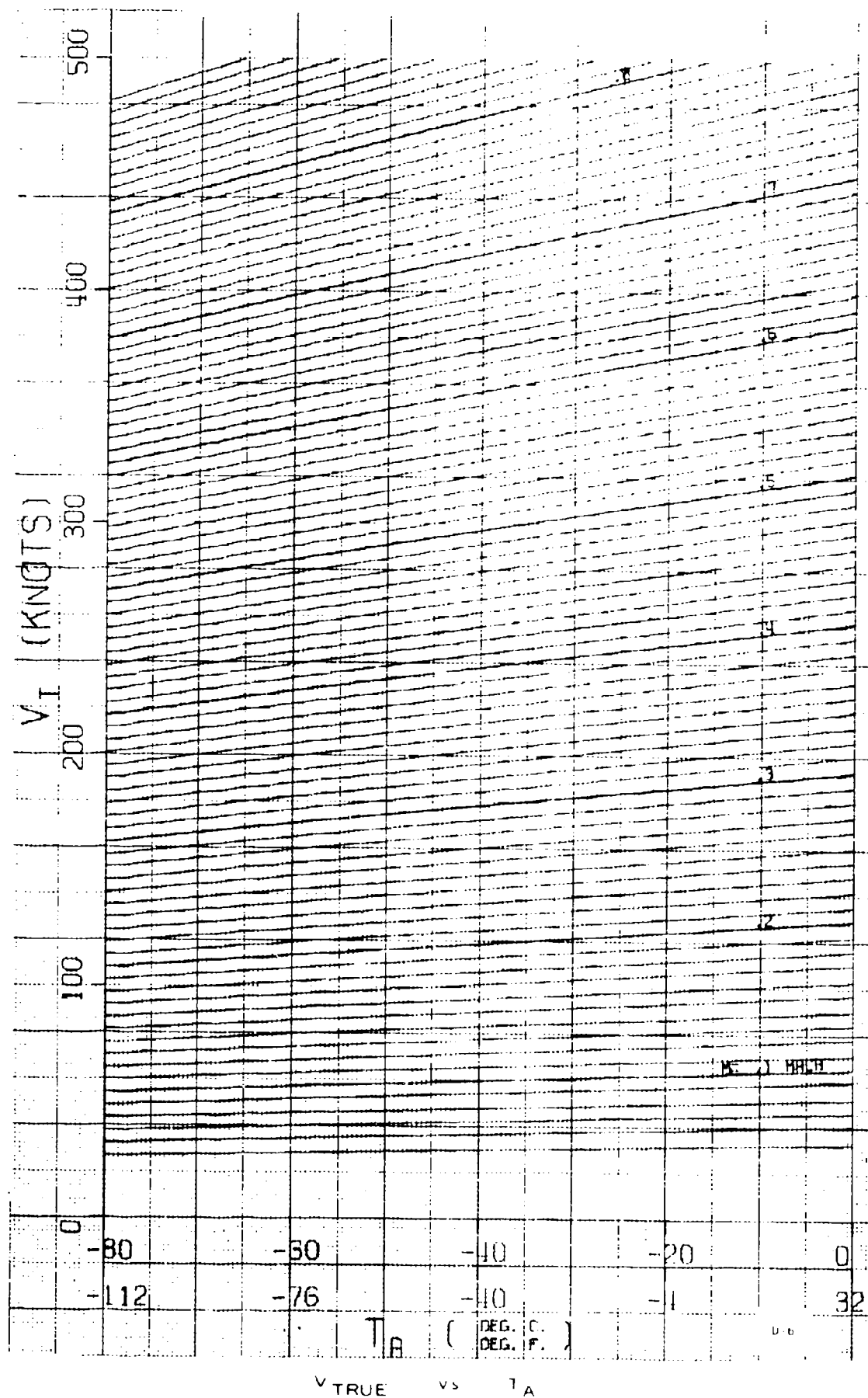
440.0 460.0 480.0 500.0 520.0 540.0 560.0 580.0 600.0 °R  
 240 260 280 300 320 340 360 380 400 °K



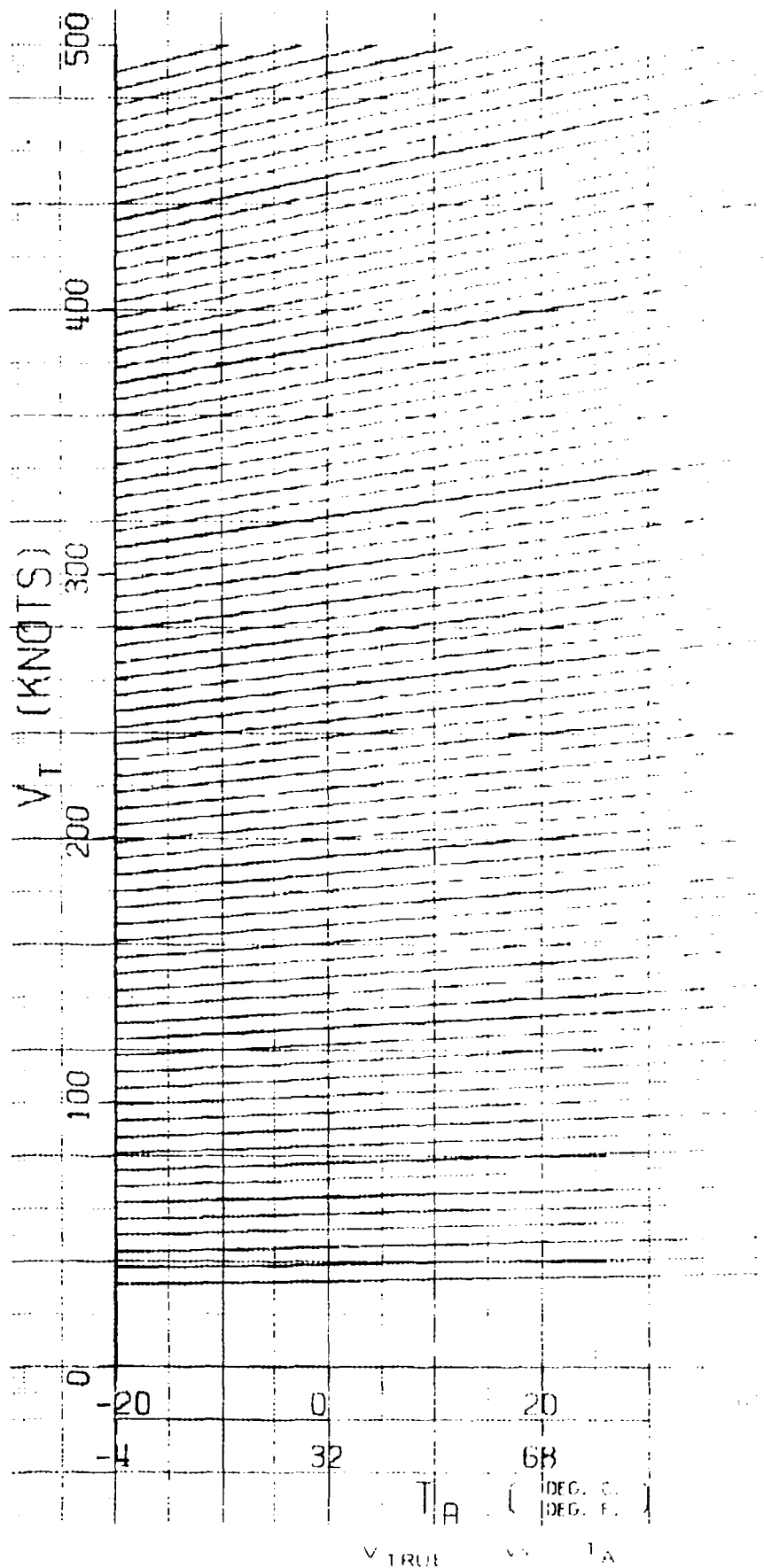
$T_{IC}/T_A$  vs MACH

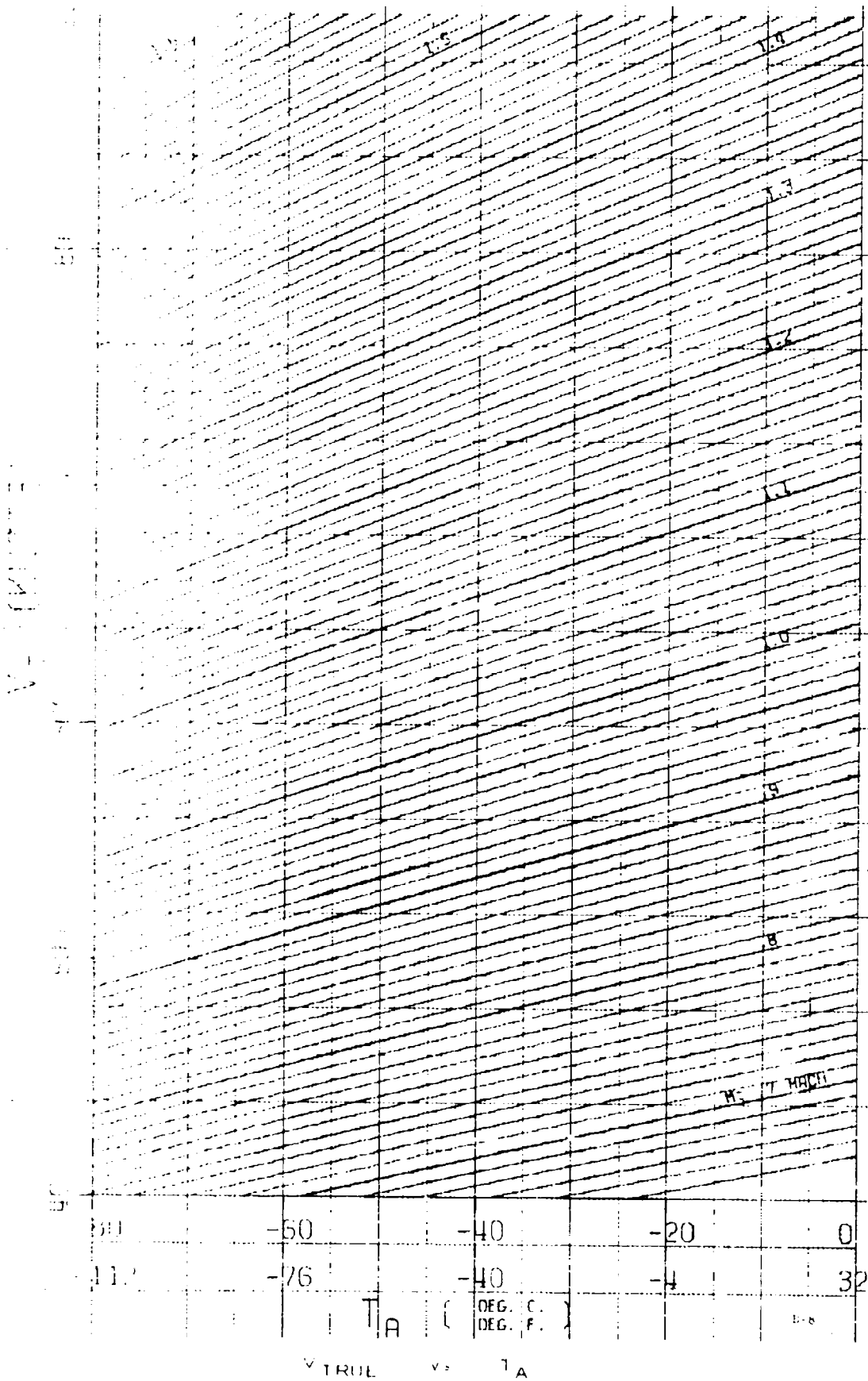


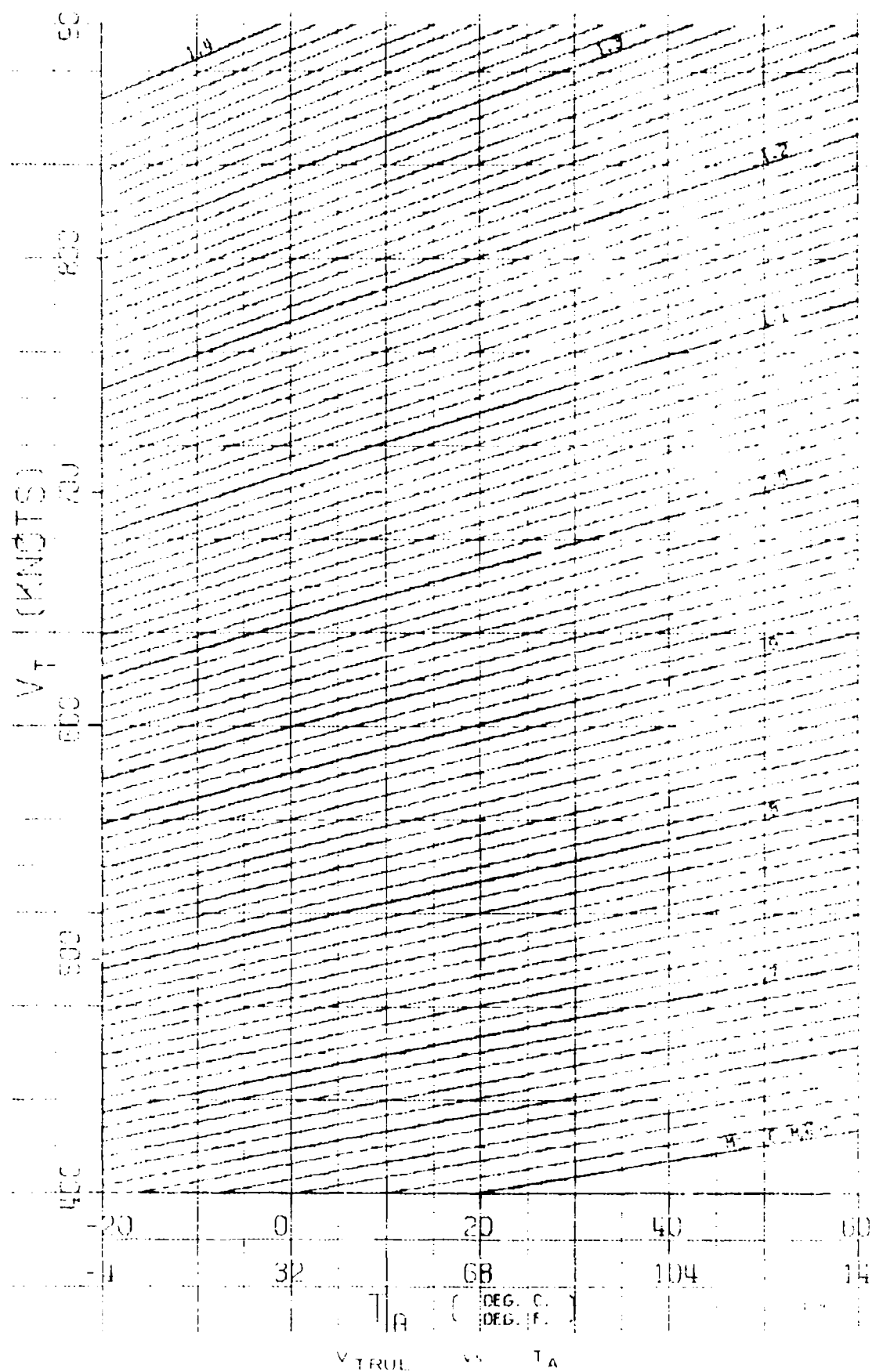
$T_{IC} / T_A$  vs MACH

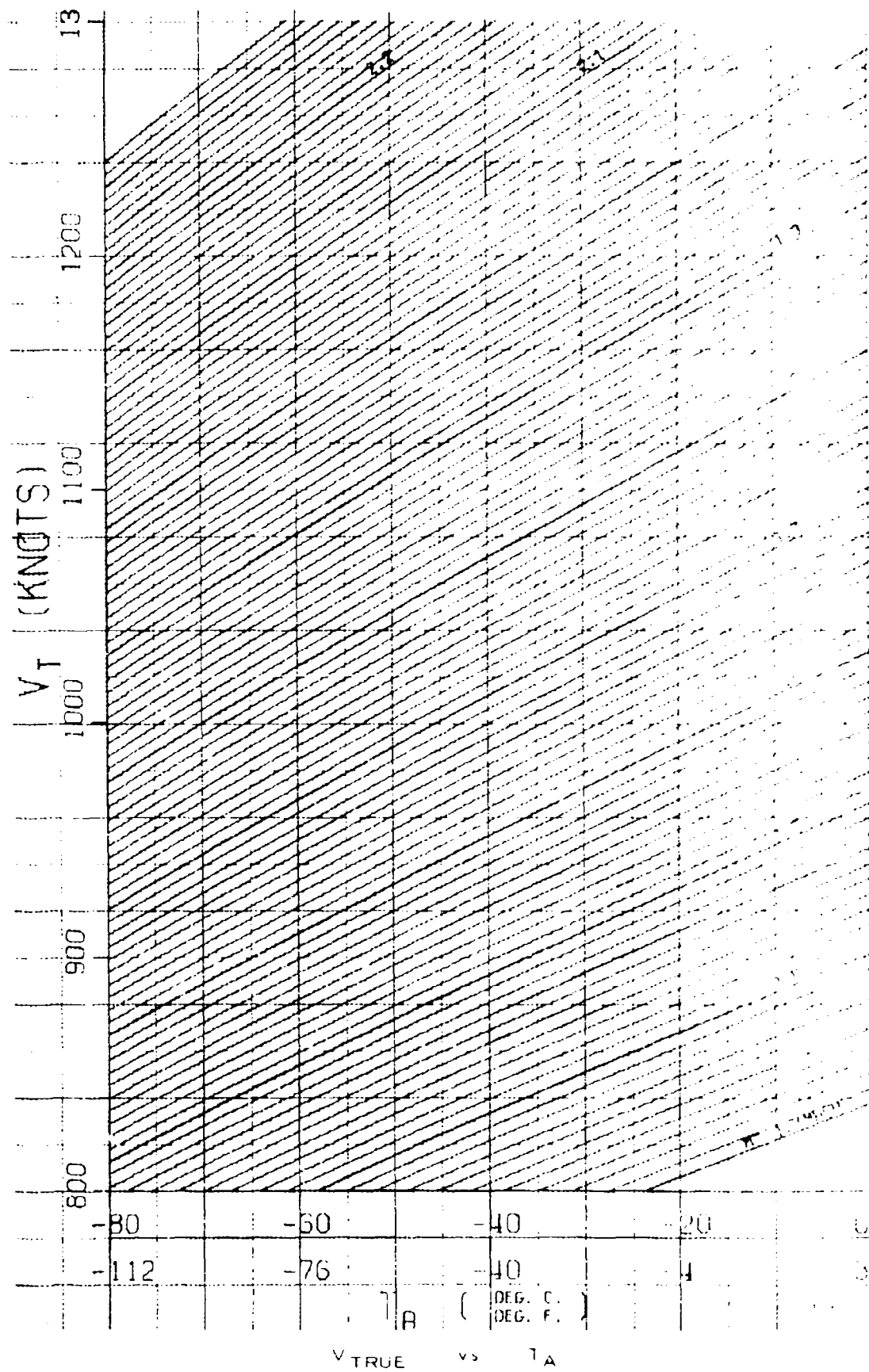


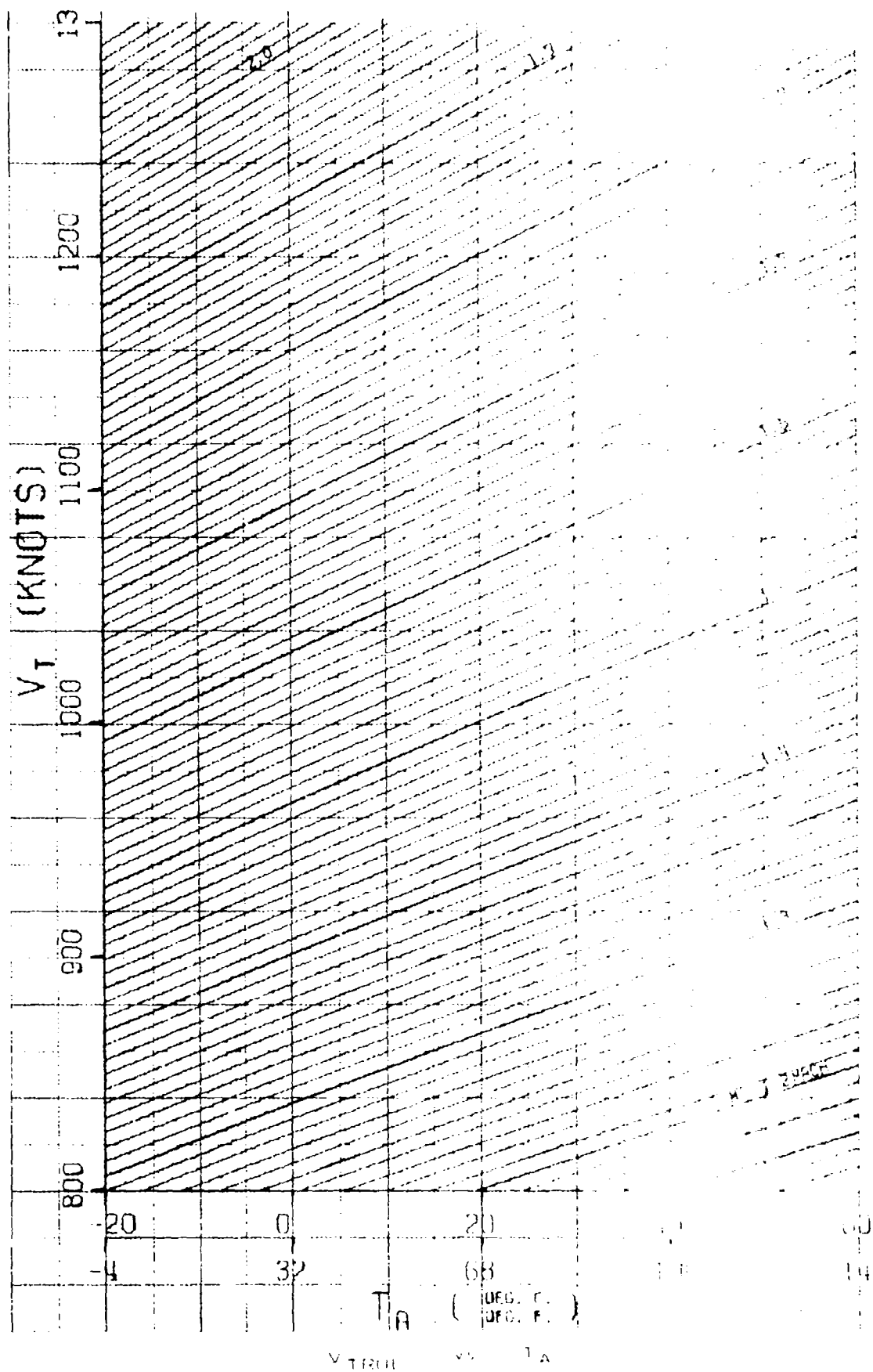




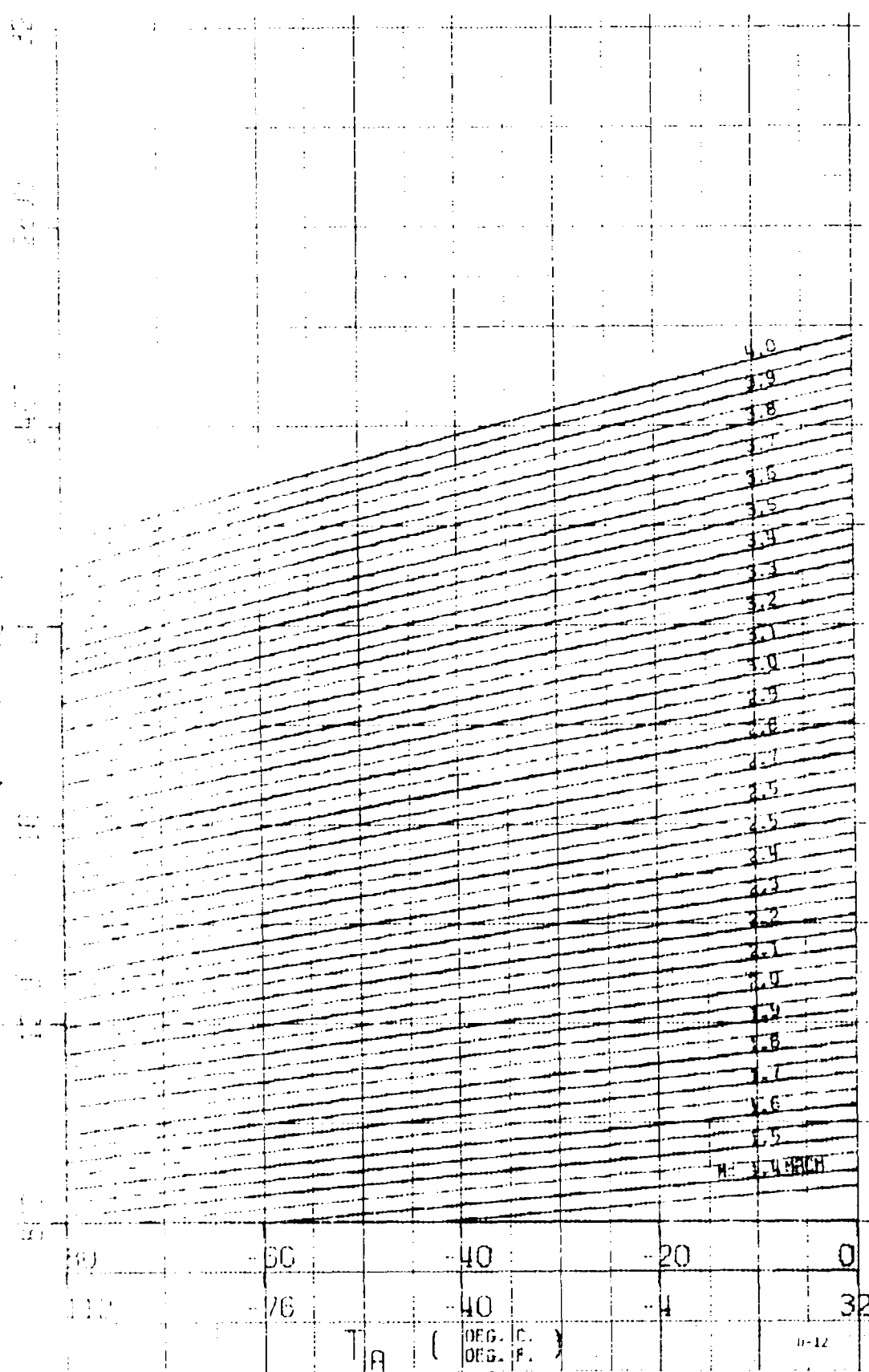








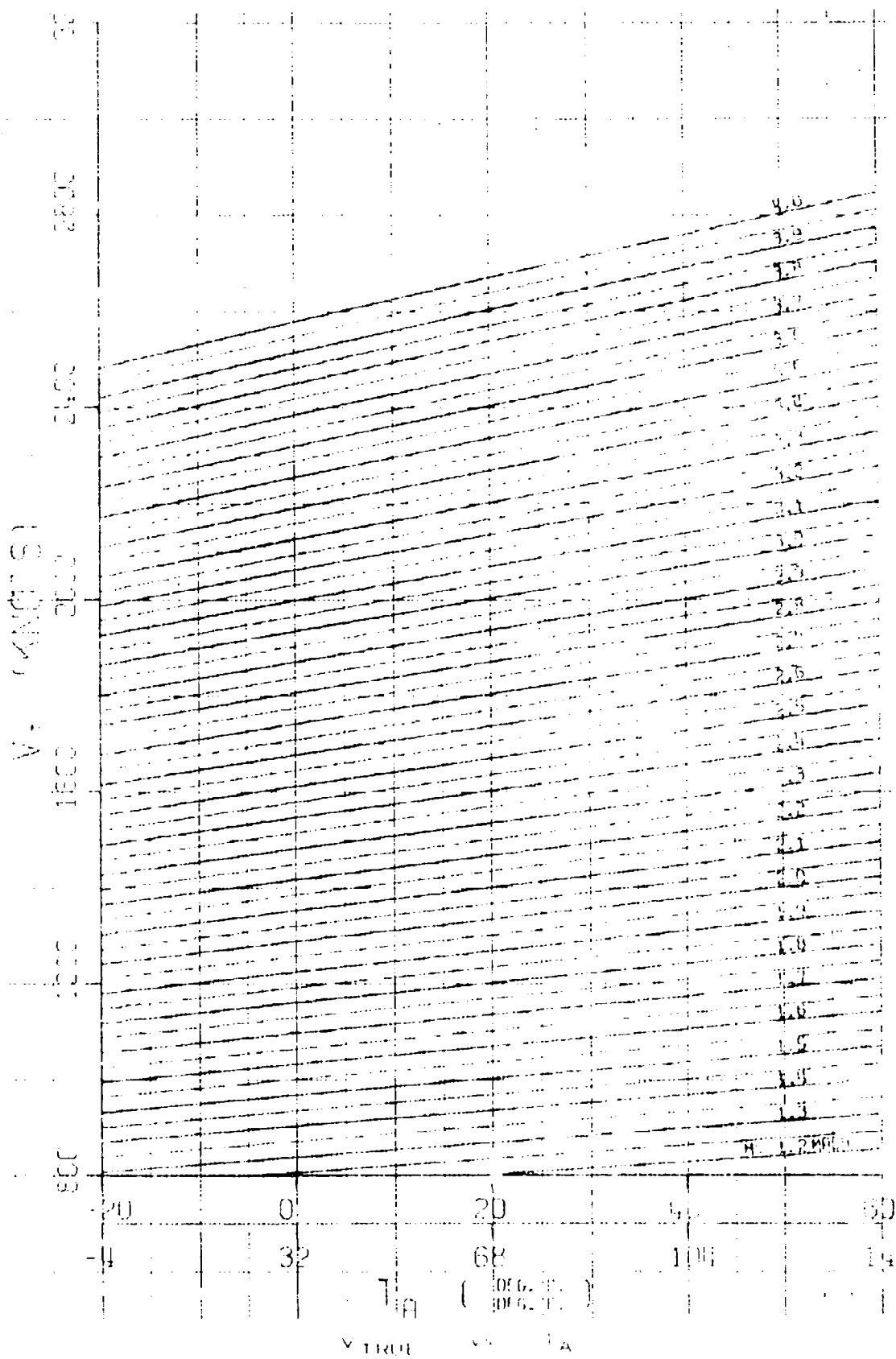
3-20-1-1-1



V TRUE V A T A

( DEG. C. )  
( DEG. F. )

H-12



( )

APPENDIX E

CHARTS OF INTEREST TO THE

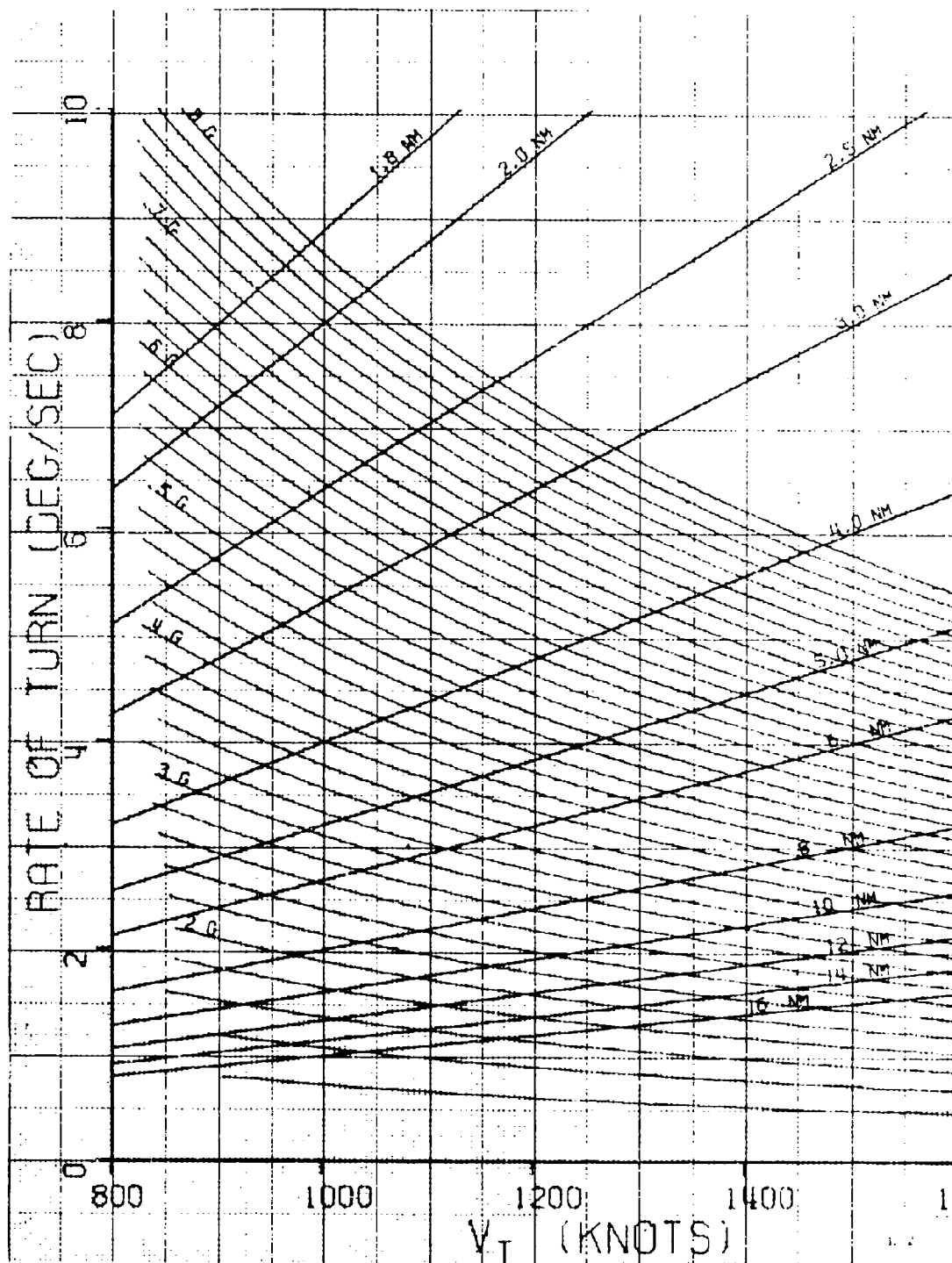
AEROSPACE RESEARCH PILOT SCHOOL

<u>PAGE NUMBER</u>	<u>TITLE</u>
E-1 - E-2	(Rate of Turn vs $V_{\text{True}}$ )
E-3 - E-4	( $F_n/S$ vs $N/\sqrt{T_a}$ ) for J-33-A-23 Engine
E-5	(Ram Pressure Ratio vs Mach)
E-6	Delta Rate of Climb Factor for Turbojets ( $.70 < \eta_r < 1.0$ )
E-7 - E-8	Test Rate of Climb Acceleration Correction
E-9	Tower Flyby Theodolite Calibration
E-10	T-33 Compressible Drag Polars

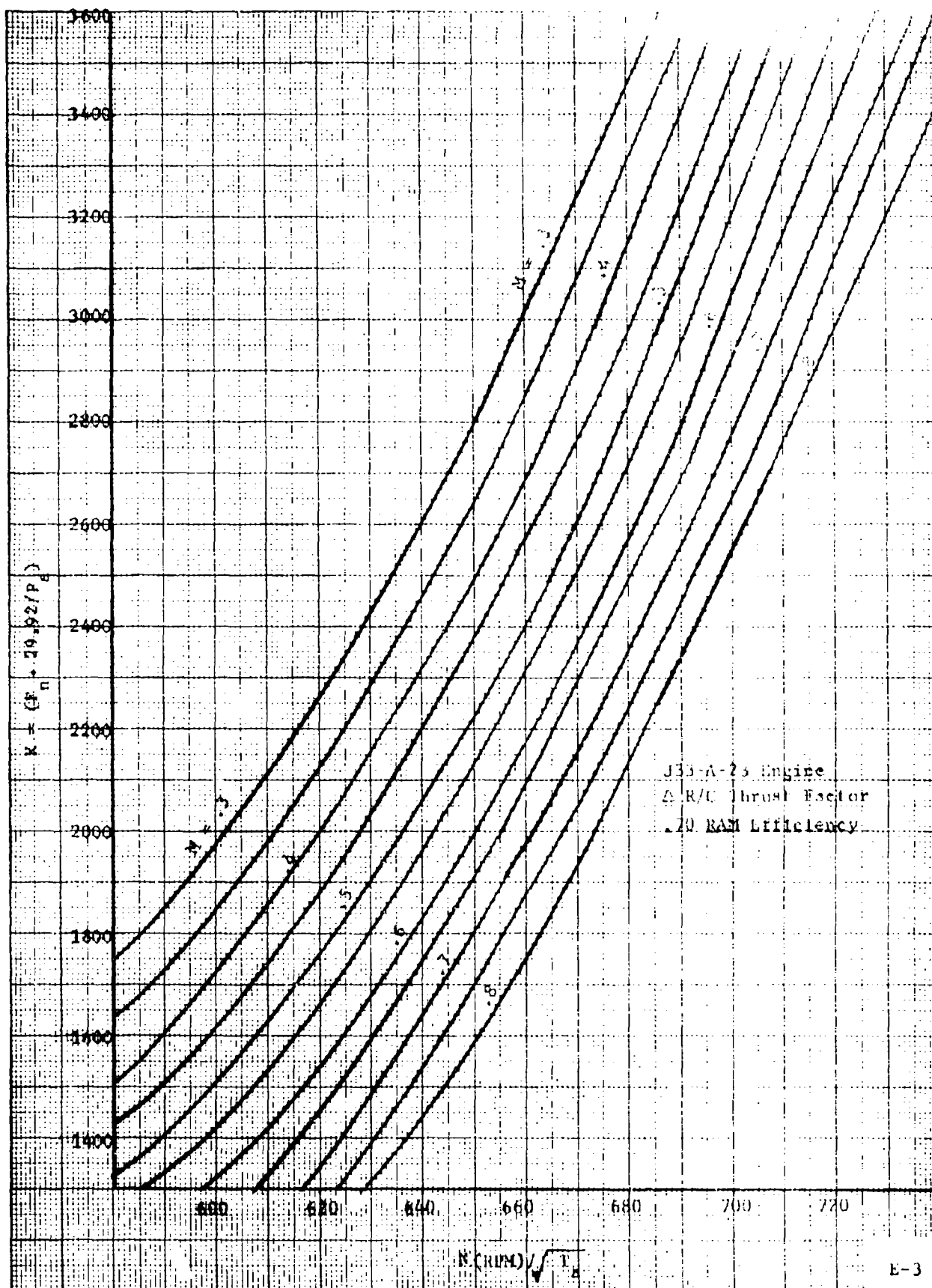
April 1967

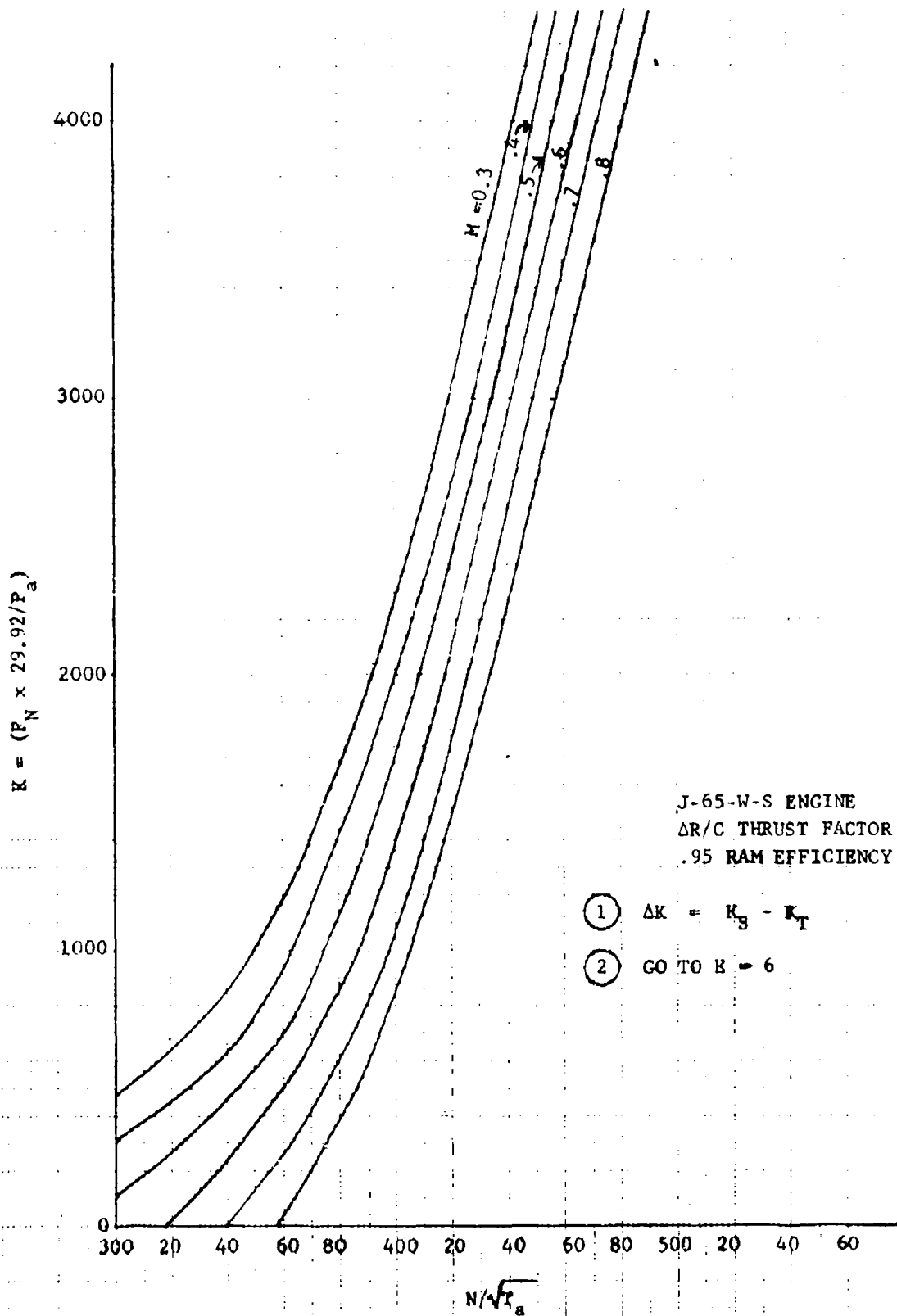


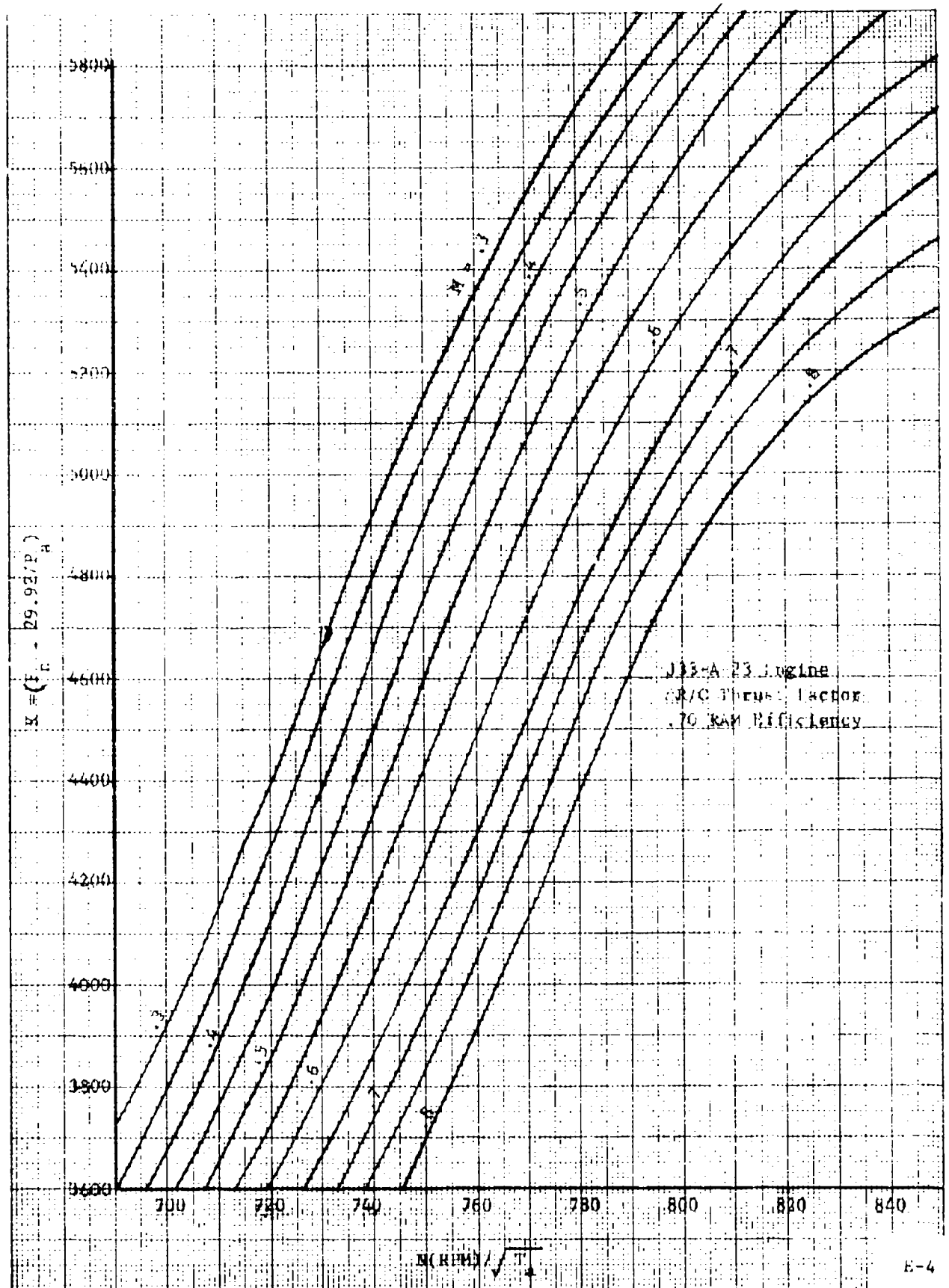


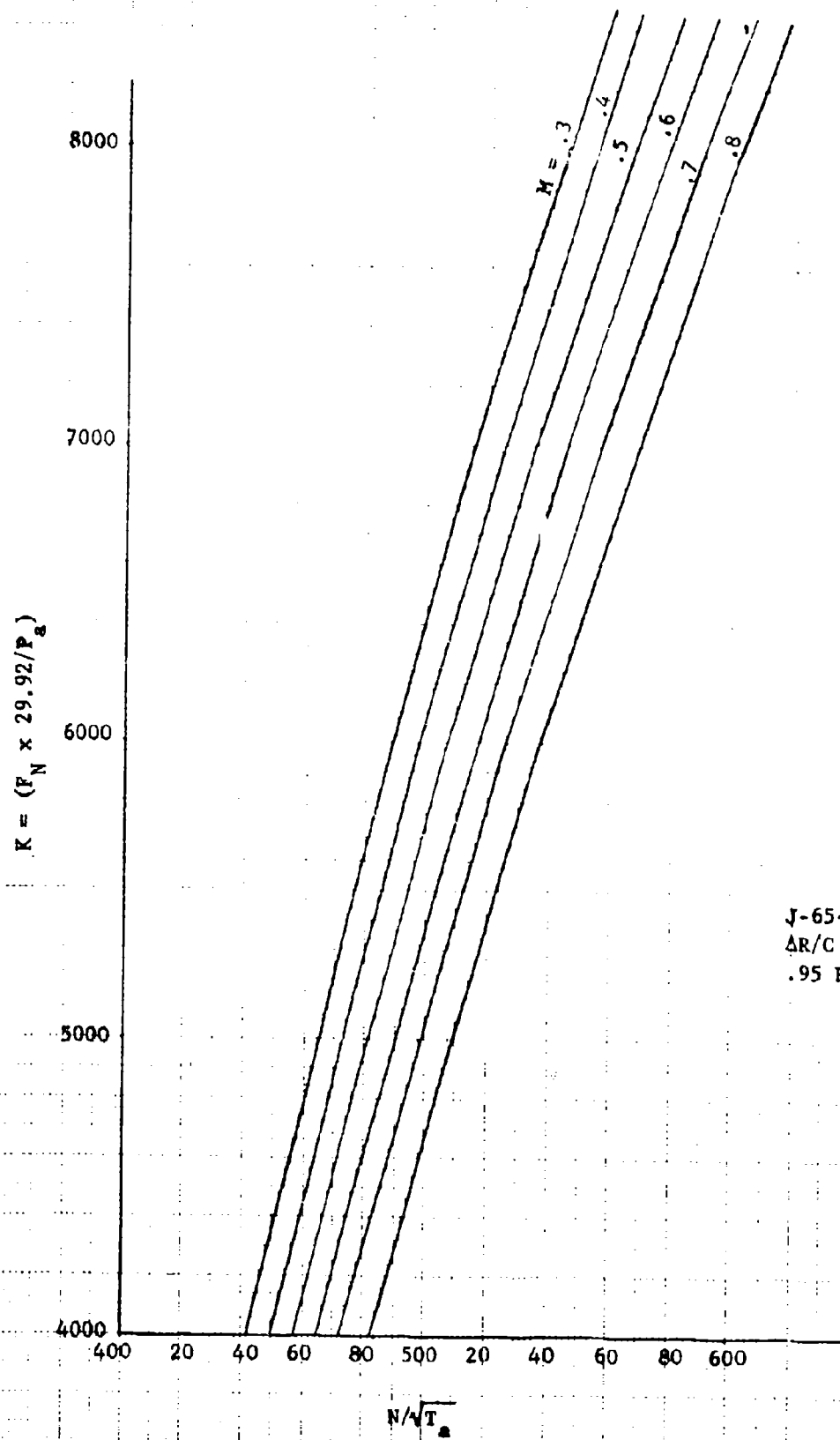


RATE OF TURN vs  $V_{TRUE}$







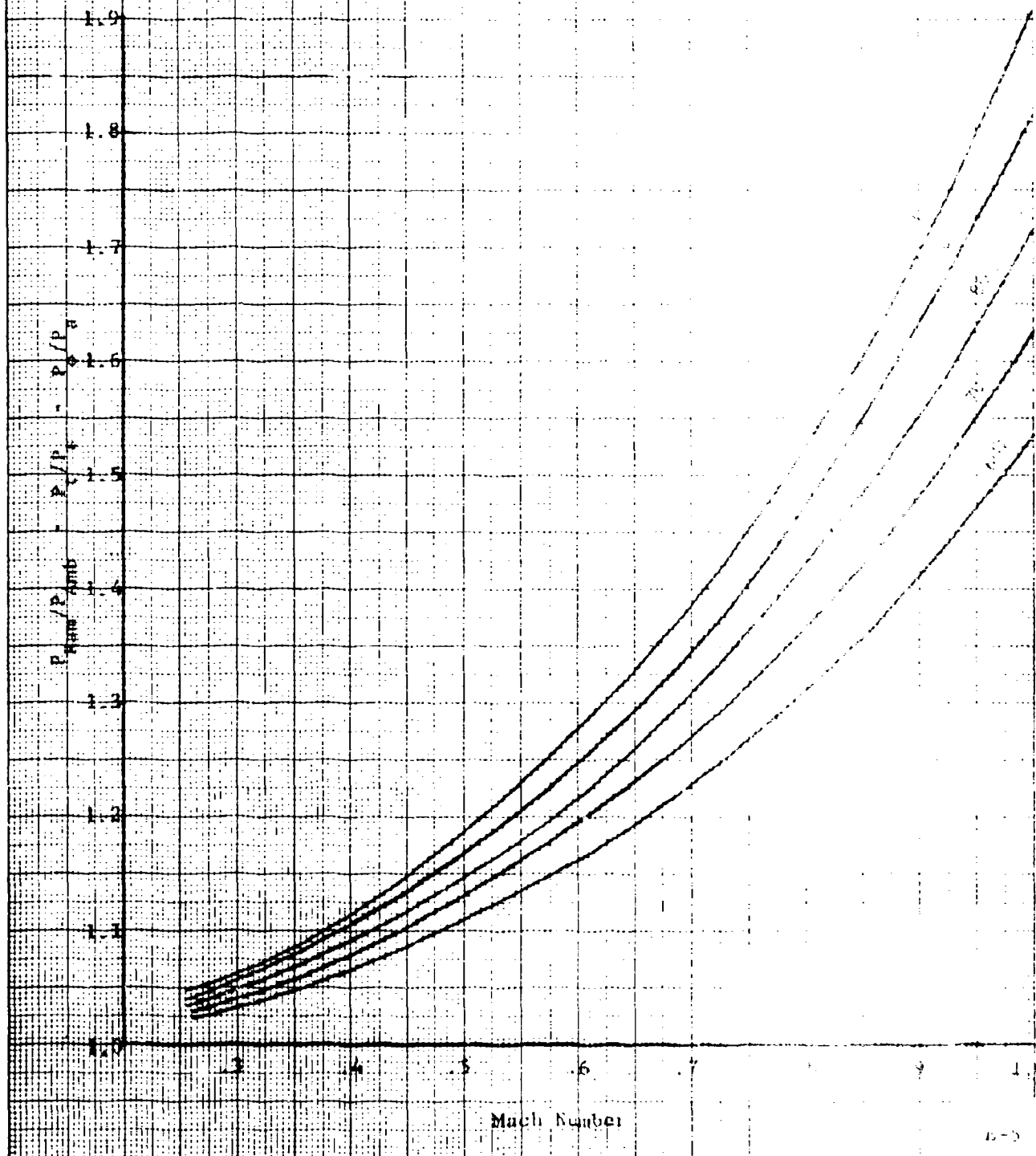


J-65-W-S ENGINE  
AR/C THRUST FACTOR  
.95 RAM EFFICIENCY

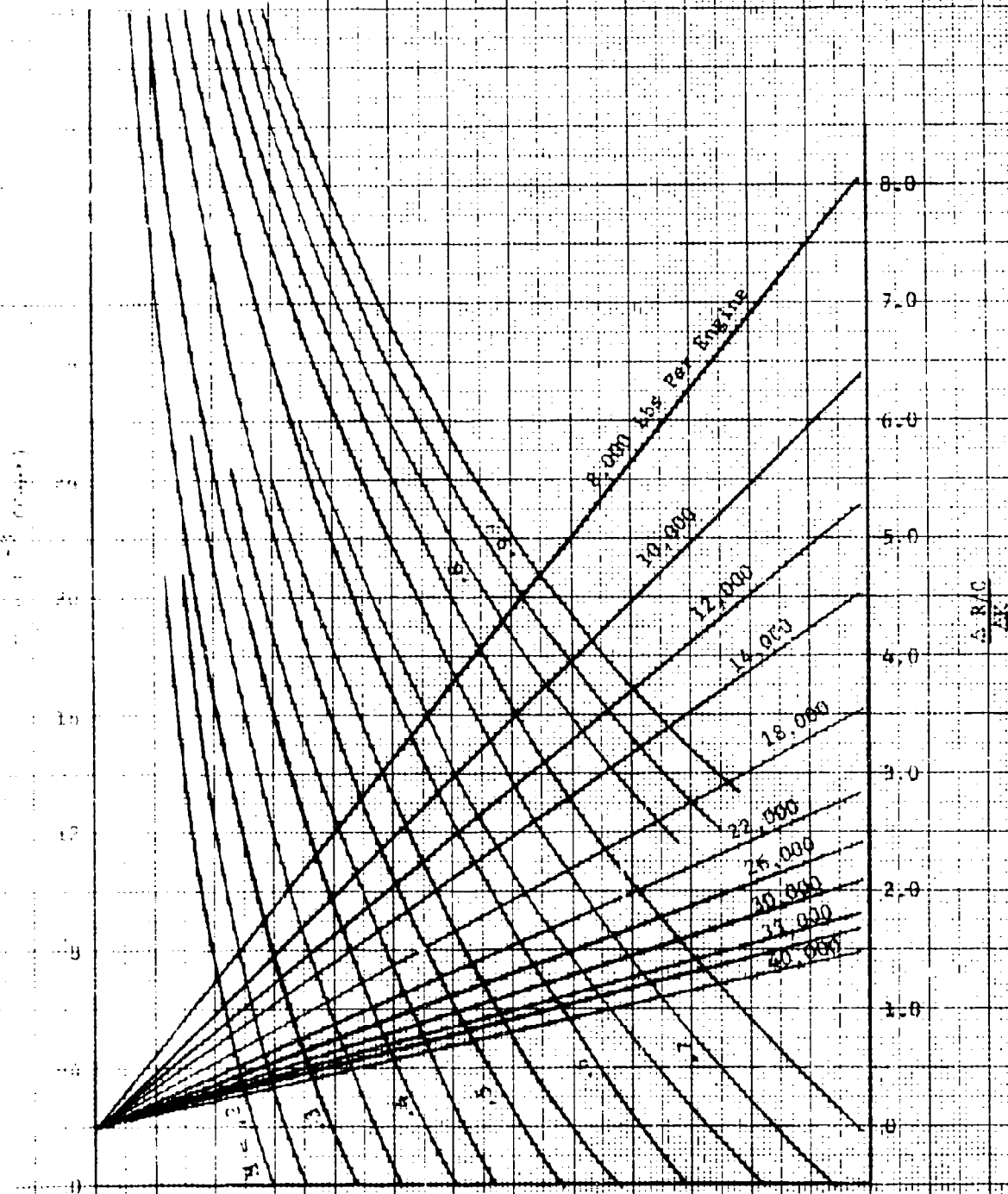
# RAM PRESSURE RATIO vs. MACH NUMBER

$$P_0/P_\infty = \left[ 1 + 0.2(M)^2 \right]^{3.5}$$

$$Z_{RAM} = \frac{P_{0,Act} - P_a}{P_{0,theo} - P_a}$$

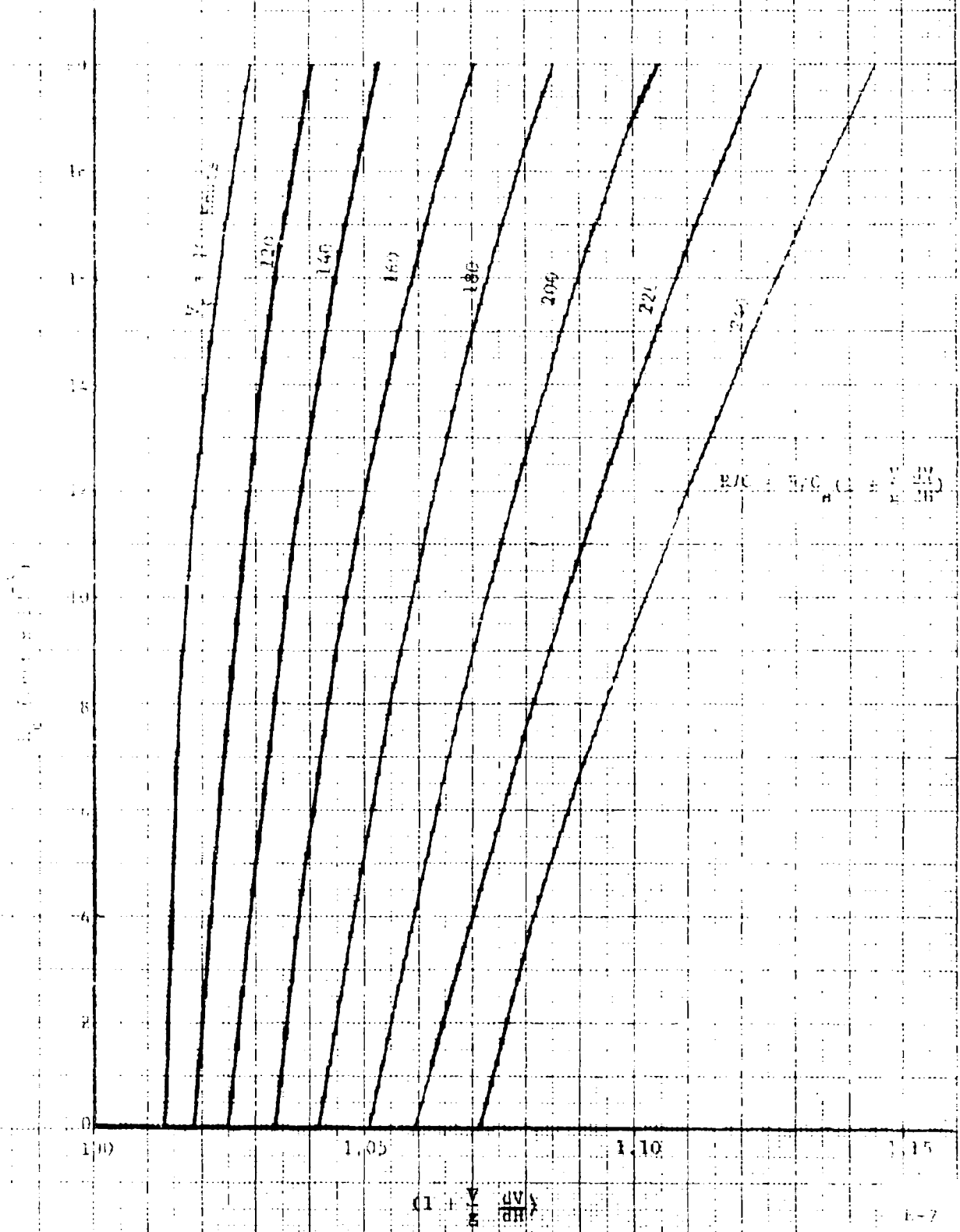


DELTA RATE OF CLIMB FACTOR FOR  
ALL TURBO-JET ENGINES WITH  
RAM EFFICIENCIES OF .70 to 1.0



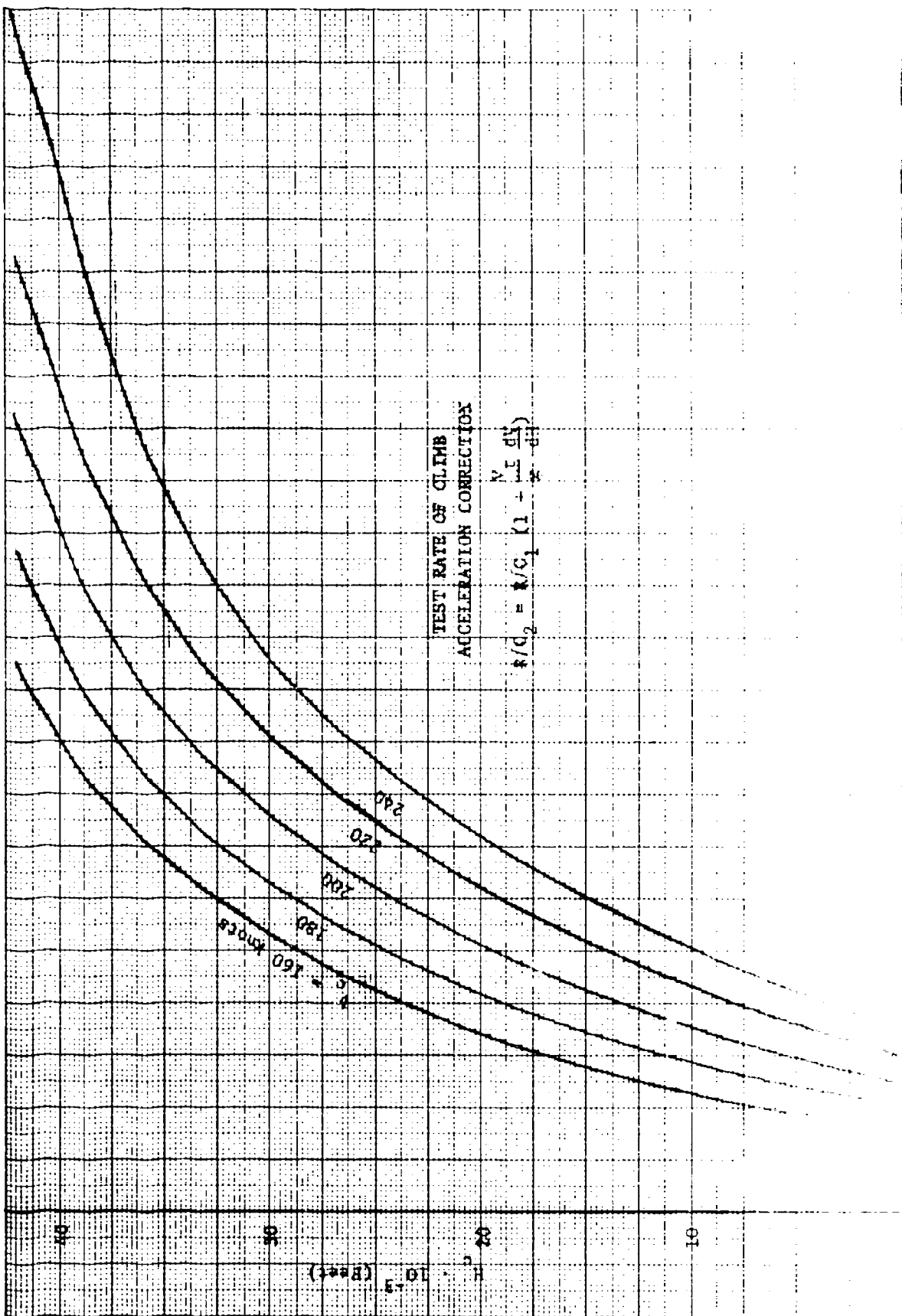


# TEST RAIL OF CLIMB Acceleration Correction

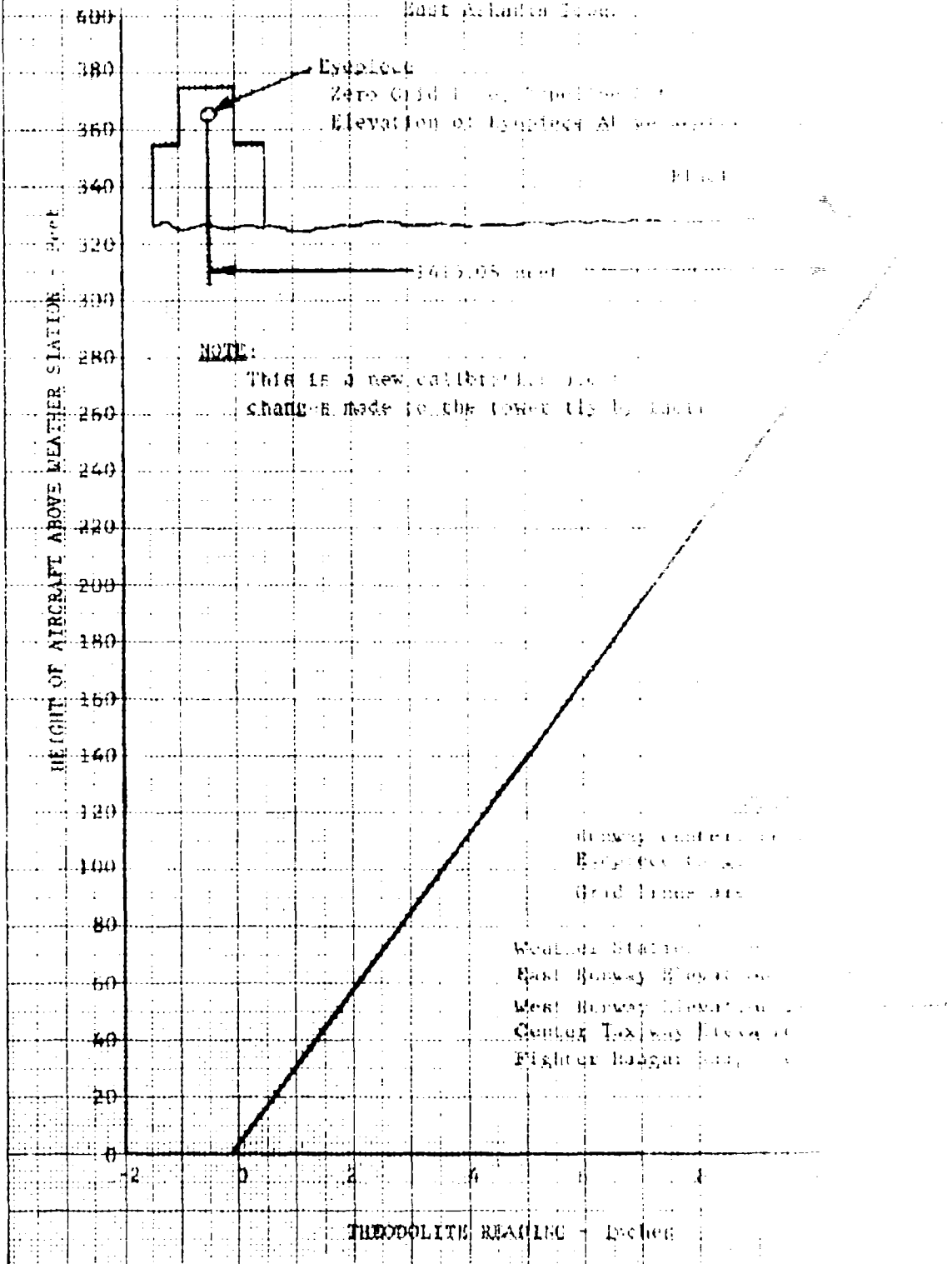


TEST RATE OF CLIMB  
ACCELERATION CORRECTION

$$K/C_2 = K/C_1 \left( 1 + \frac{V}{g} \frac{dV}{dh} \right)$$



East Atlantic Seaw.



LOCKHEED - T-32A

COMPARISON OF TWO PLANS

Two - 120 Gallon Lip Tanks Installed

Ref. LR 6753 Fig. 11

